### UNCLASSIFIED

# GUIDANCE AND NAVIGATION

#### FOR OFFICIAL USE ONLY

This document is residence of the instrumentation Taboratory use and for controlled external distribution. Reproduction of further dissemination is not authorized without express written approval of MAAL this document has not been reviewed by the Security Classifications Office, NACA, and therefore, a not for public release.

265 15367	
- (ACCESSION NUMBER)	(THRU)
15	
(PAGES)	(CODE)
	18
(NASA CR OR TMX OR AD NUMBER)	(CATEGORY)

CAMBRIDGE 39, MASSACHUSETTS

(E-1386) REPORT ON CLEAR RESINS (Massachusetts Inst. of Tech.) 16 p

TECHNOLOGY

0 F

**INSTITUTE** 

**MASSACHUSETTS** 

N78-70107

LEEL CILLS

Unclas 00/27 33751



Of Date: 9/1/5 Approved: Roger B. Woodbury, Associate Director Instrumentation Laboratory

E-1386 REPORT ON CLEAR RESINS

by

Samuel C. Smith August 1963





COPY # 44

#### ACKNOWLEDGMENT

This report was prepared under DSR Project 55-191, sponsored by the Manned Spacecraft Center of the National Aeronautics and Space Administration through contract NAS9-153.

The publication of this report does not constitute approval by the National Aeronautics and Space Administration of the findings or the conclusions contained therein. It is published only for the exchange and stimulation of ideas.

#### E-1386 REPORT ON CLEAR RESINS

į

A 1.1

#### ABSTRACT

After the recommendation of Epocast 1786 and Catalyst 9115 for potting of G. M. E. Modules, certain irregularities were encountered.

Two major problems in Epocast 1786 however, were solved. The problems were first, a pulling away from the corners of its potted case and second, a softening at temperatures above  $120^{\circ}$ F. The former was corrected by pre-heating the case to  $100^{\circ}$ F; the latter, by using Catalyst 955.

One major problem of Chomerics 202 has been that of the resin not bonding to the case. This has been solved by using a solventbased primer known as "Resin 219". However, the susceptibility of the resin to cracking at extreme temperature changes bears watching.

In a third resin, Stycast 1264, the same softening at elevated temperatures which occured with Epocast 1786 was corrected by the addition of Catalyst 9, making the resin a three-part component.

Hysol R8-2038 with Hardener H2-3404, a fourth resin, stood up well under preliminary tests; however, further tests indicated that it does not merit consideration. Three clear resins are recommended for use in potting the G.M.E. Modules.

> by Samuel C. Smith July 1963

> > ٩,

#### E-1386

#### REPORT ON CLEAR RESINS

#### INTRODUCTION

Efforts have been made to correct the irregularities in the use of Epocast 1786 and Catalyst 9115 for the potting of Gimbal Module Electronics (G. M.IE.) Modules by bringing them to the attention of the manufacturer and making successive tests incorporating the manufacturer's recommendations.

Specifically, the resin exhibited certain undesirable features such as pulling away from the corners of the case in which it is cured (see Fig. 1), shrinking abnormally, and softening upon exposure to temperatures above  $120^{\circ}$ F.

The former two faults were annoyingly unpredictable; at times they would occur, and at other times there would be no occurrence even when using the same batch.

Finally, upon advice of Furane Plastics, Inc., the faults were corrected to the extent that repeated tests showed no further pull-away from the corners of the case, and the heat distortion temperature is now higher. There seems to be some improvement on the shrinkage also.

No attempt was made to check the shrinkage per se; however, some idea is obtained by using the same type case for all the samples and comparing the amount of pull on the side of the cases. Since the amount of deflection on the case is 0.002" before potting, any deflection over 0.002" after potting can be attributed to stress from the resin.

At the same time that we were ironing out the problems of Epocast 1786, we were evaluating two other resins. These are Stycast 1264, Parts A and B by Emerson and Cuming, and Chomerics 202/56.





#### STYCAST 1264 (A & B)

Tests conducted indicated that Stycast 1264 (A & B) is suitable in all respects except that, like Epocast 1786/9115, the resin would soften at temperatures above  $120^{\circ}$ F.

The problem was finally corrected when Emerson & Cuming came up with the idea of adding its Catalyst #9 to the two-part resin, now making it a three-part resin. The resin is now light yellow in color rather than water clear as before, but this is not objectionable.

#### CHOMERICS 202/56

In addition to its good electrical and mechanical properties, Chomerics 202/56 remains hard when exposed to temperatures as high as 160°F, and its clear color does not change under any circumstances.

Unfortunately, there was one bad feature. Repeated tests indicated that the resin is not compatible with the Lexan case and will not bond to it.

After some unsuccessful attempts by Chomerics, Inc. to remedy this situation, the Company finally solved the problem with a primer.

#### PROCEDURE

For the sake of brevity and expediency, no attempt will be made to deal with details here. In all cases, except one, the experiment consisted of filling 1 3/4'' long  $\times 7/8''$  wide  $\times 15/16''$  high Lexan cases with Epocast 1786, Stycast 1264 or Chomerics 202.

Note that each case had a deflection of 0.002 inch in its empty state. This is reflected in the deflection column in Table 1. (See Fig. 2 for measuring deflection.)

1. <u>EPOCAST 1786</u>

#### A. EPOCAST 1786 AND CATALYST 9115

Two Lexan cases (Ser. No. F-1, F-2) were filled

#### TABLET

Ser, No.	Resin	Catalyst	Deflection	Deflection After Aging Test	Remarks
E-1	Furane 1786	· <sup>-</sup> 9115	0,005	0.005	Yellow after potting;
B-2	1786	9115	0,004	0,004	almost water clear before potting.
F-20	1786	955	0, 008	0,008	lligh shrinkage. Pulled away at corners.
F-21	1786	955	0.007	0.007	Same
F-22	1786	955	0.008	0.007	Same
E-23	1786	955	0.008	0.008	Same
<b>F-24</b>	1786	955	0.008	ó. 008	Same
FH-30	1786	955	0.005	0.005	Lower shrinkage. No pull away at corners.
FH-31	1786	955	0,005	0.005	Same
FH-32	1786	955	0,003	0.003	Same
FH-33	1786	955	0,004	0.004	Same
FH-34	- 1786	9115	0.005	0.005	
FH-35	1786	9115	0,006	0.006	
E-40	1264 A	в+9	0.002	0.002	······································
E-41	1264 A	B + 9	0.003	0.003	· · ·
E-42	1264 A	B + 9 .	0.001	0.001	
E-50	1264 A	B + 9	0.002	0.002	· · · · · · · · · · · · · · · · · · ·
E-51	1264 . A	В	0.005	0.007	Without Cat. #9
E-52	1264 A	в	0.006	0.006	Without Cat. #9
E-53	1264 A	B + 9	0.004	0.005	
· E-54	1264 A	B + 9	0.004	0.004	Deep yellow after potting.
C-20S	Chomerics 202	56 (Primer 219)	0.004	0.004	
C-60	` <b>†</b> †	56 (Primer 219)	0.006	0.006	
C-61	ti	56 (Primer 219)	0.005	0.005	Retains color.
^ C-62	11	56 (Primer 219)	0.004	0.004	· ·
C-63	ft	56 (Primer 219)	0.005	0.005	·
C-64		56 (Primer 219)	0.004	0.004	
C-65	TF	56 (Primer 219)	0.005	0.005	•
S-1	Stycast 1090	#11	0.002	0.002	
S-2	1090	#11	0.001	0.001	
S-3	1090	#11	0.002	0.002	
H-1	Hysol R8-2038	H2-3404	0.002	0.003	
H-2	х н х	11	0.003	0.004	
H-3	TI TI	11	0.004	0.005	

•

۰.

4

-



Fig. 2

with Epocast 1786/9115. After curing, it was observed that the resin had pulled away from the corners of the case.

#### B. EPOCAST 1786 AND CATALYST 955

Five Lexan cases (Ser. No. F-20 to F-24) were filled with Epocast 1786/955. After curing, these, too, had their corners pulled away from the case.

The experiment was repeated with six other Lexan cases (Ser. No. FH-30 to FH-35); only this time, the cases were pre-heated to  $100^{\circ}$ F. None of the cases exhibited "pull away" at the corners, shrinkage was comparatively low, and the service temperature improved.

We then slit sections 5/16" wide in one of the samples (Ser. No. F-32) and proceeded to separate the sections from the resin by pulling with a spring scale as shown in Fig. 3. An average force of 27 pounds, more than adequate, caused separation.

#### 2. <u>STYCAST 1264 (A&B)</u>

Two Lexan cases (Ser. No. E-51, E-52) were filled with Stycast 1264(A&B). After curing, the samples were exposed to temperatures of  $125^{\circ}$ F. This caused them to soften.

The experiment was repeated with six other samples (Ser. No. E-40, E-41, E-42, E-50, E-53, E-54). This time E&C Catalyst 9 was added to the 1264 (A&B) in a definite ratio.

Two of the cured samples were later exposed to a temperature of  $150^{\circ}$ F, at which point they could barely be deformed with the corner of a 6-inch scale. The samples were allowed to cool and then were put back in the oven with the temperature lowered to  $140^{\circ}$ F. After one hour, they were again tested for hardness. It was found that at  $140^{\circ}$ F the resin remained hard.

As with the previous resin, 5/16" wide slits were cut and an average force of 8 pounds caused separation between the resin and the case. Although a larger separating force would have been desirable, this was acceptable.



Fig. 3

#### 3. <u>CHOMERICS 202/16</u>

Four samples were cured as in previous cases (Ser. No. C-10 to C-13). It was observed that the cured resin would not bond to the Lexan case. Subsequently, two other samples were first coated with the resin and then allowed to cure at  $200^{\circ}$ F as per direction of Chomerics, Inc. These samples were then filled with the resin and allowed to cure at  $160^{\circ}$ F. Still, there was no bond.

The experiment was repeated with six other samples, this time pre-coated with Chomerics' new primer, Resin 219. Good bonding resulted and an average force of 10 pounds was necessary to cause separation. Scratching the case before priming increased the force to 26 pounds. However, a force of 10 pounds is ample

The resin was later exposed to a temperature of  $160^{\circ}$ F with no material change in the hardness.

#### 4. <u>HYSOL R8-2038</u>

At the time this report was being prepared, Mr. Donald Gilchrist of G.E., who has made some inquiries into clear resins in connection with the Polaris Program, gave us a sample of a recommended clear resin, namely Hysol R8-2038. Preliminary tests indicated a favorable comparison with the other resins.

It was particularly observed that the high linear shrinkage indicated in Hysol's brochure was not apparent in the tests made for comparative shrinkage. This, perhaps, indicates the inconclusiveness of this test method.

Although it was noted at the end of an aging test that the deflection increased slightly, and although it is not uncommon with clear resins that an apparent low shrinkage may become high over a period of time, further tests indicated that R8-2038 has an initial high shrinkage and negligible aging shrinkage

Table 1 shows the deflection of the various modules shortly after curing and 170 hours later. These modules were kept in the oven at  $150^{\circ}$ F for 170 hours to simulate possible slow shrinkage over 3 to 4 months at room temperature. All of the clear modules, except Chomerics 202, turned deep yellow in color. The color of Chomerics remains the same.

In lieu of a linear shrinkage test, which is somewhat too involved, we have proceeded to determine the comparative shrinkage by the percent volume loss of the various modules. This method is accurate to within 5 per cent.

The resin is air evacuated and poured into a 1.000 inch diameter by 1.271 inches deep (1.000 cubic inch) polished steel cylinder flush with the top.

After curing, the weight in grams of an amount of water necessary to refill the steel cylinder was noted. The water was then removed and the specimen placed in the oven at 150°F for 170 hours for aging test. At the end of this period, the cylinder was again filled with water and the weight noted. The water was emptied and the specimen placed briefly in an oven for drying.

An amount of the same type of resin necessary to fill the cylinder was added and the weight noted. This gave us the maximum volume loss over the aging test period.

The water was used to determine the volume loss, if any, between the time the resin was cured and the time the aging test ended. As shown in Table 2, slight increase in shrinkage over a period of time is expected. Contrary to our expectation, Hysol R8-2038, which exhibited a comparative high shrinkage, indicated negligible continuous shrinkage over a period of time. So does Stycast 1264 with Catalyst 9 added.

#### PROPERTIES

Table 2 compares the properties of Epocast 1786/955,

TABLE 2

• •

PROPERTY COMPARISON					
PROPERTIES	Chomerics 202/56	E & C Stycast 1264 Cat. B+9	Furane Epocast 1786/955	Hysol R8-2038	Stycast 1090
Specific Gravity (cured)	1.14	1.20 1.10	1.19	1.12 1.22	0.78
Viscosity (cps)	5000 at 75 <sup>0</sup> F	950 at 72 <sup>0</sup> F	4000 at 75 <sup>0</sup> F	500-1300 at 77° F	10,000
Shore D Hardness	84 at RT 70 at 140° F*	80 at 72 <sup>0</sup> F 76 at 140 <sup>0</sup> F*	88 at 80 <sup>0</sup> F 64 at 140 <sup>0</sup> F*	75 64 at 140 <sup>0</sup> F*	-
Volume Resistivity (ohm - cm)	7, 1 × 10 <sup>15</sup>	40×10 <sup>14</sup>	$1 \times 10^{15} (75^{\circ})$ 6.7 × 10 <sup>8</sup> (210 <sup>°</sup> )	4.1×10 <sup>14</sup>	$5 \times 10^{16}$ $1 \times 10^{13}$
Dielectric Strength (v/mil)	-	-	-	-	300
Dielectric Constant	4.3 (1 mc)	3.5 (60 to 10 <sup>10</sup> cps)	3.9 (10 <sup>4</sup> cy) 3.5 (10 <sup>6</sup> cy)	4.2 (1025 cps) 4.0 (105 cps)	$(10^2 to 10^{10} cps)$
Dissipation Factor	0.035 (1 mc)	<0.02 (60 to 10 <sup>10</sup> cps)	$\begin{array}{c} 0.020 \ (10^4 \text{ cy}) \\ 0.029 \ (10^6 \text{ cy}) \end{array}$	$0.010 (10^2 \text{cps})$ $0.027 (10^5 \text{cps})$	$(10^2 to 10^{15} 10 cps)$
Coefficient of Thermal Expansion (in/in/ <sup>0</sup> C)	58.8×10 <sup>-6</sup>	45 × 10 <sup>-6</sup>		61×10 <sup>-6</sup>	19×10 <sup>-6</sup>
Thermal Conductivity (BTU/ft <sup>2</sup> /hr/ <sup>0</sup> F/in)	-	1.5	1.2	1.6	0.8
Izod Impact (ftlb/in notch)	0.43 at 180 <sup>0</sup>	5.0	-	-	0.25
H <sub>2</sub> O Absorption (Wt. % gain)	<u> </u>	0.3 (24 hrs-RT)	1 2 (2 hrs-boil)	0.2 (24 hrs-RT)	0.3 (24 hrs-25 <sup>0</sup> C)
Mixing Ratios (A-B pbw)	100-15	100-20 + 6 #9	100-10	100-11	100-13
Pot Life	5 hrs	3 hrs	20 min	20 min	4 hrs
Cure Time	24 hrs at 140 <sup>0</sup> F 16 hrs at 160 <sup>0</sup> F	48 hrs at RT 8 hrs at 110 <sup>0</sup> F 3 hrs at 150 <sup>0</sup> F	16 hrs at RT +1 hr at 150 <sup>0</sup> F	2 hrs at 140 <sup>0</sup> F or 24 hrs at RT	3 hrs at 16 <sup>0</sup> F then 7 hrs at 180 <sup>0</sup> F
Discoloration Temperature ( <sup>0</sup> F)	>212	>200	-	-	-
Heat of Distortion Temperature ( <sup>O</sup> F)	180	145*	145*	145*	300
Linear Shrinkage	· _	-	0.0025 in/in	1.2%	$10.4 \times 10^{-6}$ in/in/°F
Volume Loss (%)	4.0*	6.1*	5.1*	6.7* .	3.2*
Shrinkage Ratio (aging/immediate)	1.32 *	1.02 *	1.22 *	1.02 *	wetting problem

\* Per MIT Test. All other values are given by the company.

Chomerics 202/56, Stycast 1264 (A&B) and Hysol R8-2038 together with an opaque resin, Stycast 1090. It is not known at this time how the properties of Stycast 1264 are affected by the addition of Catalyst 9.

Finally, tests were made to determine the resistance to thermal shocks. The modules were placed in a chamber and temperature cycled as follows:  $-60^{\circ}$ F for 30 minutes,  $72^{\circ}$ F for 15 minutes,  $250^{\circ}$ F for 30 minutes and  $72^{\circ}$ F for 15 minutes. The modules were then removed from the chamber and examined.

The cycle was repeated 5 times examining the modules at the end of each cycle.

Examination under a microscope revealed no cracks in any of the modules. Both chomerics and Stycast 1090 separated from their cases, and there was very mild separation in the case of Chomerics. Hysol R8-2038 exhibited some irregular soft spots. This irregularity was found in a number of samples(Hysol). A previous test consisted of the following: a steel washer 1 1/4''diameter, 1/4'' thick and having four triangular prongs at the outermost part of its faces was embedded in the resin to form a sample 2 1/4'' in diameter and 1/2'' thick.

This sample was then placed in the chamber at  $250^{\circ}$ F for 30 minutes, then at  $-50^{\circ}$ F for 30 minutes.

In all cases, including the opaque stycast 1090 sample, cracks developed.

This test was admittedly too severe in view of the geometric configuration of the washer and the difference in coefficient of expansion between it and the resin.

In addition to the previous milder thermal shock test, the above mentioned washers were embedded in the resins and examined after curing. There was a very slight crack at one point in the Chomerics 202 and in the Hysol R8-2038; no cracks appeared

in the other clear resins. This test, known as the Therman shock test, is a reliable and generally accepted one.

A point worth making is that varying degrees of hardness are obtained depending on the extent of postcuring. Tests at the end of the aging period recorded a shore D hardness of 70 for Epocast 1786/955 and 82 for the other three resins.

#### CONCLUSION

As a result of the tests, it is concluded that all the resins except Hysol R8-2038 are recommended for use in the G. M. E. with preference given to Stycast 1264.

In spite of its higher shrinkage factor, Stycast 1264 is chosen over Epocast 1786 because of its extremely low viscosity, which is a desirable feature in potting certain modules which present de-airing problems.

If viscosity is not a problem, Epocast 1786 is preferred to Stycast 1264 and both of these are preferred to Chomerics.

In potting G. M. E. Modules with connectors, however, viscosity is a problem and consequently Stycast 1264 should be used. It is recommended that unless Epocast 1786/955 is used, the Lexan cases should be sandblasted or otherwise roughened for better adhesion.

#### EQUIPMENT USED

Blue M oven Mini Mite therometer Ohaus Dial Torsion Balance (0.02 gram readability) Weights, Class S Hunter spring scale Starrett straight edge Vacuum unit Shore D hardness tester Delta Design Chamber (-100°F to + 600°F) American Optical Microscope Model #59M-1

#### E-1386 DISTRIBUTION LIST

Int	er	na	1

R. Alonso	D, Hoag
J. Arnow (Lincoln)	F. Houston
R. Barrieau	L. Junod (CDR)
W. Bean	B. Katz
J. Bimshas	R. Kowalski
M. Biren	M. Kramer
D. Bowler	W. Kupfer
A. Boyce	A. Laats
C. Briggs	D. Ladd
R. H. Brown	J. Lawrence (MIT/GAEC)
P. Bryant	L. Martinage
G. Bukow	G. Mayo
R. Bumstead	J. McNeil
S. Copps	John Miller
B. Cuevas	S. Molloy
O. DeTommaso	J. Nugent
B. Dew	B. Olsen
F. Donald	M. Prisant
E. Duggan	J. Salani
K. Dunipace (MIT/AMR)	P. Sarmanian
R. Egan	J. Shillingford
S. Felix (MIT/S&ID)	T. Shuck
J. Fish	S. Smith
E. Fisher	W. Stameris
S. Forter	D. Test
W. Foss	R. Therrien
S. Goodwin	M. Trageser
Eldon Hall	R. Weatherbee
R. Haltmaier	L, Wilk
I. Halzel	R. Woodbury
E. Hickey	W. Wrigley
	P. Zicko
	Apollo Library (2)

MIT/IL Library (6)

External	and the second	
(ref. APCAI	N; 2 July 1963)	
P. Ebersole (N.	ASA/MSC)	(2)
W. Rhine (NAS	A/RASPO)	(1)
S, Gregorek (N	AAS&ID/MIT)	(1)
T. Hueurmann	(GAEC/MIT)	(1)
AC Spark Plug		(10)
Kollsman		(10)
Raytheon	· · · · · · · · · · · · · · · · · · ·	(10)
WESCO		(2)
Capt. W. Delar	ney (AFSC/MIT)	(1)
NAA RASPO:	National Aeronautics and Space Administration Resident Apollo Spacecraft Project Officer North American, Inc. Space and Information Systems Division 12214 Lakewood Boulevard Downey, California	(1)
CAPE:	National Aeronautics and Space Administration Atlantic Missile Range Operations Port Canaveral, Florida Attn: Mr. B. P. Brown	(3)
HDQ:	NASA Headquarters 1520 H Street Washington, D.C. Attn: Mr.G.M. Low, MD(P)	(6)
AMES:	National Aeronautics and Space Administration Ames Research Center Moffett Field, California Attn: Mr. Matthews	(2)
LEWIS:	National Aeronautics and Space Administration Lewis Research Center Cleveland, Ohio	(2)
FRC:	National Aeronautics and Space Administration Flight Research Center Edwards AFB, California	(2)
JPL:	National Aeronautics and Space Administration Jet Propulsion Laboratory Pasadena, California Attn: Mr. H. R. Lawrence	(2)

.

.

LRC:	National Aeronautics and Space Administration Langley Research Center Langley AFB, Virginia Attn: Mr. A. T. Mattson	(2)
GSFC:	National Aeronautics and Space Administration Goddard Space Flight Center Greenbelt, Maryland	(2)
MSFC:	National Aeronautics and Space Administration George C. Marshall Space Flight Center Huntsville, Alabama Attn: Dr. Kuettner	(2)
GAEC:	Grumman Aircraft Engineering Corporation Bethpage, Long Island New York Attn: Mr. A. Whitaker	(1)
NAA:	North American Aviation, Inc. Space and Information Systems Division 12214 Lakewood Boulevard Downey, California Attn: Mr. R. Berry	(1)
GAEC RASPO:	National Aeronautics and Space Administration Resident Apollo Spacecraft Project Officer Grumman Aircraft Engineering Corporation Bethpage, L. I., New York Attn: Mr. Jack Small	(1)
WSMR:	National Aeronautics and Space Administration Post Office Drawer D White Sands Missile Range White Sands, New Mexico	(2)
MSC:	National Aeronautics and Space Administration Manned Spacecraft Center Apollo Document Control Group (SDG) Houston 1, Texas	(45)
General Electri	c Co. O. D.	

•

100 Plastics Avenue Pittsfield, Massachusetts

Director, Special Projects Office (SP 2303) Department of the Navy Washington 25, D.C.

## UNCLASSIFIED

UNCLASSIFIED