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GEMINI 8 INERTIAL GUIDANCE SYSTEM EVALUATION AND TRAJECTORY RECONSTRUCTION (U)

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3150-6036-R8-000 Page iii

ABSTRACT

The report contains a detailed evaluation of the Gemini 8 inertial guidance system accuracy during the ascent and reentry phases of the mission. An analysis of the external tracking instrumentation accuracy during ascent is also included. The results of the error analyses are used to construct a reference Gemini 8 trajectory for the ascent and reentry portions of the mission.

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Postflight reconstructions of the Gemini and Agena trajectories during the rendezvous interval are differenced and compared with the onboard rendezvous radar relative position measurements in an attempt to evaluate the onboard radar accuracy.

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3150-6036-R8-000 Page v

CONTENTS

			Page
1.	INTR	ODUCTION AND SUMMARY	1-1
2.	INER PER I	TIAL GUIDANCE SYSTEM	2-1
	2.1	IGS Error	2-6
	2.2	IMU Error	2-6
		 2.2.1 Accelerometer Bias Determination 2.2.2 Error Source Regression Results 2.2.3 Discussion of Error Analysis 2.2.4 Preflight Measurement of IMU Errors 	2-7 2-8 2-11 2-15
	2.3	Azimuth Update	2-19
	2.4	Reference Ascent Trajectory	2-20
3.	REEN	NTRY IGS EVALUATION	3-1
	3.1	Initial Conditions	3-1
	3.2	Platform Misalignment	3-5
	3.3	Simulation Results	3-7
		3.3.1 MSC Simulation 3.3.2 McDonnell 6-Degree-of-Freedom	3-7 3.8
			2 0
	3.4	Reference Reentry Trajectory	3-0
4.	TRAC	CKING SYSTEM PERFORMANCE	4-1
	4.1	GE Mod II	4-2
		4.1.1 GE Mod III/Burroughs(TRW-Processed) 4.1.2 GE Mod III/Burroughs(GE-Processed)	4-2 4-2
	4.2	MISTRAM	4-2
		4.2.1MISTRAM I.4.2.2MISTRAM II (Passive Mode)	4-4 4-4
	4.3	AFETR Best Estimate of Trajectory	4-4
		4.3.1 MISTRAM - Only BET	4-4 4-5
	4.4	TRW TOPS BET	4-5
5.	RENI	DEZVOUS RADAR EVALUATION	5-1
	5.1	TRW/Rendezvous Radar Comparison	5-1
	5.2	RTCC/Rendezvous Radar Comparison	5-3

2

į

3150-6036-R8-000 Page vi

UNCLASSIFIED

CONTENTS (Continued)

APPENDIXES

Α	Ascent Trajectory	A-1
В	Reentry Trajectory	B-1
С	IMU Calibration History	C-1
D	Error Source Regression Analysis	D-1
REFERENC	CES	R-1

Total Pages: 162

UNCEASSIFIED

3150-6036-R8-000 Page vii

Page

ILLUSTRATIONS

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2-1	GE/Final and 100K MISTRAM △V Sensed Coordinates	2-2
2-2	GE/Final and 100K MISTRAM $\triangle V$ Guidance Inertial Coordinates	2-3
2-3	GE/Final and 100K MISTRAM △P Guidance Inertial Coordinates	2-4
2-4	Navigation Velocity Error	2-5
2-5	IGS Error Source Contribution to Sensed Velocity Differences - x Axis	2-13
2-6	IGS Error Source Contribution to Sensed Velocity Differences - y Axis	2-14
2-7	IGS Error Source Contribution to Sensed Velocity Differences - z Axis	2-16
2-8	Sensed Coordinates ΔV With Recovered IMU Error Source Fit	2-17
2-9	Sensed Coordinate △V With Preflight Measured Error Source Fit	2-18
3-1	Map of Estimated Impact Points	3-3
3-2	Effects of Initial Conditions and IMU Corrections Upon IGS Trajectory	3-4
3-3	Reentry Trajectory Comparison (Simulation-TRW/BET) x Axis	3-10
3-4	Reentry Trajectory Comparison (Simulation-TRW/BET) y Axis	3-11
3-5	Reentry Trajectory Comparison (Simulation-TRW/BET) z Axis	3-12
3-6	Gemini 8 Retrofire - IGS Measured Sensed Velocities and Accelerations (x Axis)	3-13
3-7	Gemini 8 Retrofire - IGS Measured Sensed Velocities and Accelerations (y Axis)	3-14
3-8	Gemini 8 Retrofire - IGS Measured Sensed Velocities and Accelerations (z Axis)	3-15

UNCLASSIFIED

Page viii

3150-6036-R8-000 UNCLASSIFIED

ILLUSTRATIONS (Continued)

		Page
3-9	Gemini 8 Reentry - IGS Measured Sensed Velocities and Accelerations (x Axis)	3-16
3-10	Gemini 8 Reentry - IGS Measured Sensed Velocities and Accelerations (y Axis)	3-17
3-11	Gemini 8 Reentry - IGS Measured Sensed Velocities and Accelerations (z Axis)	3-18
3-12	Gemini 8 Reentry - Relative Velocity Magnitude	3-19
3-13	Gemini 8 Reentry - Altitude	3-20
3-14	Gemini 8 Reentry - Altitude (Terminal Phase)	3-21
3-15	Gemini 8 Reentry - Relative Flight Path Angle	3-22
3-16	Gemini 8 Reentry - Relative Flight Path Angle (Terminal Phase)	3-23
4-1	GE Burroughs and Compensated IGS ΔV in Sensed Coordinates	4-6
4-2	GE Burroughs and Compensated IGS $\triangle P$ in Sensed Coordinates	4-7
4-3	GE Final and Compensated IGS $\triangle V$ in Sensed Coordinates	4-8
4-4	GE Final and Compensated IGS $\triangle P$ in Sensed Coordinates	4-9
4-5	MISTRAM I 10 K and Compensated IGS $\triangle V$ in Sensed Coordinates	4- 10
4-6	MISTRAM I 10 K and Compensated IGS $\triangle P$ in Sensed Coordinates	4-11
4-7	MISTRAM I 100K and Compensated IGS $\triangle V$ in Sensed Coordinates	4-12
4-8	MISTRAM I 100K and Compensated IGS $\triangle P$ in Sensed Coordinates	4-13
4-9	MISTRAM II Passive and Compensated IGS $\triangle V$ in Sensed Coordinates	7-14
4-10	MISTRAM II Passive and Compensated IGS $\triangle P$ in Sensed Coordinates	4-15

UNCLASSIFIED

UNCLASSIFIED

3150-6036-R8-000 Page ix

Page

ILLUSTRATIONS(Continued)

4-11	MISTRAM Final BET and Compensated IGS $\triangle V$ in Sensed Coordinates	4-16
4-12	MISTRAM Final BET and Compensated IGS $\triangle P$ in Sensed Coordinates	4-17
4-13	AFETR BET and Compensated IGS △V in Sensed Coordinates	4-18
4-14	AFETR BET and Compensated IGS 2P in Sensed Coordinates	4-19
4-15	TOPS BET and Compensated IGS ΔV in Sensed Coordinates	4-20
4-16	TOPS BET and Compensated IGS $\triangle P$ in Sensed Coordinates	4-21
5-1	Rendezvous Radar Residuals ∆R, Radar Minus TRW Calculated	5-4
5-2	Rendezvous Radar Residuals ∆A, Radar Minus TRW Calculated	5-5
5-3	Rendezvous Radar Residuals ∆E, Radar Minus TRW Calculated	5-6
5-4	Rendezvous Radar Telemetered Relative Range	5-7
5-5	Rendezvous Radar Telemetered Relative Azimuth	5-8
5-6	Rendezvous Radar Telemetered Relative Elevation	5-9
5-7	Rendezvous Radar Residuals ∆R, Radar Minus RTCC Trajectory	5 - 10-
5-8	Rendezvous Radar Residuals ∆A, Radar Minus RTCC Trajectory	5-11
5-9	Rendezvous Radar Residuals ∆E, Radar Minus RTCC Trajectory	5-12

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UNCLASSIFIED

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3150-6036-R8-000 Page xi

Page

TABLES

2-1	Inertial Guidance System Error at SECO + 20 Seconds	2-7
2-2	Gemini 8 Accelerometer Bias Estimation (counts/sec)	2-8
2-3	IGS Error Source Summary	2-9
2-4	IGS Error Source Contribution to Velocity Error at SECO + 20 Seconds	2-10
2-5	Azimuth Update	2-20
3-1	Estimated Impact Summary	3-2
3-2	Reentry Error Source Summary	3-2
3-3	IGS (RTCC) and TRW (ESPOD) Retrofire Conditions	3-5
3-4	Assumed Steady-State Reentry Conditions	3-6
4-1	Tracking Data Errors	4-3
5-1	Ground Tracking Coverage	5-1

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1. INTRODUCTION AND SUMMARY

Gemini Flight No. 8 was launched on 16 March 1966 from Complex 19 at Cape Kennedy, Florida. The major objective accomplished on this flight was rendezvous and docking of the Gemini spacecraft with the Agena target vehicle. This report, submitted to the NASA Manned Spacecraft Center by TRW Systems in response to Task MSC/TRW G-14 of the Mission Trajectory Control Program, presents the results obtained from analysis of the inertial guidance system (IGS) performance during ascent and reentry flight phases and provides a reconstruction of the spacecraft trajectory during ascent and reentry.

The following is a brief summary of the analysis results:

a) The inertial guidance system (IGS) performance during ascent was satisfactory. Best estimates of the IGS errors at SECO +20 seconds are as follows:

$\Delta x = +896 \pm 50 \text{ ft}$	$\Delta \dot{x} = +5.1 \pm 0.5 \text{ ft/sec}$
$\Delta y = -617 \pm 200 \text{ ft}$	$\Delta \dot{y} = -5.3 \pm 2.0 \text{ ft/sec}$
$\Delta z = +985 \pm 100 \text{ ft}$	$\Delta \dot{z} = +11.0 \pm 2.0 \text{ ft/sec}$

b) A set of IGS and tracking system error source coefficients was derived from analysis of the position and velocity comparisons between IGS telemetry and tracking system data. Recovered IGS error sources that contributed significantly to the explanation of the observed differences were:

	Coefficient	Velocity error contribution in IGS coordinates (ft/sec)
<u>x axis</u>		$\Delta \dot{\mathbf{x}}$
X accelerometer scale factor	+199 ±30 ppm	+5.0
<u>y axis</u>		Δÿ
X accelerometer bias	+45.5 ±10 ppm g	-1.1
Z accelerometer bias	+84.1 ±10 ppm g	+0.9
misalignment toward x	+38 ±37 sec	-4. 6



Velocity error contribution in IGS coordinates Coefficient (ft/sec) Δż z axis X gyro spin axis $-1.1 \pm 0.44^{\circ}/hr/g$ +10.6unbalance Z gyro input axis $-0.18 \pm 0.30^{\circ}/hr/g$ -6.3 unbalance IGS azimuth +6.9 $+57 \pm 18 \text{ sec}$ misalignment

c) Significant tracking system bias errors recovered from analysis were:

	C. e. officient	Velocity error contribution in IGS coordinates SECO +20 sec
	Coefficient	(11/ sec)
MISTRAM I		
P 100K bias	-2.2 ± 0.5 ft	$\Delta \dot{y} = +28.5$
Refraction (P 100K)	+2 ±1 ppm	$\Delta \dot{y} = -10$
MISTRAM II		
P bias	+1.5 ±1.0 ft	$\Delta \dot{y} = -2.7$

 $GE \ Mod \ III$

No GE Mod III bias errors were found to be significant relative to the random error in the system. The random error, though nominal, is very large (10-100 ft/sec) late in flight at the lower elevation angles.

 d) A reentry IGS evaluation and trajectory reconstruction is attempted by comparing guidance system output with nominal trajectory characteristics during the terminal phase of descent. No major IGS errors are apparent; however, incorrect initial conditions used in the navigation contributed approximately 10 n mi of downrange miss. No reentry tracking data were available.



e) A comparison between rendezvous radar measurements and calculated values from a TRW reconstruction of the Gemini IX and Agena trajectories shows agreement within 1000 to 4000 feet. Inaccuracies in the trajectory reconstruction appear to be the limiting factor in this attempted onboard radar accuracy analysis.

Sections 2, 3, and Appendix D contain details of the ascent and reentry IGS analysis, while listings of the reconstructed trajectories are contained in Appendixes A and B. An analysis of the quality of the external tracking data obtained during ascent is contained in Section 4, and includes plots of the residuals of each system referenced to the reconstructed trajectory. Section 5 discusses a comparison made between telemetered rendezvous radar measurements and calculated values.

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2. INERTIAL GUIDANCE SYSTEM PERFORMANCE ANALYSIS

Comparisons of IGS telemetered navigation quantities and external tracking data were made for the purpose of evaluating the Gemini 8 IGS performance. The IGS evaluation was based in part on sensed velocity comparisons (Figure 2-1). These were generated by comparing external tracking data adjusted for gravity with the telemetered accelerometer accumulated count appropriately biased and scaled to engineering units. The residuals from these comparisons were attributed to inertial measurement unit (IMU) and tracking system errors.

Comparisons were also made between the telemetered total inertial position and velocity outputs from the airborne computer and external tracking data (Figures 2-2 and 2-3). These comparisons include airborne computer navigation errors caused by IMU position error feedback into the gravity calculation, gravity approximations, truncation errors, etc., as well as IMU and tracking errors. The difference between the sensed and inertial comparison sets, called delta-delta comparisons (Figure 2-4), provide a measure of the airborne computer computational error alone.

The sensed, inertial, and delta-delta comparisons are plotted in the IGS Computer Coordinate System, which is an inertial, orthogonal, righthanded system referenced to the center of the earth. The x and z axes lie in a plane parallel to the geodetic tangent plane at the launch site at platform release time, with the x axis nominally defined by the launch azimuth (actually by the misaligned azimuth), positive downrange. The y axis is positive down along the geodetic vertical, and the z axis is directed to complete the right-handed x, y, z set.

Position and velocity comparisons were also made in the external tracking measurement coordinates for the purpose of isolating IMU and tracker error coefficients by performing a statistical regression analysis on the difference. External tracking data used in the evaluation included Quick Look MISTRAM I 10K and 100K, GE Mod III Burroughs (2 per second), final MISTRAM, passive MISTRAM II, and AFETR BET. An analysis of these data sources is described in Section 4. Unless otherwise noted, the plots enclosed are referenced to liftoff time (16:41:02.389 GMT) which occurred 3.303 seconds after IGS "platform release."





Figure 2-1. GE/Final and 100K MISTRAM $\triangle V$ Sensed Coordinates











Figure 2-3. GE/Final and 100K MISTRAM △P Guidance Inertial Coordinates



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	Page 2-5	
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Figure 2-4. Navigation Velocity Error





2.1 TOTAL IGS ERROR

The IGS error at SECO +20 seconds determined from analysis of position and velocity comparisons is presented in Table 2-1. The column headed "IMU Error" represents the error contributed by the accelerometer, gyro, and platform initial alignment sources. The column headed "Navigation Equation Error" represents the contributions due to various approximations within the airborne computer. The columns headed "Total IGS Error" represent the composite of IMU and navigation equation errors.

Table 2-1(a) gives the IGS error based on the analysis of the ascent (MISTRAM and Mod III) tracking data. Table 2-1(b) lists the total error derived from the TRW reconstruction of the Revolution 1 free-flight trajectory propagated back to the time of ascent telemetry data. This reconstruction is based on the data from the Gemini network of radar tracking sites and is completely independent of the "ascent" tracking data (see Reference 1). The good agreement between the "Total IGS Error, " indicated in Table 2-1(a and b), therefore gives considerable confidence in the error assignment. The total IGS error reported in the NASA 30-Day Report is given in Table 2-1(c) for reference. The IGS error magnitudes indicated in Table 2-1 give the following "trajectory" referenced errors:

Velocity magnitude error	= +4.1 ft/sec
Flight path angle error	= +0.015°
Out-of-plane velocity error	= +11.0 ft/sec

2.2 IMU ERROR

Analyses to recover inertial measurement unit (IMU) error source coefficients were performed by using procedures and data processing programs as documented in Reference ². The error source recovery was accomplished in the following manner:

- a) Accelerometer bias errors were determined from the slopes of the IGS sensed velocities during an interval of orbit flight when no thrusting was being applied.
- b) A regression analysis in the tracking data velocity domain was performed on the IGS/tracker residuals after compensating for the previously determined accelerometer bias errors.





	(a)			(b)	(c)
Para- meter	TRW Ascent Data Analysis			TRW Orbit 1 Recon- struction	NASA 30- Day Report
	IMU Error	Navigation Equation Error	Total IGS Error	Total IGS Error	Total IGS Error
x	+5.2 ±0.5	-0.13 ±0.2	+5.1 ±0.5	+5.4 ±1.	+5.0±1.
ÿ	-4.9 ± 2.0	-0.39 ± 0.1	-5.3 ± 2.0	-3.2 ±1.	-4.9 ±2.
ż	$+11.4 \pm 2.0$	-0.38 ± 0.1	11.0 ± 2.0	$+11.1 \pm 2.$	$+11.4 \pm 2.$
x	+872. ±50.	+24. ±10.	+896. ±51.	+813. ±100.	+920. ±100.
у	-564. ±200.	-53. ±5.	$-617. \pm 200.$	$-786. \pm 100.$	$+120. \pm 100.$
Z	+1000. +100.	-15 ±5.	+985. ±100.	+1021 .±200 .	+1015. ±200.

Table 2-1. Inertial Guidance System Error at SECO + 20 Seconds

2.2.1 Accelerometer Bias Determination

The accelerometer biases are determined prelaunch by calibration, and the ascent acceleror ar output is compensated for these predetermined estimates. How ever, the free-flight intervals of orbital flight offer an ideal test situation to recalibrate these biases. This test is carried out in real-time, and the co. ater bias constants are updated during orbit if they appear to be significantly different from the preflight values. Various segments of orbit IGS telemetry data are available to TRW, and a postflight determination of accelerometer bias is also made. Table 2-2 summarizes the various bias determinations. The difference between the TRW postflight value and the preflight value inserted into the IGS computer during ascent is listed in parts-per-million of gravity as an ascent IMU error in Table 2-3. A history of the prelaunch calibration values for bias is plotted in Appendix C.

X-Bias (counts/sec)	Y-Bias (counts/sec)	Z-Bias (counts/sec)	Source	Time of Measurement_
1. 02997567	0.16331029	-0.09914397	Preflight calibration, ascent com- puter com- pensation	Prelaunch
1.040	0.163	-0.070	In-orbit up- date	Revolution 1
1.0446	0.1599	-0.0720	Postflight determination (TRW)	Revolution 4

Table 2-2. Gemini 8 Accelerometer Bias Estimation

2.2.2 Error Source Regression Results

The identification of individual error sources, in addition to accelerometer bias, was attempted mainly by a statistical error source regression, i. e., by a weighed least-square-fit of the probable IGS and tracker error sources to the (bias compensated) IGS/tracker differences. The regression was made in the coordinates of the external tracking systems and involved a simultaneous solution for IGS, MISTRAM I and II, and GE Mod III errors. A discussion of the regression technique and more details on various computer runs, problems, and limitations in the analysis are contained in Appendix D. The results of the IGS error source analysis are summarized in Tables 2-3 and 2-4. The tables also include the NASA/Honeywell preflight error source estimates as well as the postflight estimates included in the NASA 30-Day Report. The external tracker error source recovery results are presented in Table 4-1 of Section 4.

Table 2-3 lists the IGS error source magnitudes, and Table 2-4 lists their contributions to the total IGS error at SECO +20 seconds. The error sources are grouped primarily as to the type of error source and to a lesser extent in accordance with the velocity error propagation correlation among them.







						<u> </u>	
			TRW a	analysis	Preflight measured	NASA	
	Error source	Units	Recovered coefficient	Uncertainty (2)	coefficient (NASA/ Honeywell)	30-day report	
I	Accelerometer						
	X accelerometer bias Y accelerometer bias Z accelerometer bias X accelerometer scale	ppm g ppm g ppm g	+45.5 -10.5 +84.1	10. 10. 10.	+10.9 +45. -69.	+ 44 . +10. -100.	
	factor Z accelerometer scale	ppm	+200.0	30.	-80.	+200.	
	factor Z accoloromator mis	ppm	-58.	157.	+31.4	-150.	
	alignment toward X	sec	-38.	37.	-7.8	-30.	
11	Pitch drift						
	Y gyro constant drift rate	°/hr	(1)	-	-0.043	-0.1	
	unbalance	⁰ /hr/g	+0.002	0, 30	-0,029	+0.12	
ш	Roll and azimuth drift						
	X gyro constant drift rate	°/hr	(1)	-	+0.085	+0, 08	
	rate	⁰ /hr	(1)	-	-0, 107		
	X gyro input axis unbalance	⁰ /hr/g	(1)	-	-0. 221	-0.22	
	Z gyro input axis unbalance	⁰ /hr/g	-0, 18	0.30	+0.079	+0. 08	
	X gyro spin axis unbalance	⁰ /hr/g	-1.1	0. 44	-0. 41	-0. 72	
	Z gyro spin axis unbalance	⁰ /hr/g	(1)	-	-0.06	+0.1	
IV	System						
	Platform azimuth misalignment IGS time correlation IGS time scale factor	sec sec ppm	+57. +0. 025 -90.	18. 0.006 20.		+43. +0. 029 -100.	

e Summary

(1)Not included in the statistical regression error model because of high correlation with other terms.

(2) Uncertainties are 1-sigma estimates.



Table 2-4. IGS Error Source Contribution to Velocity Error at SECO +20 Seconds

Error source		TRW analysis		Preflight measured (NASA/Honeywell)		NASA 30-day report				
		ż	Ý	ż	ż	Ý	ż	ż	Ý	ż
I	Accelerometer X accelerometer bias Y accelerometer bias Z accelerometer bias	+0.18	-1. 1 +0. 93	+0. 16	+0.05	-0. 27 -0. 80	-0.7	+0. 18	-1.1	-0.1
	X accelerometer scale factor Z accelerometer scale factor Z accelerometer misalignment toward X	+4.97	+0. 40		-2.0	-0.21 -0.94		+4. 9	+1.0 -3.6	
	Total I	+5.15	-4.32	+0,16	-1.95	-2.22	-0.7	+5.08	-4.8	-0.1
II	Pitch drift									
	rate Y gyro input axis				-0.04	-1.15		-0.1	-2.7	
	unbalance		+0.06		+0.10	+0.77		+0.1	+3.2	
	lotal II		+0.06		+0.06	-0.38		+0.0	+0.5	
III	Roll and azimuth drift									
	X gyro constant drift rate Z gyro constant drift				-0.01	+0.01	-0,85			-0.8
	rate X gyro input axis				+0.02	0	-1.47			
	unbalance Z gyro input axis				+0.02	+0.02	+2.80	+0.1		-2.7
	unbalance X gyro spin axis	+0.09		-6.26	-0.04	0	+2.75			+2.7
	unbalance Z gyro spin axis	-0.06	-0.60	+10.60	-0.02	-0.20	+3.95		-0.2	+6.7
	unbalance						+0.47			+0.8
	Total III	+0.03	-0.60	+4.34	-0.03	-0.17	+7.65	+0.1	-0.2	+6.7
IV	System									
	IGS azimuth misalignment IGS time correlation IGS time scale factor			+6.85						+5.2
	Total IV			+6.85						+5.2
Tota	l I+II+III+IV	+5.18	-4.86	+11.35	-1.93	-2.77	+6.95	+5.2	-4.5	+11.8
	Navigation	<u>-0.13</u>	-0.39	-0.38				<u>-0.2</u>	<u>-0.4</u>	<u>-0.4</u>
	Total IGS	+5.05	-5.25	+10.97				+5.0	-4.9	+11.4



It must be emphasized at the outset that the complete separation of possible IMU and tracker error sources by analysis of the postflight IGS/ tracker position and velocity comparison residuals is impossible. There is simply insufficient information in the comparison to differentiate among the great number of probable sources. In other words, there is too high a correlation or similarity among large groups of possible error sources to pick out the individual contribution of each error source. Various substitute procedures can be attempted, and the one general approach used in this analysis is to limit the regression error model to only one or two representative and probable error sources within each correlated group and solve for these. The coefficient recovered in the regression for this "representative" error source is in effect an equivalent coefficient standing for some linear combination of all the possible errors in the correlated group. The net effect then is that a unique separation of error sources is not possible or to be implied from the analysis included here. What is provided is a "statistically reasonable" explanation of the observed differences and an indication of the kind of error source that is causing a trajectory position and velocity measurement error on the flight.

There are some error sources, of course, that can be identified with much better confidence than others, e.g., X accelerometer scale factor error, because of their lack of similarity to other error terms or because of preferred directional propagation with respect to the external tracking system. Another most important aspect of the analysis is that, for the most part, this problem with correlation among error sources does <u>not</u> affect the assignment of total guidance system error (Section 2.1). Therefore, there is a large uncertainty as to what some of the individual error source coefficients are, but not in their net effect. There is accuracy of 0.5 to 2 ft/sec (depending on coordinate and time) in the specification of IGS error propagation as a result of analysis of the redundant tracking data. Whatever the proposed error solution, it must give an explanation of the observed differences to within these accuracies throughout the flight.

2.2.3 Discussion of Error Analysis

The dominant recovered errors that explain the x axis residuals are the IGS time correlation and scale factor errors and the X accelerometer scale factor error (see Tables 2-3 and 2-4). The X scale factor error of approximately 200 ppm is the cause of the main trend



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in the x axis residual and amounts to 5 ft/sec error at SECO + 20 seconds (see Figure 2-1). The velocity residuals resulting from timing errors are directly proportional to acceleration and are evidenced by -1.3 and +1.2 ft/sec jumps in the x velocity residuals at 160 and 337 seconds, respectively, corresponding to the abrupt acceleration changes at BECO and SECO. Although the timing errors cause no explicit IMU velocity error after SECO, these errors do cause approximately 1 ft/sec of IGS gravity integration error at burnout and position errors equal to the integral of the velocity error. The propagations of these major x axis error contributors are shown as dashed curves in Figure 2-5. Their combined effect, along with the effect of other minor error sources, is shown as a solid line on this plot.

The Z accelerometer scale factor and misalignment and the IGS timing errors could account for the major portion of the y axis trend. These error source propagations are shown in Figure 2-6. The X accelerometer bias error, which results in an initial misalignment about the Y accelerometer axis, and the Z accelerometer bias error both have contributions to the y axis residual, but their velocity errors propagate with opposite sign so as to nearly cancel their net effect.

Figure 2-1 shows that there is good agreement between MISTRAM and GE Mod III tracking data in the crossrange, z, direction and indicates an IGS error of 11 to 12 ft/sec. Also note that there is a residual error of 1.6 ft/sec at 140 seconds, which is the time the GE Burroughs/IGS update should zero out the cross-range IGS velocity error. This inexact update, which appears due to an approximation in the Burroughs computer, results in an equivalent 50-60 arc seconds IGS azimuth misalignment and accounts for approximately one-half the \dot{z} burnout error. The remaining z error is accounted for in the regression by the Z gyro and X gyro gdependent drift rate terms (see Tables 2-3 and 2-4). All the X and Z gyro drift terms as well as azimuth alignment contribute to the z axis residual in a highly correlated manner such that the regression is severely limited in its error source discrimination. This fact is mathematically represented in the large uncertainty associated with the recovered X and Z gyro drift error sources (see Table 2-3). However, from an analysis of all the regression runs (see Appendix D), and as further indicated by the preflight



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Differences - x Axis Figure 2-5.

3150-6036-R8-000 Page 2-13



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Figure 2-6. IGS Error Source Contribution to Sensed Velocity Differences - y Axis

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calibration data, there appears to be a good reason to suspect a large X gyro spin axis unbalance drift error source. The velocity error propagation of each significant recovered error source is shown in Figure 2-7.

The net fit associated with all the recovered IGS error coefficients listed in Table 2-3 is shown as an overplot on the IGS/tracker differences in Figure 2-8. It is evident that the postulated IGS errors do not provide a satisfactory explanation of the y axis MISTRAM residuals, which show an increasing deviation from the fit-curve and the Mod III data starting at BECO and continuing beyond SECO. A MISTRAM P bias of 2.2 feet and P 100K refraction error of two parts per million in the index of refraction (2 n units) were recovered from the error analysis of the tracking data (see Section 4). Combining these errors with the recovered IGS errors provides an explanation of both the MISTRAM and Mod III residuals to within 0.5 to 1 ft/sec throughout flight in all coordinates.

2.2.4 Preflight Measurement of IMU Errors

A set of preflight-measured IMU error source coefficients obtained from NASA/Honeywell are also presented in Tables 2-3 and 2-4. Figure 2-9 illustrates the velocity error propagation curve associated with these coefficients. It is observed that the preflight error estimates (adjusted for the incorrect azimuth update) provide an explanation of the y and z axis residuals to within a few feet per second throughout flight. This is considered a reasonably good flight verification of the preflight estimates. However, the x residual is poorly compensated by the preflight estimate. The difference of approximately 8 ft/sec in burnout error is most likely due to a change from the preflight calibration of the X accelerometer scale factor and amounts to a 300-parts per million error. A time history of calibration values for gyro drifts and accelerometer bias and scale factor is presented in Appendix C.





Differences - z Axis Figure

3150-6036-R8-000 Page 2-16



Figure 2-8. Sensed Coordinates △V With Recovered IMU Error Source Fit





Figure 2-9. Sensed Coordinate ΔV With Preflight Measured Error Source Fit



2.3 AZIMUTH UPDATE

An IGS azimuth correction is calculated at three separate times by the onboard computer. On the first pass through the navigation equations after platform release, the roll gimbal angle reading is compared to the desired value, and the difference is used as a correction to the intended flight azimuth. This correction is called $\Delta \eta_x$, where a positive value implies that the platform is rotated clockwise from the desired azimuth.

Additional azimuth corrections are made during flight at 100 and 140 seconds after liftoff. These are calculated by comparing the crossrange (z direction) velocity, as measured by GE/Burroughs, with that derived from the airborne system and attributing the residual to an IGS azimuth misalignment. The calculated updates were telemetered on the Gemini 8 mission for the first time and are presented in Table 2-5. The update values determined during the postflight data analysis are also presented as determined by the following methods:

- a) Calculated from the telemetry data, and simulating the in-flight calculations
- b) Calculated from the jumps in the inertial velocity comparisons and the delta-delta curve



Table 2-5. Azimuth Update

		Postflight d	,		
Time (sec from liftoff)	Onboard computer	Flight calculation simulation	Delta-delta	Units	
0	+0.0018382	+0.001942	+0.001942	rad	
100	-0.0014965	-0.001009	-0.001402	rad	
140	-0.0001249	-0.000733	-0.000135	rad	
TOTAL	-0.0016214	-0.001742	-0.001537	rad	
(100 and 140)	-0.092899	-0.0998	-0.08806	deg	

The values indicated at 100 seconds include those at 0 seconds. The postflight value for 0 seconds was determined from an observable jump in the IGS z velocity after platform release. This jump corresponds to the first IGS correction. The telemetered total azimuth correction of -0.0929° has been included in all plots contained in this report. This is the smallest correction required of all the Gemini flights. A brief history of updates follows.

Flight Number	Azimuth Update (deg)	Mean Value	NASA/Honeywell Specification
2	-0.29		
5 4	-0.12		
5	-0.27	-0.033	±0.75
6	-0.53		
7	-0.48		
8	- 0. 09		

2.4 REFERENCE ASCENT TRAJECTORY

Appendix A contains a reconstruction of the ascent trajectory generated by correcting IGS output for those recovered errors listed in Table 2-3. The trajectory is provided in Cartesian earth-centered inertial coordinates and in earth-referenced coordinates. A plot of the sensed acceleration obtained by differentiation of the IGS accelerometer output is also included.



3. REENTRY IGS EVALUATION

There was no post retrofire tracking data available for direct comparison with IGS output during reentry. However, a trajectory reconstruction using ground tracking data during the two orbits preceding retrofire has permitted an accurate estimate of reentry initial conditions, and a span of IGS data beyond main chute deployment makes possible an evaluation of IGS platform misalignment.

Table 3-1 presents a summary of spacecraft impact measured by the IGS, the recovery ship, the sighting aircraft, and the TRW postflight reconstruction. The same information is displayed in Figure 3-1. The large crossrange motion of the telemetered IGS ground trace is due to one of the obvious IGS errors recovered in the TRW analysis. The best estimate of total IGS error at drogue chute deployment is:

- 7.6 ± 1 n mi right
- 8.1 \pm 1 n mi long
- 3.7 ± 1 n mi low

As seen in Table 3-2, which summarizes recovered error sources and their effects, most of the downrange error is attributable to the error in initial conditions, the altitude error is primarily due to IGS platform pitch misalignment, and the crossrange error is caused by both roll and azimuth misalignments. Figure 3-2, which presents a plot of ground traces of the uncorrected IGS trajectory, the IGS trajectory with initial conditions corrected, and the IGS trajectory with both initial conditions and misalignments corrected, provides an indication of the contribution of the various errors.

3.1 INITIAL CONDITIONS

Table 3-3 presents the retrofire state vector from the Real-Time Computer Complex (RTCC) used by the IGS for reentry initialization and the retrofire state vector recovered by the TRW orbital reconstruction program (ESPOD)(see Reference 1). It is also shown that the difference is primarily due to inaccuracies in the RTCC vector. To obtain retrofire conditions, this RTCC vector was propagated through approximately two orbits from the Hawaii 05 differential correction; ESPOD, on the

		·			
Description		Latitude (deg)	Longitude (deg)	Crossrange miss distance (n mi)	Downrange miss distance (n mi)
Intended target		+25.25	+136.0		
Ship pickup		+25.37	+135.93	+6.18	-5.28
Aircraft sight.		+25.23	+135.90	-2.36	-5.0
Telemetered IGS [*]	Drogue chute	+25.19	+136.081	-2. 59	+3.27
	Main chute	+25.10	+136.094	-7.5	+6.9
	Final point ~8000 ft	+24.97	+136.031	-16.01	+5.34
	Drogue chute	+25.349	+135.941	+4.99	-4.86
TRW Trajectory Reconstruction	Main chute	+25.352	+135.967	+5.58	-3.09
	Final point ~8000 ft	+25.349	+135.973	+5.47	-2.73

Table 3-1. Estimated Impact Summary

The "drogue chute" impact estimate should be used for IGS accuracy evaluation, since IGS guidance capability essentially ends at this time.

Note: A positive value indicates, respectively, North latitude, East longitude, a long downrange miss, or a crossrange miss to the left of the intended target.

Table 3-2. Reentry Error Source Summary

Emma 2	Recovered error	Position error at drogue			
LFFOF Source	(sec)	Downrange (ft)	Crossrange (ft)	Up (ft)	
Initial conditions	*	54000	-4000	-8000	
Platform misalignment			······		
About X accelero- meter axis	-1565 <u>+</u> 300	-4000	-19000	-300	
About Y accelero- meter axis	-1325 ± 100	+2500	-4000	-20000	
About Z accelero - meter axis	-2220 ± 300	-3000	-14000	+500	

*See differences in Table 3-3.

** The \pm numbers are 1 σ estimates.

Note: The position error values listed here are only approximate. Other, less significant errors were caused by those sources found during the ascent analysis which were also assumed present during reentry.



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Figure 3-1. Map of Estimated Impact Points




Figure 3-2. Effects of Initial Condition and IMU Corrections Upon IGS Trajectory



other hand, used all available data including the Ascension 07 radar pass, which occurred less than 8 minutes before retrofire. Moreover, the RTCC Ascension 07 fit agrees closely with the ESPOD fit. The coordinate system of the state vector shown in Table 3-3 is ECI with x through Greenwich at $0^{\rm h}$ day of launch.

	IGS vector	TRW vector	Difference: IGS - TRW			
x	+10,094,700 ft	+10,131,910 ft	-37,210 ft			
Y	+19,407,000 ft	+19,393,020 ft	+13,980 ft			
Z	-317,700 ft	-338,502 ft	+20,802 ft			
x	-19,638.0 ft/sec	-19,609.7 ft/sec	-28.3 ft/sec			
Ŷ	+10,417.8 ft/sec	+10,461.0 ft/sec	-43.2 ft/sec			
ż	+12, 259.8 ft/sec	+12,259.7 ft/sec	+0.1 ft/sec			

Table 3-3. IGS (RTCC) and TRW (ESPOD) Retrofire Conditions*

*Time = $1^d 2^h 45^m 49^s$ from 0^h day of launch

3.2 PLATFORM MISALIGNMENT

An accurate set of trajectory measurements against which the IGS may be calibrated is necessary for recovery of IGS error sources. On Gemini 8, this condition was partially met by the extension of IGS data into the lower atmosphere where the main chute was deployed. Due to the lack of conventional trajectory measurements during main chute descent, nominal steady-state conditions were used for comparison with IGS indicated values. These are listed in Table 3-4. The assumption of nominal conditions was primarily based upon postflight reporting that a smooth Gemini 8 splash-down occurred. Nevertheless, had the actual main chute velocity been as large as twice nominal, the assumption would have been approximately five times more accurate than the IGS indicated value.

Event	Time from retrofire (sec)	Altitude (ft)	Velocity crossrange	Velocity downrange	Velocity vertical (ft/sec)
Drogue chute	1909	50,000	0	*	*
Main chute	2005	10,000	0	*	*
Main chute plus 2.37 minutes	2147	*	0	0	-32

Table 3-	4. Assume	l Steady-State	Reentry	y Conditions
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*No assumption made

As noted, asterisks in Table 3-4 indicate no assumption was made for the given quantity. In fact, the three velocity components at the final point and the zero crossrange velocity at 50,000 feet were used to compute the misalignments, and the other values were used only to check the reasonableness of the resulting trajectory. The final horizontal components of velocity could be in error by tens of feet per second due to surface winds at reentry, but this is small compared to the nearly 400 ft/sec indicated IGS horizontal velocity that was probably due to platform misalignment.

The error model used to fit the observed velocity differences consisted of only platform alignment errors for the following reasons:

- a) No other error source could supply a significant portion of the observed error without being grossly out of tolerance.
- b) Nominal IGS performance was seen during the ascent flight, which was only 10 hours before reentry.
- c) The recovered misalignments are all of reasonable size relative to expected values.

Although their effect was relatively small on the reentry error, the ascent-recovered IMU errors were also removed from the IGS indicated reentry trajectory.

3.3 SIMULATION RESULTS

3.3.1 MSC Simulation

Two point-mass reentry simulation runs were made by MSC, one using the same retrofire state vector as the IGS and the other the retrofire state vector recovered by the TRW orbital trajectory reconstruction. The simulation impacts were then compared with the two trajectory impacts formed by integrating the IGS accelerometer data from each of the retrofire state vectors, as was done in the TRW reentry reconstruction. The position difference between the two impact points was of the same magnitude in simulation and integration of IGS, but of opposite direction (see diagram below).



The explanation of this somewhat unexpected result is that, in simulation, drag acceleration is a function of computed altitude and depends directly upon initial conditions. On the other hand, in integration of IGS data, drag acceleration is given by accelerometer output and is independent of both computed altitude and initial conditions. Note that the actual reentry navigation and guidance encompasses use of IGS data for navigation and simulation results for guidance from the indicated position to the intended target. There is, therefore, a complicated tradeoff among initial condition error, navigation error, and resulting guidance or



steering errors. It was beyond the scope of this analysis to demonstrate how each of these add together to give an effective total system miss from the intended target.

3.3.2 McDonnell 6-Degree-of-Freedom Simulation

The position and velocity differences between the McDonnell simulation and the TRW reconstruction of reentry are presented in Figures 3-3 through 3-5. These plots appear in IGS coordinates.

The differences are large primarily because the McDonnell simulation begins with the RTCC retrofire state vector used by the IGS rather than the updated one used by TRW. The in-plane differences observed (x and y) are consistent with the differences in initial conditions and their resulting propagation through reentry in a strictly simulation sense. That is, from the MSC point-mass results, it is expected that a simulation using IGS initial conditions will impact approximately 10 miles short of the same simulation using the TRW initial conditions. Actually the position error indicated at the end of the comparison (Figures 3-3 through 3-5), which corresponds to an altitude of 80,000 feet, is about 20 miles short of the TRW reconstruction at that point. The additional error may be due to what amounts to an effective timing error between the two trajectories near the end (the velocity difference has not get gone to zero, and the position error is getting smaller). It is also expected that there is some true simulation error in addition to the initial condition error, and this error will also appear in this comparison.

The peak crossrange error at 1800 seconds (see the plot of delta z in Figure 3-5) may also be partly due to the different crossrange acceleration profile resulting from the incorrect initial altitude. Due to the TRW analysis uncertainty in dividing main chute crossrange velocity error between IGS platform yaw and roll alignment error, it is believed that not more than 50 percent of this error is also in the TRW reconstruction.

3.4 REFERENCE REENTRY TRAJECTORY

The reentry trajectory was reconstructed by integrating the equations of motion using corrected IGS measurement of sensed velocity and the TRW estimate of the initial conditions. The corrections applied to the IGS output were for the ascent recovered IGS errors defined in Section 2



and for the initial platform misalignment errors recovered during the reentry phase evaluation. Plots of spacecraft sensed velocity and acceleration, relative velocity magnitude, flight path angle, and altitude follow (see Figures 3-6 through 3-16).

Appendix B contains a complete listing of the reentry trajectory reconstruction in an earth-referenced coordinate system.



























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Figure 3-9. Gemini 8 Reentry--IGS Measured Sensed Velocities and Accelerations (x Axis)

3150-6036-R8-000 Page 3-16



3150-6036 Page 3-17



and Accelerations (z Axis)



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Figure 3-13. Gemini 8 Reentry-Altitude

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3150-6036-R8-000 Page 3-20

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Figure 3-14. Gemini 8 Reentry-Altitude (Terminal Phase)

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Figure 3-15. Gemini 8 Reentry-Relative Flight Path Angle

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3150-6036-R8-000 Page 3-23

CONTROLLES.

4. TRACKING SYSTEM PERFORMANCE

Tracking data available for analysis of the Gemini 8 IGS performance included the following:

- a) GE Mod III/Burroughs (TRW-processed)
- b) GE Mod III/Burroughs (GE-processed)
- c) MISTRAM I Quick Look 10K and 100K
- d) MISTRAM II (passive mode)
- e) AFETR MISTRAM-only BET
- f) AFETR final BET

Each of the above sets was used for position and velocity comparisons, as described in Section 2. The TRW-processed GE Mod III/Burroughs data were used for quick look analyses; however, detailed analyses were subsequently accomplished with the remaining sources. A TRW program (TOPS), which is used to produce powered flights best estimates of trajectory (BET), was also used to aid in the tracking data analysis. The results of the ensemble IMU/tracking system analysis accomplished on this flight are presented in Table 4-1. Also presented are error sources obtained by AFETR, GLAD, and BET programs.

For a clear picture of what portion of the observed differences are considered a tracking error, tracking system data were compared with inertial guidance data that had been corrected for guidance system errors derived from the regression analysis results of Section 2.

In general, the most significant tracking system error was an approximate 2-foot bias in the MISTRAM I 100K P channel measurements (because of forced internal consistency, there was about 0.2-foot bias also in the 10K P channel). The GE Mod III system performance was nominal, as was the performance of the MISTRAM II system. The AFETR MISTRAMonly BET agreed well with the final TRW trajectory, while the AFETR final BET contained a small difference in the vertical direction, amounting to about 3 ft/sec at SECO.





4.1 GE MOD III

Page 4-2

4.1.1 GE Mod III/Burroughs (TRW-Processed)

The Burroughs data received at TRW consisted of raw counts recorded on punched paper tape at a rate of two samples per second. The data were transferred to magnetic tape at TRW and processed in the data reduction programs.

Figures 4-1 and 4-2 show GE/Burroughs (TRW)-compensated IGS comparisons in guidance coordinates. No major errors are evident, and differences are within the uncertainties of both the GE system and the compensated IGS data (see Section 2). The regression analyses using the GE-processed Burrant data (Section 4, 1, 2) resulted in estimated azimuth and elevation biases of -0.000015 radian and -0.00005 radian, respectively, and a range bias of about -75 feet, all of which are nominal values for the GE Burrough tracker measurements. The analysis, including the GE rate $(\dot{r}, \dot{p}, \dot{q})$ measurements (Section 2), showed some remaining residual errors in these data, although their level was generally within the expected uncertainties.

4.1.2 GE Mod III/Burroughs (GE-Processed)

The General Electric Company processes essentially the same two per second Burroughs data which are transmitted to Syracuse in near real-time via hardwire. The primary differences between the two processing techniques (TRW and GE) are the amount of filtering applied to the data and the method of correcting for refraction effects.

Figures 4-3 and 4-4 show the GE-processed Burroughs datacompensated IGS comparisons. Comparison with Figure 3-3 clearly shows the heavier degree of filtering in the GE-processed data. These results disagree with the TRW data (Figure 4-1) in the y direction by approximately 1.5 ft/sec at SECO because of differences in refraction corrections applied.

4.2 MISTRAM

The MISTRAM data received at TRW are fully scaled and corrected raw range sum, P, and Q measurements. These data were processed through the TRW transformation and comparison programs in the usual manner.



			TRW analy	sis	AFETR only	MISTRAM- BET	AFETR	iinal BET
Syat	em error	Units	Estimated bias ı	ار incertainty	Estimated blas	lσ uncertainty	Estimated bias	ار uncertainty
	RSUM	ft	-r-	6.0	+0.68	0.76	-3, 9	0.4
	P 10K	ft	+0.19 (post-BECO)	0.05	+0.21	0,006	+0.10	0.005
	Q 10K	ŧ	0.0 (post-BECO)	0, 05	+0.08	0.007	-0.036	0,006
	P 100K	ţţ	+2.2 (post-BECO)	0.5	+2.46	0.06	+1.2	0.05
MISTRAM I	A 100K	ft	+0.06 (post-BECO)	0.5	+0.81	0.07	-0.50	0.06
	Refraction (central site)	n-units	- 1, 71	3, 3				
	Refraction (P 100K)	n-units	+2	1.				
	f rsum	ft	+2	5.	-0,09	0.4	-1, 13	0.4
	Д	ţţ	+1.5	1.	2.15	0.1	+0.095	0, 1
	α	ft	+0.5	0.5	1.08	0.04	+0.651	0.04
MISTRAM II	ksum	ft/sec	+0.22	0.1	0,002		+0,005	0.002
	Refraction	n-units	-3,2	ч.				
	(Timing	Sec	-0,00088	0, 002				
	(R	ft	- 74. 3	12.				
	Υ	millirad	-0.015	0.010				
GE Mod III	ы	millirad	-0.050	0.020				
	Refraction	n-units	- 15. 3	З,				
	Timing	sec	+0°0	0.0004				
 TRW resu AFETR M AFETR Fi 	lts obtained fron ISTRAM only BE inal BET results	n regress 3T results from Ref	ion and TOPS analysi i from Reference 3 cerence 4	œ				

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Table 4-1. Tracking Data Errors

3150-6036-R8-000 Page 4-3

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4.2.1 MISTRAM I

Figures 4-5 through 4-8 show the MISTRAM I 10K and 100K-compensated IGS comparisons.

Except for noise levels, these results agree with each other because of forced internal consistency between the 10K and 100K systems. The primary error found to be present in MISTRAM (Section 4.3 and 4.4) was an approximate +2-foot bias and 2 n-unit refraction error in the P 100 channel, the effect of which is most noticeable in the IGS y (vertical) coordinate (Figure 4-7) where a positive trend culminating in about +16 ft/sec at SECO +20 seconds is apparent. This P bias error also propagates somewhat into the x and z coordinates, although at a greatly reduced level. Subsequent analyses by AFETR (Section 4.3) and TRW (Section 4.4) indicated that there were no other significant errors in the MISTRAM I measurements.

4.2.2 MISTRAM II (Passive Mode)

Figures 4-9 and 4-10 show the MISTRAM II-compensated IGS comparisons in IGS coordinates. These results in general represent the best performance of MISTRAM II observed thus far in the Gemini series. Except for an initially high noise level due to the low elevation angle at acquisition, these differences agree quite well with those of the BET analyses (Sections 4.3 and 4.4). These same analyses showed no large errors in the MISTRAM II measurements. This fact, coupled with the improved geometry of the Gemini 8 trajectory relative to MISTRAM II, resulted in the overall good performance of this system for this flight.

4.3 AFETR BEST ESTIMATE OF TRAJECTORY

4.3.1 MISTRAM-Only BET

The MISTRAM-only BET is computed by means of the AFETR "GLAD" program using MISTRAM I (10K and 100K) and MISTRAM II measurements. The solution is obtained from a conventional least-square adjustment of measurement biases and Cartesian trajectory values. A rate bias term is included in the MISTRAM II (passive) range sum error model. No refraction terms are solved for.

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3150-6036-R8-000 Page 4-5

Figures 4-11 and 4-12 show the final MISTRAM BET-compensated IGS comparisons. These differences imply that the GLAD trajectory adjustment agrees well with the results of the IGS regression of Section 2. The biases estimated by GLAD were +2.46 feet for MISTRAM I P 100 (0.21 for P 10), +0.81 foot for Q 100 (0.08 for Q 10), +2.15 feet for MISTRAM II P, and +1.08 feet for MISTRAM II Q. Range sum estimated biases were 0.68 foot for MISTRAM I and -0.09 foot for MISTRAM II. These values also agree well with those estimated by the TRW TOPS analysis (Section 4.4).

4.3.2 Final BET

The AFETR final BET is a conventional weighted least-square adjustment using measurements from MISTRAM, GE, FPQ-6 radars, and x-band GLOTRAC stations.

Figures 4-13 and 4-14 show the final BET-compensated IGS comparisons. The most significant difference is the trend in the y coordinate, which implies that the BET incorrectly estimated tracker bias errors by an amount sufficient to cause about 3 ft/sec vertical velocity error at SECO. For example, this is reflected in the final BET's estimate of MISTRAM I P100 bias, which was +1.2 feet, a figure low about 1 foot (Section 4.4 and 4.4.1). This same type of final BET error was noted during the analysis of the Gemini 6 IGS.

4.4 TRW TOPS BET

Input to the TRW TOPS program consisted of MISTRAM I and II and GE Mod III (track and rate) measurements. Figures 4-15 and 4-16 show the TOPS-compensated IGS comparisons. These results generally agree with those of the preceding analyses and help to verify the estimates of guidance system errors. In terms of MISTRAM I 100K, the TOPS estimates of P and Q biases at SECO were approximately +2.1 and +0.12 feet, respectively. Estimated range sum bias was approximately -5 feet. A 2 n-unit P 100K refraction error was also estimated in the TOPS analysis. Estimated errors for the MISTRAM II and GE Mod III systems were nominal and agreed well with the regression results of Section 2.



Figure 4-1. GE Burroughs and Compensated IGS △V in Sensed Coordinates

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	Page 4-1
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如此的思想是我们的人,我们就是我们的人们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是 我们就是我们就是我们就是我们我们就是我们就是我们就是我们就是我们就是我们的人,我们就是我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是你们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,我们	, 또, 많은 것은 것을 많은 것을 다 가 가 다 가 가 가 가 다 가 가 다 가 다 가 가 다 다 가 가 다 다 가 다 다 가 다 다 다 가 다 다 다 가 다
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Figure 4-2. GE Burroughs and Compensated IG	S riangle P in Sensed

Coordinates







Figure 4-3. GE Final and Compensated IGS $\triangle V$ in Sensed Coordinates



Figure 4-4. GE Final and Compensated IGS ΔP in Sensed Coordinates





Figure 4-5. MISTRAM I 10 K and Compensated IGS △V in Sensed Coordinates





Figure 4-6. MISTRAM I 10 K and Compensated IGS $\triangle P$ in Sensed Coordinates







Figure 4-7. MISTRAM I 100K and Compensated IGS △V in Sensed Coordinates





Figure 4-8. MISTRAM I 100K and Compensated IGS △P in Sensed Coordinates





Figure 4-9. MISTRAM II Passive and Compensated IGS $\triangle V$ in Sensed Coordinates





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		212만 수는 것이 못했다. 1997년 - 관련 문제		
■新聞書 法有效 化磷酸钙 医白花属 医子前间的 现在,让他在我们的人们的一个。 「我们我们就是我们的,我们就是我们的,我们就是我们的,我们就是我们的,我们就能能能了。"				: 25 만원은 1월에 있는 · · · · · · · · · · · · · · · · · ·
刘浩浩,我们这些这些,你们是你没有要你不会是你,我们就是你的,你不是你?" "你们我们,你不是你的吗?"			1977-111 11日 表演演会 1987-111日 日本語 表演演会	· 我们就能会到了这些人的问题。 - 我们就是你们都没有的。
: : : : : : : : : : : : : : : : : : : 	19月1日日 - 19月1日 - 19月100000000000000000000000000000000000		- 当らら三型番び編集 編集書: 二連 現 委 増 編	· · · · · · · · · · · · · · · · · · ·
雺漝褬瞷貗龗ۦ漝麙聭漃臶弡۔跟礛鐕 櫩鐁齀 齀瑿齫櫩勪勪譱癵裶峬 箽愮煭艍攱ᆟ洔夰夰 莂劅駲壛驑犦 塣礹峫雗璑즼岃晀韲頺탘椣夎擈摝薎瀒麙薒薗遧誁莌韺猐遪繿仱扷芕芕丂	2011年1月1日日の日本日本日本日本日本日本日本日本日本日本日本日本日本日本日本日本日本日本	····양국 및 및 비한 영화적 ····영택 ····중·············		????????????????????????????????????
颰曔黺瘷囒婯勫勫枩水 湬笷笍銌荌屰瞏苃霻 迼嫾嫾嫾蓙聮殔瘷欰 碞焑乭庈彑頙淔鴂 颰曔黺瘷囒琧勫麆 枩埢湬笷笍盵唟荌碤瞏苃霻濸鑝 漝蓵蕸歱朣憿剓 袮搻塣蒮朾譋顀庍秥	(論語)新聞者教育人が 2000に、ジールでし. 新聞教育の問題を引き、その人気してた。			
王帝 建筑 化化化学 美国 所有 为这样的 建设 计学 计图 的第三人称单数 化化学 化化学 化化学 化化学 化化学 化化学 化化学 化化学 化化学 化化				
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	「「「」」、「」」、「」」、「」、「」、「」、「」、「」、「」、「」、「」、「」	「小川 ちゃ 東方 をぎょう	슻놰썦셤킿쏚툹촫킲 줂놰뱮숺휇궳쁥홂믋	, 유럽 및 유통 이 관계 가 이 소 식 등 수 있다. 이 가 하는 것 같은 것 이 가 가 하는 것 같 것 이 가 하는 것 같 것 이 가 하는 것 같 것 이 가 하는 것 이 가 하는 이 가 하는 것 이 가 하는 것 가 가 하는 것 이 가 하는 가 하는 것 가 하는 것 이 가 하는 것 이 가 하는 것 가 하는 것 이 가 가 하는 것 이 하는 것 이 가 하는 것 이 가 하는 것 같이 가 가 하는 것 이 가 하는 것 이 하는 것 이 가 하는 것 이 가 하는 것 수 있다. 이 가 하는 것 같이 않는 것 같이 않아. 이 가 가 하는 것 같이 것 같이 것 같이 않아. 이 가 하는 것 같이 않아. 이 가 가 가 가 가 하는 것 같이 않아. 이 가 가 하는 것 같아요 않아. 이 가 가 가 가 가 가 하는 것 같아. 아니 가 가 가 가 가 가 가 하는 것 같아. 것 같이 것 같아. 것 가 가 가 가 가 가 가 가 가 가 가 가 가 가 가 가 하는 것 . 가 가 가 가 가 가 가 가 가 가 것 수 가 가 가 가 가 하는 것 같아. 것 수 가 가 가 가 가 가 가 가 가 가 가 가 하는 것 . 가 가 가 가 가 가 가 가 가 가 가 . 가 가 가 가 가 가
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·····································	1999年春日に、1999年4月に2013年9日 1998年春日に、1999年1月に対応す。	となりの自己の登録的構 で構立したようで通知	はなどの 部にある。 時代できた の空気活動	業業 新市 法保 建物 智慧 化性 希望 教室 法建立所 力型 教育 计数 利用 金属 医原
에는 것은 것은 것을 통해 가는 것은 것은 것은 것은 것은 것을 것을 가 같은 것을 것을 가 했다. 같은 사실 것은 것은 것을 다운 것을 다 있는 것을 다 있다. 것은 것을 가 같은 것을 것을 것을 하는 것을 것을 것을 하는 것을 가 있는 것을	· · · · · · · · · · · · · · · · · · ·			
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刘雯,你们的你,你们的你?你 你不是你的你?""你们你不是你的你?"	審査時間を行う。 こうりょう	가지 같은 것 같은 것 가격했다. 	뾃훕끹뜡波 촣 츐홵뾃 삖귟곾슻쳛옱틳퍳먬	·승객학부 삼국 삼중 권통 후미 유수 같이 ·수객학부는 1월 관년 유명 보상 문화 관년
드랑 김래 민준 기방 우수 또는 분별 운영 등 김 것 나라 전북 전북 전북 관계 	(27)	・ ドロド村・台駅将 第三回に、 市職権	铝石的复数 1.1 动物 建新 新闻的 最近 和书 维朗	놂쓕궦휶슻 휳랦긢쑵꺌끹쌲곜쁥 훬톎 놂껆놂괎 슻먣 슻븮뮾뮾슻쁥꿗탒욯냬
드려 마르 비밀 시민 만열 방법 의해 가장 바람 바람 귀엽 원종 강점 유명초 중 분야 하는 것은 특별 마르 비밀 신문 마을 해당 바람 관람 관람 강별 상품 방법 영화 관계 유통 관람 보내는 것은 것	12. 春野養鮮年後の世代にというため! 1編編査運送が2011年に1月4日にという。	토동원 이 11년 - 166년 - 이 이 이 이 도입이 주	蔳奆垥丷丷 衤 衦 刐 鼅蓙誷扳ᅴ羘泀鵋螕	Դ댴珥ᅴ蓙棆 琞 뭱 轚榝茡夦蘷麈輡 솖藅乄殸弡궻륟 ╸ ℴ茡┍┍迼귿ᅿᄐ
ᅋᅊᅋᅘᅊᅝ ^ᆞ ᅖᆕᇻᄚᇊᅘᄔᅆᄹᇾᅋᇾᇘᇛᇊᄧᆂᇍᇌᅒᅒᇑᄔᆎᅒᆍᆍᅖᆋᇤᇑᄢᅆᅸᇾ ᄜᇃᄪᇕᅒᇃᇦᆎᇦᇦᇃᄧᅊᇴᆎᆤᄩᄼᆄᄡᅒᇾᄸᇑᇕᄨᄧᇎᇛᆑᇑᄷᄢᅆᅖᇎᇩᇨᆞᆞ	審査: 職務起来考示:			
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Figure 4-10. MISTRAM II Passive and Compensated IGS $\triangle P$ in Sensed Coordinates



	NISTRAM FINAL AND	COMPENSATED IGS VELOCI	TY COMPARISON		F16 42	· · · · · · · · · · ·				
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Figure 4-11. MISTRAM Final BET and Compensated IGS △V in Sensed Coordinates





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Figure 4-12. MISTRAM Final BET and Compensated IGS △P in Sensed Coordinates





Figure 4-13. AFETR BET and Compensated IGS $\triangle V$ in Sensed Coordinates







Coordinates





Figure 4-15. TOPS BET and Compensated IGS $\triangle V$ in Sensed Coordinates





5. RENDEZVOUS RADAR EVALUATION

The rendezvous analysis for the flight consisted of comparing the onboard radar measurements (R, A, E) with a set of calculated measurements. The calculated values were obtained by reconstructing the trajectories for both the Agena Target Vehicle (ATV) and the Gemini spacecraft during the rendezvous sequence and then differencing the trajectories to obtain a relative position vector.

5.1 TRW/RENDEZVOUS RADAR COMPARISON

The ATV and Gemini trajectories were reconstructed using the ground radar data detailed in Table 5-1. Gemini 8 IGS accelerometer data were used in the TRW orbit prediction program to propagate the Gemini trajectory through the terminal maneuvers preceding docking.

Flight	Comparison interval GET	Tracking data used in orbit determination							
phase	(min)	Gemini	Agena						
Pre NSR	212	CALC 02	CYIC 01						
	to	WHSC 02	CYIS 01						
	220	GTIC 03	CROC 01						
		PREC 03	HAWC 01						
			HAWS 01						
			CALC 01						
			GYMS 01						
Post NSR	270	CALC 03	WHSC 01						
to	to	HAWC 03	TEXS 01						
TPI	315	PREC 04	HAWS 02						
		1	CALS 02						
			EGLC 03						
		1	MLAC 03						
TPI	316	Pre TPI	GBIC 04						
to	to	fit propagated	CALS 04						
rendezvous	355	through burns	1						

Table 5-1. Ground Tracking Coverage



The results of the comparison between observed and calculated rendezvous radar measurements are presented in Figures 5-1 through 5-3. These plots show the range, azimuth, and elevation residuals over the data span from 210 to 344 minutes from launch. Figures 5-4 through 5-6 are plots of the rendezvous radar measurements themselves.

There appears to be an inability to reconstruct the trajectories, most probably the Gemini trajectory, to better than a mile or so over this rendezvous interval. The quality of the Gemini orbit reconstruction over the main period of interest, NSR to TPI, depends primarily on the quality of three radar passes:

HAW	03,	maximum elevation 16 ⁰	
CAL	03,	maximum elevation 5 ⁰	
PRE	04,	maximum elevation 9 [°] , which represents the pre-TPI burn portion of this pass	e

Fifty minutes of orbit must be determined by this tracking, and the conclusion must be that the tracking data quality is not adequate for a better overall orbit determination than the 1000 to 4000-foot residuals shown in the comparisons. (The assumption here is that the rendezvous radar is relatively accurate, which appears justified in this case since the radar measurements successfully accomplished the rendezvous, and no major radar biases were noted by the astronauts when the Gemini and ATV were relatively close together.)

The lack of a precision reconstruction means that a detailed rendezvous radar evaluation cannot be done. However, the comparisons (Figures 5-1 through 5-3) can and do demonstrate grossly adequate radar accuracy and provide good estimates of system noise (the reconstruction is smooth, if biased). A comparison of this accuracy would be very useful in the event of a system malfunction.

Both the tracking coverage and maneuver telemetry data on Gemini 8 were better than for the rendezvous interval of Gemini 7/6, and a considerably better comparison was obtained. Gemini IX will rendezvous a full orbit earlier, which should provide better ground tracking coverage than either of the previous missions. Therefore, an improved relative position determination should be possible. The analysis procedure is also being examined in an effort to improve the accuracy of this comparison.



5.2 RTCC/RENDEZVOUS RADAR COMPARISON

It is desired to generate a comparison which demonstrates the accuracy with which the MSC RTCC real-time operation computes the Gemini/Agena relative trajectory in the post-coeliptical (NSR) maneuver interval. A comparison identical to that just presented (Figures 5-1 to 5-3), but substituting an RTCC-calculated trajectory for the TRWcalculated values is an attempt to show this accuracy.

Figures 5-7 to 5-9 are plots of the comparison between observed onboard radar measurements and predicted parameters using RTCCinitialized Gemini and Agena orbits. The RTCC vector nearest NSR was taken for Agena; the first vector print <u>after</u> the NSR maneuver was taken for the Gemini initialization. No subsequent updating by the RTCC is reflected in this trajectory; that is, the RTCC vectors at the indicated times were simply propagated forward using the TRW reconstruction program, and the resulting Gemini/Agena trajectory differenced and compared with telemetered radar values.

The Gemini orbit was constructed using initial conditions provided by the RTCC program at $20^{h}15^{m}0^{s}$ GMT. (The vector was taken from the RTCC on-line print.) The Agena orbit was constructed using initial conditions provided by the RTCC program at $20^{h}33^{m}0^{s}$ GMT. The comparison span was limited to the interval of time between the NSR and TPI maneuvers.

It is apparent that utilizing RTCC initialized orbits leads to somewhat greater residuals in <u>relative range</u> than the TRW reconstruction presented here; however, no significant differences exist in azimuth and elevation angle residuals.



4.4

Rendezvous Radar Residuals ΔR, Radar Minus TRW Calculations 5-1. Figure !



Figure 5-2. Rendezvous Radar Residuals ΔA , Radar Minus TRW Calculations

3150-6036-R8-000 Page 5-5





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Figure 5-3. Rendezvous Radar Residuals \Delta E, Radar Minus TRW Calculations





Figure 5-4. Rendezvous Radar Telemetered Relative Range

3150-6036-R8-000 Page 5-7



3150-6036-R8-000

Page 5-8

Figure 5-5. Rendezvous Radar Telemetered Relative Azimuth



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3150-6036-R8-000 Page 5-9



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Figure 5-6. Rendezvous Radar Telemetered Relative Elevation



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Rendezvous Radar Residuals ΔR, Radar Minus RTCC Trajectory Figure 5-7.

3150-6036-R8-000 Page 5-10



Rendezvous Radar Residuals AA, Radar Minus RTCC Trajectory Figure 5-8.



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E



Figure 5-9. Rendezvous Radar Residuals ΔE, Radar Minus RTCC Trajectory

APPENDIX A ASCENT TRAJECTORY

The ascent trajectory is provided in three separate forms: a) guidance coordinates as sensed by the accelerometers (these data are uncorrected for errors determined during flight); b) an earth-centered inertial coordinate set; and c) various special earth-referenced parameters. The latter two have been corrected for apparent IGS errors and therefore represent the TRW best estimate of the ascent trajectory.

The earth-centered inertial coordinate system has the z axis aligned with the earth's rotational axis, positive north, and the x-y plane is in the equatorial plane with the x-z plane containing the Greenwich meridian at platform release time.

Figure		Page
A-1	Sensed Acceleration in IGS Coordinates	A -2

Tables

A - 1	Sensed Trajectory Listing for the Ascent Flight Phase	A-3
A-2	Reconstructed Ascent Trajectory, ECI Coordinates	A - 5
A-3a,b	Reconstructed Ascent Trajectory, Special Parameters	A-7





Figure A-1. Sensed Acceleration in IGS Coordinates

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3150-6036-R8-000 Page A-3

Table A-1. Sensed Trajectory Listing for the Ascent Flight Phase

				CEMINE EDIT	FRGGRAM				
TIME IN SECURES FROM LIFTOFF									
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.475 2.578	-1	-231	- 1	29	-127.22	23	11	-41.22	02
5.121	-1	-1265	-1	26	-319.01	55	.02	-41.76	14
7.663 5.736	-2	-2211 -5165	-3	05	-425.75	-1.69	• u 0	-42.28	22
12.266	-1	-463*	-11	29	-523.34	-2.28	7	-43.19	36
14.029		-6367	-35		-754.24	-3.20	12	-43.72	42
19.471	- 5	-10240	-38	-1.2?	-938.97	-5.36	- 23	-44.75	45
24.453	-10	-12762	-53	-2.01	-1954-10	-6.67	04	-45.39	44
26.487	-20	-1744	-+7	,	-1259.17	-8.63	1.58	-40.56	51
29.094	-15	-21288	-112	5.1J	-1391.77	-10.14	3.21	-47.26	53
32.656		-26249	-154	27.22	-1501.64	-12.41	6.67	-48.30	50
26.306	145	-32594	-158	47.49	-1728.39	-13.93	e.75	-48+83	44
40.568	474	-41165	-201	fe.17	-1955.91	-15.45	12.37	-49.61	22
42.515	1060	-46342	-367	1:4.27	-2065.18	-15.83	14.41	-50.05	22
48.121	1535	-5e472	-392	265.72	-2317.32	-15.99	18.07	-50.72	22
50.725	2139	-+2+8+	-428	256.06	-2449.70	-17.76	20.15	-51.07	03
55.330	3542	-74562	-507	351.77	-2556.76	-10.53	23+66	-51.51	.14
57.538 80.030	4555		-545	421.74	-2921-25	-15.48	20.57	-51.e7	.45
62.540	6767	-55215	-614	550.72	-2924+25	-13.11	27.12	-51.65	- 34
65.147	8326	-105363	-645	671.33	-3193.J5	-13.91	72.34	-51.18	.10
65.747	11567	-112552	-676	796.57	-3274.65	-14.71	34.30	-50-98	- 30
72.362	13764	-127725	-742	290.22	~ 3559.49	-9.20	39.09	-50.90	33
76.965	15035	-144645	-761	570.77	-3550.41	-10.59	45.27	-51.43	-1.14
75.572	212±€	-154726	-854	1186.91	- 19:4.20	-24.80	42.94	-53, 39	-2.82
B1.565	23716	-102676	-90 8	1273-15	-4041.48	-29.57	44.44	-53-68	-2.97
86.766	36553	-124513	-1109	1518.19	-4324.36	-46.99	49.94	-54.05	-3.29
58.779 C1 303	74115	-193235	-1268	1615.69	-4431.79	-52.36	52.14	-54.14	-3,19
94.002	42215	-217123	-1525	1966.63	-4715.70	-73.30	57.81	-54.55	-3.35
\$5.554	47230	-226626	-1675	2024-04	-4824.45	-74-55	60.12	-54.60	-3,35
101.255	58729	-25.762	-2126	2357.16	-5111.51	-94.62	65.54 65.66	-54.47	-3,49
102.250	e357e	-263165	-2322	2402.53	-5230-17	-101.76	65.11	-54.55	-3.52
105-171	73352	-216531	+28L1 +2836	2626.80	-5475.64	-119.40	74.64	-54.86	-4.03
110.535	8364;	-362551	-3159	3627.56	-362L.#5	-129.54	78.47	-54.53	-4-51
112.145	91853	-317425	-3014	3426.54	-5867.76	-152.49	82.57 85.90	-52.73	-4.67
117.769	117733	-34441 5	-4225	2637.09		-164.43	90.03	-51.93	-4.39
120.368	125652	-306514	-4676	36 73.59	-0243.56	-183.47	93.92 56.96	-52.13	-4.55
125.046	136654	-344672	- 5532	4321.79	~6391.52	-195.83	100.54	-53.02	-4.85
127.663	148234	-476557	-6962	4595.33	-5522+19	-209-15	104.38	-54.09	-3.31
132.2E4	170722	-437262	-76 57	51 42.37	- 5775. 70	-235.49	112.05	-55.66	-5.91
134.903	184469	-4:5213	-7724	5257.59	-6522.80	-251-35	110-56	-56,48	-6-07
135.524	210651	-467611	-8951	5511.58	-7186.96	-279.67	126.47	-58.03	-6.44
141.563	22:107	-502557	-9534	6220.05	-730ú-14 -7461-58	-293.00	131.09	-58.79	-6.72
146.E73	258-47	-54:22*	-11185	6949.69	- 162 3. 73	-330.93	144.26	-64.93	-1.50
148.674	272246	-657662	-11866	7244.14	-7746-54	-345-02	159.04	-61.87	-7.82
153.453	307354	-554052	-13553	7568.33	-8357.34	-383.95	164.14	-64.15	-8.55
154.600	316273	-6.2564	-13981	8151.84	-9116.53	-393.51	167.52	-64.10	-8,73
156-117	228638	-+:=1.7	-14586	8210.49	-2133.70	-347.15	44.25	-14.12	-3.30
156.736	350226	-636643	-15630	8314.87 8355.88	-8167.96 -8197.20	-405+60	46.93	-14.19	-3.39
163.396	389514	-674862	-17558	85CE.85	- 9234 . 26	-421.92	42.34	-14.33	-3.60
166.013	411973	-656462	-10675	8620.87 F766.81	- 1271.02	-431.44	45.12	-14.41	-3.62
170.554	+51533	-7:4175	-2-673	8620.23	- 3337.94	-447.66	45.11	-12.79	-2.38
173.172	474775	-756656	-21852	8544.06	-8365.61	-451.98 -457.51	46.44	-10.35	-1.22
177.607	514891	-743247	-23858	9151.71	- 3403. 54	-452.57	48.46	-7.00	03
180.263	535371	-015593	-25041	S261+45	-3421-12	-452.64	45.27	-6.38	.11
184.815	562172	-854(21	-271-1	95.°.22	- 3448 . 97	-451.51	50.59	-5.81	.29
167.495	6C7H45	-87669C	-24330	9645.66	-6463.86	-450-00	51.32	-5.49	•37 •41
192.017	651949	-9149E1	-34352	5880.95	-8498+02	-448.73	52.79	-5.68	.51
194-657	67E±27	-537752	-11563	10123-05	-350T+12	-447.26	53.58	-4.76	.59 .61
199.215	724461		-3,57t	1-1265-52	-0521.49	-444.31	55-14	-4.39	.70
201.935	752555	-\$55357	-34762	10415.87	-8533.24	-442.18	55.84	-4.14	.75
2020105	800210	-1037564	-36776	10675.42	-6551.67	-438-65	57.45	-3.66	.81
205.129	829625	-1050951	- 17643	16830.51	-8566.57	-435.43	58.75	-3.33	. 85
213.645	74850C 876574	-1055575	-395(5	11056.35	-9574.46	-432.53	60.02	-2.60	.91
214.325	906*-2	-1122574	-41661	11220.26	-8581.38	-429.92	60.93	-2.50	.93
218.157	929234 960000	-1158299 -11013c4	-42004	11540.04	-8591.19	-425.84	62.83	-1.68	.95
223.561	541543	-1164725	-44]	11/12.25	-8595.81	-423.15	63.82	-1.48	1.01
228.076	1 113201 3 145142	-1223545	-46648	121 5.00		-416.31	65.BU		1.13
230.757	10775E1	-1246610	-47164	1/162.79	- 3633.55	-415.13	66.50	67	1.18
e360371	*******	- ********						• • •	





Page A-4

Table A-1 Sensed Trajectory Listing for the Ascent Flight Phase (Continued)

TIME	×	۲	_ Z	XCCT	YOCT	2007	X000T	TODOY	DODT
(SEC)	. (ET)	{FT}	(FT)	IF1/SEC1	(FT/SEC)	(FT/SEC)	(FT/SEC+	(FT/SEC+2)	/SEC+21
		10(6+10		1740 33	- 4 - 14 - 53	-405-72	69.13	. (4	1.27
232.569	116744.)	-12(5532	-501 45	12470.23	-8624-22	-405.98	79.19	49	1.33
239.642	1191962	-132475	-50866	12909,99	-95)3.12	-403.65	70.83	.66	1.35
242.554	122158	-1348452	-51991	13008.16	- 9600.27	-399.72	72.66	1.32	1.33
245.361	1262169	-1371728	-5306A	13256.83	-3595.93	- ? 96 . 37	74.04	1.90	1.37
247.155	1286674	-1587657	-53861	13344.95	-9592.73	-393.85	75.17	2.27	1.35
249.864	1323117	-141(933	-54862	13550.84	-8565.24	-389.83	10.08	Z. HO	1.38
251.715	1348:25	-1426515	-53582	13055.01	-3565.87	-383.79	75.39	3.94	1.38
254.423	1422724	+1473278	-57663	14123.98	-8558.34	-379.97	81.04	4.67	1.43
258.567	1445953	-1489100	-53353	14275.13	- 8549.20	-377.37	82.49	5.12	1.46
261.740	1464619	-1512623	-59397	14504.15	-9534.44	-373.27	84.15	5.73	1,50
264.446	1525175	-1535656	-6.3401	14734.49	-8519.12	-369.08	85.93	6.41	1.55
264.259	1556623	-1551405	-61082	14894.96	-8505.75	-366.29	27.46	6.95	1.57
269.011	1597341	-1574595	-62070	15135-01	-8462.77	-361.92	85.49	/ . 68	1.60
270-260	1625474	-1590179	-63702	16561.17	- 1447.48	~ 354 . 57	93.20	9.06	1.61
276.282	1705811	-1635989	-04653	15866.96	-9422.29	-351.02	95.35	9,99	1.70
278-132	1739212	-1051545	-653.)?	15985.05	-84.2.54	-346.66	\$7.55	10.77	1.7!
280.844	1787923	-1674258	-66237	16252.37	-9372.95	-342.12	95.8¢	11.70	1.7
283.590	16522633	-1697245	-67165	16:29.90	-8339.39	-336.90	102.34	12.74	1.8
265.445	1854765	-1712668	-67791	16722.03	-8314.86	-333.56	104.78	13.69	1.9
288.157	1904514	-1755154	-64685	17004.08	-527C.CJ	-328.20	137.39	14.07	1.9
290.7122	1948662	-1756450	- 3 - 5 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7	17415.69	- 3137623	-319.65	112.88	16.87	2.0
295.071	2124734	-1762033	-73911	17775.75	-8163.55	-214.3	115.18	18.18	2.20
297.645	2076961	-1013639	-71713	18062.64	-9115.31	-308.2"	115.40	19.39	2.30
300.225	2117545	-1833855	-72500	18354.56	-8063.68	-302.2 !	122.77	20.64	2.40
302.840	2156476	-1854875	-73282	18721.60	-4337.77	-295.8/	126.61	22.07	2.50
304.604	2199654	-1+c25t4	-73800	14548.11	-7967.77	-291.42	129.94	23.39	2.63
307.184	2249013	-1865441	~74543	19260.49	- 1935 - 36	284.43	134.88	23.25	2.19
309.783	2295217	-1965/45	-/5266	21/211.60	-7765.20	-769-27	143.70	28-82	3-07
212.300	23377463	-175010.		20011100			1430.0		
314.144	238r 62 3	-1943314	-75451	23264.97	-7712.73	-263.62	148.60	30.50	3.44
316.724	2439417	-1962616	-77744	26658.04	-7544.74	-255-12	160-62	35.04	3.57
221.919	2493154	-2002756	-78398	21489.88	-7450-13	-236.73	165.40	36.46	3.69
124.455	2604757	-2021845	-78950	21525.85	-7351.03	-226.73	173.65	39.67	3.91
326.261	2643752	-2034781	-79390	22242.53	-7279.11	-219.63	181.64	42.80	4.19
328.840	2701765	-2053411	-79942	22717.58	-7156.45	-208.89	189.52	45.67	4.54
331.459	2761921	-2672622	-80474	23223.78	-7042.72	-156.72	197.65	49. 2	2.08
334.033	2022374	-2085582	-80962	23191+32	-5909.50	-168.07	211.04	57.4	6-06
330.911	2081254	-2100/00	-81541	24257604	-6712.43	-161.75	213.70	59. 3	6.26
338-455	2929401	-2115590	-81712	245 57 . 26	-6689.15	-159.51	2.31		.14
341.065	2953493	-2137442	-82127	24567.01	-068t.94	-158.70	2.31	• • 5	.10
343.445	3051565	-2153354	-82504	24574.28	-5685.22	-157.90	2.41	• 55	-06
345.842	3110851	-2165380	-828P1	24578.65	-5584.40	-157.48	1+44	• 37	.07
348.120	3166891	-2184eC5	-83244	24560.32	-6684.08	-159.43	70		
350.405	3223061	-2155683	-83665	24766.80	-6684.00	-157.27	. 12	-03	.19
355.301	3254054	-2235464	-84374	24581.48	-5684-11	-157.23	.05	.0.	00
357.594	3355764	-2247930	-84735	24581.54	-0683.79	-157.10	.11	.01	.00
359.905	3456585	-2263380	-85058	24581.60	-6683.56	-157.26	12	•02	•00
362.862	3527786	-2282739	-85553	24581.91	-6683.63	-157.21	. 34	.11	.01
364.564	3581414	-2257321	-8535c	145E2.08	-6083.81	-1-7-18	.58	•11	.01
367.1e0	3674528	-2311861	-36239	24585.47	-0682.79	-157.05	• 57	. 14	02
370.030	3766760	-2351042	-93083	24301411	-0002.07	-157.36		01	04
374.419	3813400	-2360376	-87380	24587.82	-6682.47	-157.32	.14	03	01
376.558	386657-	-2374935	-87723	24567.80	-6682.60	-157.48	.04	01	.00
379.523	3936865	-2354480	-84193	24587.80	-5682.47	-157.24	.00	.14	• DZ
381.653	3996175	-2410051	-88549	24587.76	-0682.45	-157.40	07		.03
384.051	4351213	-1425009	-88901	24587.83	-6692.33	-157.17	.12	02	01
386-270	4104783	-2439567	-89244	24587.80	-6682.51	-15/.23	- 01	01	02
385.147	4175518	-/432/52	-94026	24361.61	-2024.35	-131+38	4	• • •	
391.359	4229983	-2472567	- 70(44	24567.88	- 5682.46	-157.35	00	•02	00
393.536	4283453	-248E125	-90387	24567.65	-5682.23	-157.31	.26	12	-01
396.412	4354164	-2507343	- 30829	24517.86	-6682.31	-157.27	02	- 02	
358.704	-+16519	-2722035	-41500	24381.92	-0002.38	-121-33		-+00	



Table A-2. Reconstructed Ascent Trajectory, ECI Coordinates

GENINI & ASCENT TRAJECTORY 1. ECIG. COORCINATES.)

TIME									
FROM LIFTOFF	PX	PY	PZ	٧X	٧Y	• V7	XA	84	A Z
(SEC)	_					.		· · · ·	
.4748	3024939.5	-18152177.0	0927951.0	1324.178	215.753	2.133	1.1822	-7.8154	4,3316
2.5793	3027727.6	-18151938.5	9927964.7	1326.732	2:31).435	10.992	1.2783	-8-1502	4.3831
5.1213	3031105.6	-18151455.n	9928006.9	1330.122	179.645	22.175	1.3698	-8,3229	4.4713
7.6633	3034491.5	-18151025.7	9928(77.6	1333.443	157.896	33.657	1.4711	-8,8154	4.6587
9.7356	3037255.7	-18159717.7	0928157.6	1336.795	134.281	47.619	1.4634	-9.1914	4.8194
12.2663	3041477.0	-18150393.0	9929284.6	1346.45	115.159	56,081	1.4736	-9.6565	4.9784
14.8391	3044100-5	-18150131.0	9928444.5	1344.482	99.848	69.ne7	1.4914	-10.1749	5.1807
16.9143	3046893.2	-18149966.7	9925598.7	1347.404	68.241	79.706	1.4979	-10+6026	5.3778
19.47-39	3057343.1	-18145827.2	9928820.6	1351-288	49,634	93.991	1.5226	-11.1062	5.6542
22.0217	3453794.9	-18149761.0	9929079.1	1355-192	11.339	176.773	1.794?	-11.6373	5.0517
24.4014	3657140.(-18149768.2	0929356.4	1359.285	-17.687	123.924	2.5821	-12-1611	6.1614
20.444	1009861.2	~18149828#Z	9929625,7	1304,04/		1 ****11	5.2214	-12+2022	6. 411 4
24.1444	3403933.1	-10149982.7	99 30 433 4	13/7.919	-10.192	123.034	7.2727	-12.7441	
32 4046	300034 3	-10179227+2	77 78/42340	1391.914	-110.102	104.070	1.2477	-13 4444	6 4520
33.0-02	30070.74.1	-1017-911-1	79 57 (10.4	1477 548	-177 407	103.002	10 0528	-13 4475	4.7425
34 3051	3674414.0	-18151345 7	00014004	14334708	-100 810	214 240	17 5877	-13.7404	6 8475
40.9184	3080267-5	-18151814.2	9932272.9	1402.511	-735.744	232.249	14.6478	-13.8284	6.9814
43.5198	3084216 2	-18152477.0	9932901.1	1533.576	-272.024	250.690	16.7197	-13,9799	7.0037
45.5086	3687300.6	-18153045.7	9933416.0	1548-095	-299.783	264.805	18.3441	-14-0641	5.9893
49,1213	3091467.7	-18153878-0	9934131.9	1618.763	-337.152	282.845	20.4312	-14-1611	6.9745
5. 7787	3795756.7	-18154805-3	0334 807 .	1675-161	-373,965	300.587	22.5401	-14.1475	7.1126
57.7199	3-199137.4	-18155578.4	69355P5 C	1721.108	-472.306	315-167	24.1472	-14-0946	7.2252
55.33 3	31 127 14.0	-18154475.7	0936357.9	1786.949	-438.025	334.460	76.2P54	-14-(772	7.3562
57. C377	31-15465.7	-18157868.2	9937250.0	1858.231	-475.539	353.660	28.4R28	-12.7869	7.2606
59,0289	3112223.7	-18159842.5	9937968.6	1916.777	-502.839	368.103	30.1057	-13.6454	6.9938
62-5402	3117334.1	-1816 201.2	0938954.5	1995.105	-537.923	386.435	32.2358	-13.3752	6.4837
65.1457	3122653.7	-18161649.0	9939087.7	2784.612	-572.90P	477.095	34.5852	-12.8546	5.1281
67.1379	3126873.6	-18162815.7	0941794.1	2154.75*	-598.1.13	413.125	36.4937	-12.3684	5.9271
69.7473	3132623.7	-10164418.7	9941892.4	7253.759	-670.331	429.283	39.0473	-11.7880	5.8397
72.3615	3138652.6	-18165101.7	994303R.C	2359.507	-658.519	445.915	41.1879	-12-0944	4.9843
74.3537	3143436.4	-18167437.0	9943935.4	2443.470	-682.512	454.424	42.4041	-12.8264	4.3992
76.9651	3149964.8	-18159264.0	9945132.4	2556.570	-717.773	462.682	43.7302	-14.1011	3.7384
70.5775	3156779.2	-18171187.2	9946351.1	2671.105	-757.352	472.615	45.2570	-15.4503	3.6457
#1.5647	3167190.6	-18172725.7	9947301.2	2762.086	-797.471	480.924	46.7997	-15.3917	3.6071
94.177	3169567.0	-18174837.7	9548569.6	2884.745	-829.139	489.309	49.3584	-15.3373	3.3667
86.7863	3177271.0	-18177053.7	0949855.9	3019.288	-868.914	497.549	52.2405	-15.0601	2.9791
86.7785	3183399.9	-18175813.7	9950253.9	3125.488	-897.999	503,999	54.4216	-14.8923	2.9212
91.3918	3191748.7	-18181210.2	9952178.6	3271.795	-936.512	510.002	57.2035	-14.7867	2.5785
04.0322	3201486.3	-181837:4.7	9953518.6	3424.111	-975. #66	516.702	62.1.663	-14.7143	2.3478
95.9943	3207428-2	-181 45679.7	9954553.0	3545.783-	1024. 847	521.557	62.3486	-14-5193	2.1576
98.4776	3216010.7	-18184355.2	9955972.0	3712.696-	1042.635	526.653	65.51P6	-14-1573	1.7698
101.2551	3226972.7	-18191164.7	9957322.5	3890.193-	1079.593	530.585	68.7760	-13.7696	1.3578
103.2532	3234972.8	-18193346-0	9958383.7	4030-091-	1176.756	533.014	71.1995	-13.5851	1.1414
105.8713	3245684.7	-18196291.7	9959783.4	4720.975-	1141.289	535.243	74.3048	-13-6132	. 9351
107.0221	3754498.7	-18198661.0	9960883.4	4375.501-	1159.759	537.345	76.8696	-13.4869	. 3893
11. 5354	3766157.7	-18201766.5	9967789.6	4579.761-	1226.312	538.022	95.3817	-13-0448	6035
113.1496	3278444.=	-187-4962.7	3953691.5	4734.679-	1239.244	\$34.295	84.2765	-11-88"2	-1-6467
115.1467	3298194.8	-18207461.7	9964754.4	4966.337-	1261.799	579.514	87.4383	-10-7594	-7-3074
117.76*8	3301521.6	-18210896-2	9965134.0	52 30 . 607-	1258.349	522.697	91.4044	-9.4957	-7.8244
120.3979	3315440.8	-18714211-2	9967493.4	5445.256-	1311.778	514.925	95,2195	-8.9254	-3-1943
122.4779	3326759.9	-18216902.2	9958574.5	5642.709-	1327.554	5:17.744	98.1556	-8.9633	-3.4239
125.0461	3341683.8	-18223409.0	9959853.5	5904.292-	1351.783	498.237	101.8936	-9.5313	-3.4747
127. 4633	3357689.F	-182730A1.5	9971144.7	6175.469-	1375.706	488.518	135.8134	-10.2652	-3.9235
129.6652	3370265.9	-18226761.2	9972115.1	6390.254-	1399.029	480.619	179.1331	-10.6907	-4.1426
132.7644	3337381.3	-18230463.2	9977358.7	66F1.189-	1429.005	469.985	113.5746	-11.0949	-4.4116
134.9925	3415267.9	-18234240.7	9974571.0	6994.353-	1457.632	457.070	118.4196	-11.3703	-4.6136
136.9035	3419482.7	-162371 802	P975476.5	7724.833-	1489.415	447.829	122.5012	-11.5505	-4.7725
139. 236	3438878.5	-10241008.5	9976611.2	7552.487-	1511.779	435.040	128.1027	-11.8512	-5.7876
141.56?7	3454517.7	-18744204.0	99775: 0.6	7818.036-	1535.301	474.469	132.7471	-12.1526	-5.3979
144.1958	3475477.0	-18248273.5	997863.9	81 73. 756-	1557.695	409.637	139.0914	-12.5579	-5.8258
146.8733	3497953.3	-18252532.5	9979683.1	8555.651-	1601.971	393.405	146-0063	-12.9661	-6.2937
148.5742	3515369.2	-18255764-0	9980457.6	9853-433-	1628.121	390.535	151-8333	-13,2989	-6.6664
151.4943	3539112.8	-18243779.2	9081431.0	9260.597-	1663.561	362.318	159.894R	-13.7545	~7.1615
153.4934	3457929.3	-18263429.7	9982141.9	9585.937-	1691.349	347.646	166.P338	-14.1021	-7.5382
154.6090	3568649.2	-18265309.5	9987421.0	9771.495-	17.7.443	339.194	169.4352	-14.2949	-7.7458
156.1174	3583509.1	-18257879.7	9957071.C	9825.870-	1687.769	318.395	36.4437	17.9367	-14.9500
158.7356	3679357.7	-18272217.7	9983804.0	9920.171-	1633.666	279.594	37.0505	17.8751	-15.7462
160.7736	3629652.7	-18275510.5	9984342.7	9996.253-	1597.508	248.978	37.5226	17.8273	-15.1211
163.2957	3655993.7	-18279637.7	0994943.N	10095.881-	1550.501	208.887	38.4008	17.7707	-15.2647
166.0120	3672548.9	-18283634.5	99 95 437. 7	10197.401-	1574.611	168.709	39.1476	17.7509	-15.3061
167.9465	3702344.2	-18786509.7	9985735.1	1-273.757-	147*.29%	139.192	39 .94 85	18.3^8%	-15.1894
176.5539	3729264.2.	m18790284-2	9986045.5	103.28-675-	1423.708	99 368 ,	40.8562	19.9292	-15.1521.
173.1721	3756578.5	-18293947.7	9996255-2	10487-083-	1368.783	67.521	41.8197	22.7318	-15.4166
174.5719	3775521.6	-18296367.0.	9986339+2 .	10563+274-	1324.443	32.73?	42.5326	24.4864	-15.6047
177.6067	3803502.3	-18799765.5	99.86275.0	1-676.500-	1255.^#	-9.671	43.3173	26.4759	-14.1392
180.2629	3832014.9	-18303(04.7	9986786.2	10792.281-	1143.658	-53.314	43.9939	27.0737	-16.3794
182-1240	38522#5.7	-18305172.0	9984157,9	10975-270-	1137.678	-73.923	44.5126	27.2460	-14.4571
1.84.8186	3881642.5	-1830A113.7	9985873.2	10995.641-	1058.702	-178.255	45-1612	27.7604	-16.5859
187.4952	3911280.7	-1831(851.2		11117-353	~953.588	-173.043	45.7996	28.1315	-18.7244
159.3322	3971736.7	-18312607.0	9985124.1	11201+622	-932.004	-Z03.816	46.3959	28.2944	-10.1820
192.0160	3961976.3	-1831506.5	9784516.*	11377.399	-833.55"	-249.039	47.1333	25.6771	-15,9054
194.6575	3992511.5	-18317196.5	9983787.6	11454.738	-775.184	-294.664	47.8341	29.0535	-17-7481
196.5295	4113577.5	-18319573.0	9953219-4	_11212.007.	-724.457	~37% 909	45.2578	29-0186	-17-0765
199.2150	4044751.5	-18320413.5	9982282.2	11675.765	-645.767	-372.125	49.1581	29.5566	-17+2450
201.9348	4074684.0	-18772059.5	9981205-1	11009.594		-419-231	49.8813	29.8633	-17.5860
293.7649	4098378.3	-18323-43-2	9987469.7	11900.286	-517-140	-451.132	50.5394	30-0913	-17.4880
206.4494	4130508.0	-18324303.5	4979135.4.	12736.831	-425.742	-498.371	51.3Z79v	. st. 4433	-11.04602





Table A-2. Reconstructed Ascent Trajectory, ECI Coordinates (Continued)

TIME		•							
ROM LIFTOFF	DY	D ¥		VY	~~	47			
(SEC)	PA	P 1	P 2					a r	A 2
209.1291	4162448.9	-18325343.^	9977776+2	12175.785 .	-345.730	-545.035	5?.1724	31.8375 -	17.8871
210.9611	4195342.9	-19325926,2	097671.5.6	12771.660 .	-789.969	-579.(8)	52.8526	11.0775 -	-18.0125
213.6447	4218456.2	-18326592.2	9975086.5	12414.762 .	-206.139	-627.678	53.6403	31.4659 -	-18.2101
216.3254	4251939.7	-18327031.0	9973338.2	12559.383	-121.115	-676.769	54.4742	31.8140 -	-18.4155
218.1574	4275040.8	-18327199.5	9972067.4	12659.019	-62.680	-710.685	55.2914	32.1416 -	-18.6201
220. 8470	43 9239.7	-18327251.2	9970091.0	12809.426	24.263	-761.234	56.17/1	32.5383 -	-18.9473
223.5518	4344261.5	-18327664.5	9967952.2	17963.371	113.296	-812.765	57.476	32.9979 -	-19, n62r
225.3928	4369115.9	-18326801.5	0056431.2	13-168.585	173.851	-847.802	57.8994	33.2791 -	-19.1749
228.0764	4403387.3	-18326214.5	9954086.6	12225.179	263.807	-899.609	58.8567	33.6980 -	-19.3736
230 757	4439051.8	-18325386.0	9961605.4	13384.134	354.702	-951.799	59.8402	34.0689 -	19.5606
232.601.	4463496.4	-18324677.7	9959626-6	13494.873	417-568	-987.978	60.6543	34.7231 .	19.6805
235.2815	45:11212.2	- 18373420-0	9957097.6	13659.205	51-1-1.97-	1341-489	61.796.2	34.9359	19,9959
237 CPar	453743	-19321018.	9254703.9	13828.234	6 6.187-	1095-971	62 8251	35.4448 -	20.2539
230 3430	4563140.0	-1932.1733.5	0357137.5	13945.387	672.1.91-	1133 703	63 2060	35 6776 .	20.3695
227.01	44 11 700 3	-103107/7 3	0049033 7	14137 013	771 601-	1100 626	46 6 4 6 1	36 6136	20 0441
272+3941	40 11 1	1031010102	0046430 F	14300 445	970 016-	1747 047	44 2010	37 0744	- 21 - 2247
240. 1010	404 201.2	1021/04/ 5	00(2000 0	14 300 . 0 3 3	070.910-	1303 (13	17 2004	37.00170	
247.1545	4000152.0	-18114840.0	9943290+0	14424.331	479.024-	1201.412	01.521.9	31,4942 -	-21.5157
249. 4545	473528 .5	- 18312160.7	9919722.2	140 8. 708	1.42.548-	1140.100	58.0/4/	38.1042 -	-21.8987
251.715	4733273+2	-18310165+7	0437103.1	14736.277	1113.532-	1487.249	69.0423	38.6678 -	-222276
254.4779	4113619.1	-1847/002.0	0911741.6	14921.333	1219-224-	1448.016	11.1151	39.3161 -	-72.6513
353 13/4	4014310 -	10202554 5	00303/3 /	15121 057	1274 000	1610 011	77 5010	AC 1004	- 12 0017
257.1159	4814315.2	-18303559+0	9929341.4	15121.977	1 320.039-	10194012	72.0170	46.1904	-23.0462
228.9965	4842404.8	-18351030.7	4420008.5	10/0/+020	14114 714-	1223.103	12.9110	40.1452	-23.4120
261.74.4	48847.03.3	-18297015.2	9922142.0	15462,506	1514, 164-	1614.196	75.4703	41.4614	-23,8173
264.4465	4926824.2	-18292763.5	9917675.4	15469.94A	1027.950-	1683.262	77.0190	42.248	-24.2553
266.2990	4555584.2	-18289675.	9914515.1	15912.762	1706.768-	1729.696	78.4154	42.8858	-24.6284
269.0179	4999158.1	-18294987.2	9909735.6	16027.984	1874.418-	1796.321	80.2665	43.7359	-25.1343
270.8596	5128975.4	-18281434.5	9906371.7	16177.289	1975.713-	1843.127	81.8475	44.4378	-25.5477
273.5735	5773083.4	-18276109.2	9901280.6	164 1.293	2027-070-	1913.127	83.6385	45.3490	-26,0648
276.7824	5117372.4	-18270444.5	9895995.6	16630.826	2151.342-	1984.727	85.5650	46.3917	-26.6696
278.1320	5148780.1	-18266385.2	9992278.7	16790.631	2238.181-	2134.552	87.5945	47.3282	-27.1980
280.8440	5194639.1	-18260141.2	9386660.1	17030.660	2347. 257-	2109.260	89.6795	48.3868	-27.8099
283.5930	5241747.2	-18253456.2	599.762.5	17279.868	2511.951-	2186.533	91.9185	49.5755	-28.4832
285.4445	5273952.2	-18248736.5	9876658.0	17452.447	2594.871-	-2249.2(1	94.1613	50.6826	-29.1036
288.1574	5321646.8	-18241593.5	9870472.7	17710.351	2733.670-	2320.025	96.5407	51.8040	-29.7654
296.7717	5367559.9	-18234293.2	9864400.9	17962.351	2868.905-	2397.893	98.8517	53.1171	-30.5098
292.4914	5393324.2	-18229161.5	9850123.2	18138.800	2953.522-	2452.441	101.5457	54.3350	-31.1900
295	5446445.3	-18221336.7	0853703.1	18403.275	31:5.174-	2534.113	114.5618	55.9240	- 32,0351
297.4486	5494740.9	-18213144.1	9847642.9	18675.843	3251 . 45-	2617-542	17.5085	57.3583	-32.8150
300.2248	5547712.7	-187 74576.7	9845 209 6	18956.685	3400. 75 7-	2703 407	110-5886	58,8513	-33.6366
302.8400	5507672 1	-18195479.7	08331 22.0	19251 302	3556.974-	2793.057	114.1791	AG. 5439	-34.5870
304 4037	5474804 7	-10100111 2	0078047 4	10455 405	3465 347-	2854 007	117.1733	62.1099	- 35. 4135
307 1039	5477365 3	-1013-111.2	0020667 0	10742 567	3837 407-	2047 002	121 7330	44 1225	-36 6172
301.1020	001/05040	-161/9446./	9720771.2	19/07 - 227	3911005 054	2947.49.12	121.19	64 1703	- 37 41 39
313.7024	57017/0 7	- 10104354	0004724 4	200.00.000	4173 300-	3144 405	120 9234	44 5000	-30 8026
212+25-1	5/51/62+1	-18103671+7	0700127.2	20417.050	4112.109	22144.492	124.0 20	70 44 26	- 40 6933
314+1438	541/9/2.7	-1815(200+0	4704121.2	2009/10022	429561424	-3214+312	1 14 . 34 90	72.0027	-41,021
316.7238	5871696.7	-18139886.2	9790699.2	50444.454	4479.925-	•3314•400	1 14. /834	13.3091	-41.7218
319.3.120	5925304.6	-18128091.0	d/ascu2.2	21 302.324	40/1.00/-	-342M+218	142.4490	12.9824	-43.111
321.0192	5642724.6	-18115601+5	9772990.1	21752.635	4913.156-	-3543.24/	144.8956	11.7858	-44."267
324.4957	6439213•3	-181/2781.2	9763607.1	22151.637	5180.344-	- 1660 - 417	157.5276	81.5732	-46+1358
326.2509	6078634.0	-18093682.7	9757064.4	27435,438	5226. 724-	3743.486	165.1293	85.3261	-48.1633
328.8420	5137549.1	-18079917.5	9747249.6	22 966 . 807	5449.309-	-3869.886	172.2437	88.8260	-49,9473
331.4592	6197536.0	-18-65337.7	9736939.7	23326.865	5686.640-	4003.877	179.6577	93.4852	-52.1695
334.0334	6258193.6	-1815/383.5	9726457.0	238:12.936	5933.973-	-4141.497	185.7511	98.0759	-54.3554
336.4865	5317152.2	-18-35-26.7	9716131.0	24265.651	6179.836-	-4777.978	191.5559	102.4502	-56.4383
337.5100	6342085.9	-18^29148.5	9711722.9	24467.908	6285.581-	-4336.443	193.9772	104.2751	-57.3773
338.4553	6365279.4	-18023167.?	9757651.6	24531.812	9333 008-	-4366.541	-6.8912	26.5691	-14.278P
343 344-			0101-F0 ·	A/F1					
341. 1047	Z - Z - Z - 4	-18996531.7	7070159.6	24517.377	0417.548	-4474.110	-0.9255	26.5099	-14.2964
343 4447	6487603.4	-11041194•S	1242030.1	24502.309	6474.425	-4437.975	-6.9568	20.4356	-14.3124
347.8420	6546324.7	-1/4/5636.7	96 14951.5	24484.188	4537.413	-4471.675	-7.9730	26.1403	-14.0872
348.12/3	5502086.2	-17060641.0	9664770.9	24464.320	6595.396	-4575.278	-8.7577	25.8918	-13.9231
351.4155	6657967.0	-17945521.0	9654401+5	24443.304	6555.214	-4534.939	+9.1942	25.7553	-13.7849
352.8869	6719592.9	-17928907.0	9643125.1	24419.979	6719,054	-4569.580	-9.4753	25.7419	-13.6775
355.3 110	6777516.4	-17912612.7	9632033.9	24396.905	6787.562	-4602.723	-9.6423	25.6270	-13.8303
357.5940	6837432.2	-17896997.2	9621443.7	24374.633	6839.561	-4634.397	-9.6585	25.5875	-13.7975
359.9055	6889748.6	-17881119.2	9610694.1	24352.008	6898.+69	-4566.451	-9.9687	25.5477	-13.7669
362.8020	6960743.4	-17861(29.7	° 9597119.9	24323.648	6972.695	-4705.317	-9.6754	25.6514	-13.8294
364.9836	7012294.3	-17845757.7	9586820.0	24302.072	7028.214	-4736.207	-9.4572	25.6650	-12.8399
367.1504	7:56164.2	-1783 23 97.0	9576477.0	24283.377	7:85.008	-4756.795	-9.7589	25.6766	-13.8675
370.0295	7135757.3	-17809964.2	9562743.6	24255.83A	7158.241	-4806.487	-9.6978	25.6135	-13.8441
372.2175	7189330.7	-17794096.2	9552096.9	24233.854	7714-688	-4837 .084	-11-1415	25.4073	-13 7334
374.4192	7242175.4	-17778296.2	9541511.0	24211-477	7269 014	-4866.775	-10-2067	25.2835	-17.4808
376.5570	7294930	-17762397	153 A75 9	241 88. 814	7325 164	-A996 - 695	-1/ .38CB	25.3719	-13.6565
179.5227	7365403	-1774 1863 5	9516406 1	74158.140	7300 564	-4936 445	-10 5287	25,3015	-13.6447
381, 2627	7421844 0	-17773563.7	95-4054 5	241 37 674	7459 610	-4040 344	-11 49202	25.2454	+13.4147
384.(914	7475455	-17706794.2	9493831 9	24109.742	7515 300	-4008 701	-10.5552	25.2916	-13-6124
381.9407	767 0380 7	-1760/1241 7	9493970 0	24084 204	7571 201	-4770+101	-10 4044	25.3784	-13.4000
300. 1031	1.25 4 5.24 1	107/2014	770201761	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	121104491	- 2720+274	-1:40044	C 3+ C 100	- 15+001.4





Table A-3a. Reconstructed Ascent Trajectory, Special Parameters

<i>,</i>	GEM	INI 8 ASCENT BE	т				1
TIME FROM LIFTOFF (SECONDS)	INERTIAL VEL. PAGNITUDE (FT/SEC)	RELATIVE VEL. MAGNITURE IFT/SECI	INERTIAL FLT. PATH ANGLE (DEGREES)	INERTIAL FEADING ANGLE (DEGREES)	ALTITUDE (FEET)	GECDETIC LAT. (DEGREES)	GEODETIC LONG. (DEGREES)
2.578	1341.8	23.3	.996	90.004	48.0	28.507	-84.555
5.121	1342.4	47-4	2.023	90.316	137.7	28.507	-8G.555
7.663	1343.6	72.5	5-093	90-037	289.7	28.507	~80.555
12.206	1346.6	121.6	5.181	90.C 8G	736.7	28.537	-80.555
14.835	1349.3	150.E	6-406	90.116	1643.7	28.507	-80.555
16.914	1351.5	175-0	7.437	90.163	1421.2	28.507	-80.555
22-422	1359.5	239.8	16-154	90.244	2477-2	28.507	-84.555
24.453	1365.0	273.0	11.530	90.278	3116.0	28.507	-80.555
26.487	1372-1	301.5	12.689	90.325	3682.0	28.507	-89.555
29.094	1300-3	380.7	15.628	90.513	4318+2	28.507	-86+777
33.696	1426.1	413.3	16.810	90.594	6247.7	28.507	-80.555
36.306	1457.8	457.8	18-207	96.736	7379.7	28.507	-80.555
38.295	1450.1	493.5	19.226	90.839	6319.C 9656.2	28.507	-80+334
43.519	1577.6	594.8	21.615	91.119	11112.5	28.506	-80. 553
45.508	1618.3	636.7	22-420	91.229	12304.C	28.506	-80.552
48.121	1677.5	695.3	23.391	91.410	13980.5	28.506	-80.551
52.720	1795.4	837.4	24.816	91.701	17242.	28.505	-60.547
55.330	1670.2	876.8	25-480	91.832	19274.7	28.505	-80.545
57.538	1950.4	950.5	26.045	91.966	21439.5	28.505	-80.542
59.929	2012+3	100940	20.342	92.197	25551.5	28.504	-80.535
65.147	2199.u	1175.0	27.012	92.394	28126.7	28.503	-80.530
67.138	2274.2	1242.3	27.131	92.548	30153.2	28.503	-80.526
69.767	2379-0	1335-4	27.181	92.665	32923-2	28.502	-80-520
72.362	2489.5	1434.3	27.154	92.749	35829.0	28.501	-40.514
74+354	2577.4	1513.0	27.104	92.924	38129.7	28.501	-80-568
76.565	2695.4	1621.3	27.066	93.242	41261.7	28.500	-86.586
81.565	2912.2	1825.6	27.131	93.755	47133.2	28.498	-80.484
84.177	3C43.C	1949.7	27.129	94.073	50678.5	28.497	-60.473
26.786	3181.C	2080.3	27.060	94.353	54375.5	28.495	-80-462
91. 392	3441.2	2326.2	26.86	94.805	61277.2	28.492	-80.439
94.002	3597.7	2476.2	26-648	95.047	65407.2	28.490	-80.424
95.554	3722.1	2594.9	26-457	95.213	68666.7 73085.7	26.489	-80-412
101-255	4071-9	2929.7	26-019	95.639	77727.0	28.484	-804378
103.259	4213.1	3.65.2	25.792	95.786	81335.2	28.482	-80.363
105.671	4405.2	3249.6	25.486	95.967	86217.7	28.479	-80.343
107-922	4260-4	3409.2	23+200	96.286	95325.7	28.473	-80-303
113.149	4981.0	3806.8	24.622	96.479	100664-0	28.470	-80.278
115.147	5151-4	3971.7	24.319	96.619	104653.7	28.467	-80.256
117.765	5383.2	4196.3	23.858	90+113	11349045	25.463	
122.428	5819.0	4619.1	23.102	97.001	123681.7	28.455	-80-176
125.046	6077.5	4871_4	22.695	97.133	126934.5	28.450	-80-143
127.663	6346-2	5134.4	22-322	97.264	133151.5	28.445	-80-108
132-284	6339.2	5627.4	21.713	97.457	144560.5	28.435	-80.040
134.523	7149.5	5924.1	21.351	97.625	151283.7	28.429	-79.999
136.504	7388.5	6159.8	21.154	97.715	156555.0	28.424	-79.966
159-529	7978.7	6481.5	20.853	97.829	163637.5	28-417	-79.921
144.186	8332.6	7693.3	20.349	98-031	176775-5	28-404	-79.883
146.873	8713.2	7469.9	26.076	98.146	184679.0	28.396	-79.779
148.874	9009.9	7764.C	19.878	98.229	190729-2	28.389	-79.736
153.493	574ū.2	3100+0	19.445	98.471	205270.5	28.350 28.373	-79.678
154.600	9925.3	8672.5	19.345	98.466	206879.7	28.369	-79.605
156.117	9973.6	5718.7	19-142	98.499	213850.2	28.363	-79.568
150.774	10057-7	8799+2	18,780	98.573	222361.2	20.353	-79.503
163.396	10216.4	8951.8	18.160	98.701	237309.3	28.335	-79.386
166.913	10309.1	9341.2	17.818	98.776	245592.5	28.325	-79-326
167.948	10379.4	9109-1	17.572	98.832	251664.0	28.317	-79.276
173.172	16576.2	9299.5	16-881	98.945	267863_7	28.306 28.795	-79.202
174.972	10646.0	9366-8	16.603	98.960	273357.5	28.267	-79-085
177.607	10750.0	9466.9	16.180	98.980	281299.7	28.275	-79-014
162.134	10934-4	9570+Z 9645-D	15.456	99.011	289181.0	28.264 28.754	-78-942
184.819	11047.2	9754-2	15.633	99.029	302401.7	28.243	-78-816
187.499	11162.1	9865.6	14-615	99.046	310004.7	28.231	-78.740
192.017	11242.4	9943.5	14.333	99.057	J15128.2	28.223	-78.667
194.697	11464.9	10179.6	13.523	99.093	329773.7	28.197	-78-531
196.530	11570.1	10262.7	13.253	99.100	334654.7	28.189	-78.477
199-215	11697.5	10387.2	12.641	99.116	341699.2	28.175	-78-396

.



-CONFIDENTIAL-

Table A-3a. Reconstructed Ascent Trajectory, Special Parameters (Continued)

TIME FROM LIFTOFF (SECONDS)	INERTIAL VEL. Magnitude (FT/Sec)	RELATIVE VEL. MAGNITUDE (FT/SEC)	INERTIAL FLT. PATH ANGLE (DEGREES)	INERTIAL HEADING ANGLE (DEGREES)	ALTITUDE (FEET)	GEODETIC LAT. (DEGREES)	GEODETIC LONG. {DEGREES}
201.935	11829.5	10516.3	12.470	99.132	348699.2	28.162	-78.313
203.765	11919.8	10604.7	12.213	99.143	353334.7	28.153	-78.257
206.449	12054-8	10737.0	11.838	99.100	366573-5	28+139	-78-174
210.961	12288.7	10966.8	11.222	99.189	370975.7	28.116	-76.030
213.645	12432.3	11168.0	10.865	99.207	377315.2	28.102	-77.944
216.325	12578.2	11251.6	10.513	99.225	383517.7	28.088	-77.795
220.843	12832.0	11501.9	9.935	99.259	393678.0	28.063	-77.705
223.561	12989.3	11657.1	9.595	99-280	399613.0	28.048	-77.613
225.393	13097-2	11763.7	9.370	99.295	403539.2	28.038	-77.549
228.076	13427-6	11922.9	9.045	99.337	414689.7	28.007	-77.361
232.591	13537.4	12199.0	8.513	99.352	418383.7	27.997	-77.296
235.280	13708.4	12368.3	6.205	99.375	423693.7	27.981	-77.198
237.588	13884.8	12543.2	7.901	99.397 09.414	428910.2	27.953	-77-030
242.554	14193.9	12849.7	7.397	99.438	437485.0	27.936	-76.926
245.301	14381.4	13035.8	7.107	99.465	442349.7	27.919	-76.823
247.155	1451211	13165.6	6.913	99.483	445605.2	27.908	-76.751
249.864	14843.6	13494.9	6.442	99.530	453356.2	27.878	-76-571
254.428	15046.9	13697.0	6.169	99.560	457790.Z	27.860	-76.462
257.137	15255.U	13904.C	5.901	99.590	462086.7	27.842	-76.352
258.987	15400-1	14048.4	5.720	99.612	464944.0	27+829	-76.275
261.743	15620.0	14489.2	5.203	99.677	473018-0	27.791	-76-045
266.299	15998.3	14643.8	5.032	99.700	475635.5	27.778	-75.965
240.011	14231 3	14076 4	4 744	00 375	470764 7	17 764	-76 447
279.860	16393.1	15037.1	4.621	99.759	481813.0	27.744	-75.765
273.571	16636.5	15275.7	4.385	99.796	485307.0	27.724	-75.643
276.282	16886.4	15528.9	4.152	99.833	488669.2	27.703	-75.520
278.132	17060.9	15702.8	3.995	99.858	490884.7	27.589	~75.434
283.590	17596.4	16237.0	3.546	99.938	497056.7	27.645	-75.176
285.445	17785.5	16426.0	3.397	99.967	499028.0	27.630	-75.087
288.157	18069.7	16709.1	3.183	100-008	531795.7	27.607	-74.954
290.132	18347.4	10986.3	2.983 7.84F	100.049	505929-7	27.570	-74.820
295.671	18834.7	17472.7	2.654	100.120	508219.5	27.547	-74.605
297.649	19136.6	17774.1	2.464	100.162	510381.5	27.524	-74.471
300.225	19448.1	18085.3	2.278	100.206	512413.0	27.501	-74.334
304-404	20062.4	18439-0	2.099	100+251	515571.5	27.460	-74-193
307.184	20344.5	18980.6	1.796	100.328	517257.2	27.435	-73.954
309.763	20699.3	19335.0	1.623	120.374	518810.2	27.409	-73.808
212.300	21673.3	19708.6	1.451	100.422	520250.2	27.383	-73.657
316.724	21727.2	27362-1	1.173	100.504	522331.2	27.337	-73.401
319.302	22137.2	20771.8	1.013	100 553	523382.0	27.310	-73.245
321.919	22571.8	21206.1	.855	100.605	524306.2	27.281	-73.083
324.495	23019.6	21653.7	.705	100.657	525076.0	27.252	-72.920
328.840	23823.6	22457.2	.459	130.747	526057.0	27.201	-72.638
331.459	24341.6	22975.0	.313	106.802	526450.0	27.169	-72.463
334.033	24878-6	23511.9	•169	100.054	526484.2	27.137	-72.288
336.487	25403.0	24036.1	.628	100.904	526759.2	27.106	-72.116
337.510	25627-1	24260.1	031	100.926	526745.5	27.093	-72.044
338.455	25711.3	Z4344.3	053	100.954	526711.0	27.081	-71.976
343.445	25728.9	24362.0	053	161.121	526527.5	27.015	-71.619
345.842	25733.4	24366.5	052	191.252	526439.7	26.983	-71.448
348.120	25735.2	24368.3	051	101.285	526357.0	26.952	-71.286
3564445	25/35+8	24369.0	049	171.357	526275.7	26.921	-71-122
355.301	25736.6	24369.7	046	101.524	526104.5	26-854	-76.773
357.594	25736.8	24370.C	045	101.602	526026.5	26.822	-70.610
359.905	25736.9	24370.1	044	101.683	525948.0	26.790	-70.445
364. CP4	2213163	24370.8	043	101.952	525851.5 525780 #	20.749	-70-239 -70-084
367.160	25741.1	24374.4	040	101.925	525710.5	26.687	-69.929
376.030	25742.8	24376.1	038	102.022	525619.2	26.646	-69.726
372.238	25743.5	24376.9	037	102.097	525550.5	26.614	-69-569
374.419	25743.6	24317.1		102.170	525484.0	26.583	-69.260
379.523	25743.7	24377.2	033	102.345	525333.2	26.508	-69-052
381.853	25743.8	24377.2	031	102.418	525265.7	26.473	-68.887
384.091	25743.9	24377.4	030	102.492	525202.2	26.440	-68.729
386.270	25743.9	243/7.4	029	102.565	525042.0	26.407	-08.575
						203 304	





Table A-3b. Reconstructed Ascent Trajectory, Special Parameters

	GEMIN	E & ASCENT BET			
TIME FRUM LIFTOFF (SECONDS)	RELATIVE FLT. PATH ANGLE (DECREES)	RELATIVE HEADING ANGLE (DECREFST	INERTIAL LONG. (DEGREES)	GEDCENTRIC LAT. (DEGREES)	RADIUS TC EARTH CENTER (FEET)
3. 674	e9.165	-116.584	-23-533	28.346	20909011-5
5.121	89.332	-141-238	-80,520	28.346	20910003.2
7.663	89.267	-142.239	-80.569	28.346	26910155.2
9.736	89.231	-159-658	-80.500	28.346	20910327.7
12.206	89.014	-157-674	-80.490	28.340	20910602.2
14.635	68-6C2	-155,455	-80-470	28.346	20911286.7
19.471	88.519	-152.136	-80.440	28.346	20911774.0
22. 222	88.346	-148-492	-60.449	28.346	20912343.0
24.493	88.320	-147-189	-80.439	28-346	20912975+7
20-931	88.401	-170-807	-80.432	28.344	209143297+7
31.740	87,452	134_159		28-346	20915322.7
33.696	86.281	123.907	-83.453	28.346	20916113.7
35.306	64.254	114.298	-83.389	28.346	26917245.7
38+295	82-547	109-891	-60,380	28.346	20918185+2
43,519	77.477	100-202	-80.357	28.345	20920979-0
45.508	75.797	162.476	-80.348	28.345	20922178-7
48.121	73.285	301.446	-89.336	28.345	20923847.5
59.129	76.768	1.0.649	-80.323	28.344	20925647.5
52.720	68-959	100.020	-60.313	28.344	209271(9+5
776330 47.538	64.287	58.712	-50,286	28.343	20931358.0
59.929	62.551	56.339	-80.275	28.343	20933052.7
62.540	66.345	\$7.555	-80.260	28,343	20935459.7
65.147	58.209	57.854	-30.244	28.342	2-1937996-5
67.13B	26+ 745	57.802	-8J.232	28.342	20990023.5
49.767	54.445	97-567	-80-215	28.341	20942794-2
72.342	52.404	97.181	-80.197	28.340	20945700.5
74.354	50.507	\$7.242	-82.184	28.340	20948002.0
76.565	49.152	\$7.540	-80-165	28.339	20951135.0
79.572	41.164	71.013 67.657	-80.143	28.337	2095900100
84.177	45.373	58.234	-80.127	28.335	20960555.0
£6.786	44.676	56.426	-80.085	28,334	20964253.5
88.779	43.656	58.514	-83.667	28.333	20957181.5
91.352	41.632	58.677	-83.643	28-331	20971150.2
99.002 65.684	76.766	70.00V 56.564	-79,998	20+327 28-328	20978551.5
96.668	38.667	58.953	-79.97.	28.325	20982972.7
141.255	37.553	99.529	-79.941	28.323	20987616.5
103.250	36.731	99.074	-79.918	28.321	20991226.7
105.871	35-661	59.123	-79.886	28.318	20996112.2
1.5.636	34.740	47.100 66.734	-79.821	28-312	21005226-0
113.149	33.634	99.316	-79.791	28.309	21010508-0
115.147	32.285	99.374	-79.763	28.306	21314765.5
117.765	31.312	55-417	-79.724	28.302	21020401.5
120.366	364145	990431 88 441	-79.669	20.290	2102018902
125-040	28.774	59-471	-79.607	28-289	21036858.2
127.663	27.599	99.508	-79.561	28.284	21643080.5
129.665	27.441	95.537	-79.524	26.280	21047957.7
132.264	26.757	\$5.590	-79.474	28.274	21054459.7
134.503	- 26-116	99.C30	-19.422	28.205	21001229.2
136.504	25.645	95.666	-79.380	28.263	21666565.5
\$39.524	25.067	99.723	-79.324	28.256	21073595.6
141.563	24-638	99.734 cc 177	-79.278	28.251	210/9260.5
144.180	23.4(3	57. 111 69. \$72	-79-151	28.235	21094658-2
146-874	23.24	95.855	-79.102	28.229	21100715-2
151.496	22.767	99.902	-79.031	28.220	21106877-2
153.493	22.456	\$5.537	-78.976	28.213	21115272.7
154-660	22.274	55.557	-78.945	28.209	21123847.6
1700117 158-736	220C31 21_59A	100-050	-78_826	28.193	21132383.7
160.774	21-264	1CC.102	-78.767	28.185	21138960.7
163.396	20.837	166-170	-78.690	28.175	21147350.2
166.013	20.426	100.238	-78.612	28.164	21155644.5
167.946	20.121	100-269	- 18.334 -78 474	200220 28.145	2110172440
173-172	19.284	100.382	-78-396	28.134	21177946.0
174.972	18.952	1GC.387	-78.340	28.127	21193447.5
177.607	18.446	166.390	-78.259	28.115	21191401.5
183.263	17.939	100.393	-76.175	28.104	21199294.7
182.134	17.585	100-393	-/8.116	25.395	21217534_7
104.019	17.L82 16.587	100.373	-77.943	28_071	21220151.7
189.332	16-254	100.394	-77.882	28.063	21225283.7
192.017	15.772	100-393	-77.794	28.650	21232690.2
194.697	15-297	100.393	-77.704	Z8-037	21239955.0
190.330	14.978	10L+ 392 10G- 302	-11.042	284027	21251902-5
4770667	140311	4000 372	-114220	LOCVAU	





Table A-3b. Reconstructed Ascent Trajectory, Special Parameters (Continued)

3150-6036-R8-000

Page A-10

201.935	14.657	166.391	-77.456	28.(02	21258916.2
233.765	13.755	166.392	-77.392	27.993	21263561.0
206.449	13.316	it C.392	-77,297	27.980	21270264-7
209.129	12.866	101.394	-77.201	27.966	21276827.2
210.561	12.596	100.396	-77.135	27.957	21281239-0
213.645	12.179	166.399	-77.037	27.943	21 287592.7
216.325	11.776	166.462	-76.938	27.928	21293809.7
218.157	11.495	103.405	-76.879	27,919	21297984.5
220.843	11.097	11.0.412	-76-769	27 904	21203004.7
223.561	10.74	1(1-418	-76.665	27 890	21300046 0
225. 193	16.443	106.423	-76-564	27 976	21313001 7
228.076	10 648	100.425	-76 699	17 044	2131300107
230. 757	0.702	100 437	-76 383	17 84 9	2131933903
732.601	0 455	100 447	-76 310	27.040	21323002.1
235.280	0 102	100 451	-76 201	27.030	21328/08.0
237. CAR	9 752	1004451	-76 001	27.022	2133909940
230.847	6 516	100 447	-76 014	27.808	21339327+0
242.664	9 176	100 479	-75 800	27.194	21342834+3
245.101	7 845	100.403	-75 794	27.777	2134/930.2
247.155	7.424	167.501	-75 704	27.700	21392812.0
3/0 444	7 364		-75 507	21.149	21326079.5
241 215	7 / 96	100 677	-75.507	21.131	21300141.1
354 439	4 795	1020321	-73.300	27.719	21303860.2
767 127	4 477	100 640	- (3.305	27.101	21308312.5
2210121	4 373	100.502	-/3.204	27.003	213/2027-2
230.101	0.2/3		-75.179	27.071	21375497+2
201.444	3.710	100.095	-15.053	27-652	21379656.0
204.440	5.691	100.015	-/4.926	27.632	21383609.7
200.299	5.499	100.031	-74.839	27.619	21386240.5
209.UII	5.223	100.653	-14.709	27.600	21389979.2
270.850	5.039	166.669	-74.619	27.586	21392451.7
273.571	4.775	106-654	-74.486	27.566	21395966.2
275.282	4.516	100.726	-74.352	27.545	21399349.2
278.132	4.341	100.737	-74-258	27.531	21401579.2
280.844	4.692	166.766	-74.120	27.509	21404736.0
283.590	3.844	100.794	-73.978	27.487	21407794.7
285.445	3.679	100.815	-73.880	27.472	21409781.2
288.157	3.442	100.845	-73.736	27.449	21412571.7
290.732	3.222	100.875	-73.597	27.428	21415092.0
292.491	3.074	100.856	-73.501	27.413	21416742.7
293.071	2,861	100.528	-73.358	27.390	21419055.2
297.649	2.653	100.559	-73.213	27.367	21421240.2
300.225	2.449	160.992	-73.966	27.343	21423295.2
362.840	2.249	101.026	-72.914	27.319	21425250.7
334.634	2.116	101.050	-72.811	27.302	21426495.0
307.184	1.925	101.085	-72.657	27.277	21428205.5
305.763	1.738	161.120	-72.500	27.252	21429784.0
312.380	1.552	101.157	-72.338	27.226	21431250.2
314.144	1.428	101.183	-72.228	27.208	21432159.7
316.724	1,252	101.220	-72.064	27.181	21433376.2
319,302	1.080	101.259	-71.897	27.153	21434454.7
321.919	.910	101.299	-71.724	27.124	21435407.5
324.495	.749	101.340	-71.551	27.095	21436206.C
326.261	.642	101.368	-71.433	27.075	21436673.7
328.840	.487	101.411	-71-251	27.045	21437237.5
531.459	.332	101.454	-71.065	27.013	21437661.7
334.033	.178	161.453	-74-878	26.982	21437927.7
336.487	-03C	101.533	-70.697	26.950	21438033.5
337.510	032	161.549	-70.620	26.937	21438032.7
338-455	656	161.577	-7.1.548	26.925	21438010.5
341.065	56	161.669	-70.351	26.891	21437948.7
343-445	056	101.754	-73-171	26.859	21437892.0
345.842	655	101.839	-69.989	26.827	21437835.7
348-120	053	101.926	-69.817	26.797	21437783.5
356.405	652	162.603	-69-645	26.766	21437732.5
352.AR7	-,651	162.693	-59,457	26.732	21437678.0
355. 301		162-180	-69-275	26.699	21437627.2
357. 194	048	102,262	-69,102	26.667	21437580.2
359 905	647	102-345	-68-928	26.635	21437533.5
367.802	045	102-449	-68-710	26-595	21437476.7
364.484	- 643	162-527	-68-545	26-564	21437436-0
347.140		162-404	-68.297	24.533	21437396-2
370.030		102,707		26.492	21437345-5
172.314		102,784	-66.100	26.461	21437507-7
374 410	-/ 27	105.443		24.479	21437272.2
374 800	036	162. 641		26. 307	21437238-2
710+790	/ 24	167.644	-010012	24-155	21437194-2
3176743		167-194		24. 120	21437160-5
2010022	(32	163.205	-47 11.1	26.287	21437129-2
384 370	036	103.282	-64-947	26.254	21437103-7
300 147		103.102	-44 313	24.211	21437064-2
2070191	-1427	1436303	-00+134		**********





APPENDIX B

REENTRY TRAJECTORY

The reentry trajectory is provided in two sets, the earth-centered inertial coordinates and the special earth-referenced coordinates. The inertial set has the z axis aligned with the earth's rotational axis, positive north, and the x-y plane is in the equatorial plane with the x-z plane containing the Greenwich meridian at the time of retrofire (17 March $2^{h}45^{m}49^{s}$).

Tables

Page

B-1	Reconstructed Reentry Trajectory, ECI Coordinates	B-2
B-2a, b	Reconstructed Reentry Trajectory, Special Parameters	B-12





431 5747 1	1 1 2 3 7 4 25	17437677 5	67-9758 61	-21577.35	9466.91	9223 . 32
631.142	1 1 3 1 7 4 5 7	1			04.30 37	
633.9746 1	12961226.53	1746 2275.5	675 364	#210124 (P	9420 .1	014/.//
636.3674 1	0909628.97	17492803.25	6772291.00	-21649.67	9371.41	9175.57
439 7744 1	467221 37	17555356 00	6704434	-21686.03	9313,15	9152.87
C30.1144 1	•			21721 60	0355 01	0130 60
641.1454 1	8 5774 87	1/52/405.50	6816115.60	-21721.34	4733.4	415 . 39
643.5493 1	1753602.50	1754655	68380	-21757.14	9197.75	91 7.82
A45 0407 1	17. 344 67	17671553.75	6850331.44	1792.87	0130.4	9085.07
043.74-2				- 11070 5	2081 1	0043 33
648.3496 1	143591.11	1/593422.0	6801411.65	-21916+ ·	Strie L.	01.62.22
A51.7495 1	596553	17615145.75	69 3732 56	-71863.6	9727.71	9039.20
		17435314 50	4018440 10	-21887.9	8081.03	90 23 15
002.4275 1		103 2174		21012 01		
655.5215	10492565 • 6	17657924.50	6946358.1.		HAL.0*45	8004.42
657.9214 1	1.420386.53	1757 72 29.4	A967913.81	-21967.57	3849.5	897.37
	1101010	177154/1 55	4 7 9 7 4 4 7 3	-271 52.53	3799 44	9944 94
00.03440						13-0.04
662.7495 1	1123156.75	17721662.51	7.1111 .6.	- 22 30 . 9 3	1129. 11	8921.38
665.1494 1	A 280229.12	17742547.50	7032498.00	-???71.19	3670.97	9902.12
(() 6403	2227230 50	17762281 25	7053970 37	- 22105.33	8612 (13	9976 73
001.3493	1927 - E. 17 - 71	1 0 2 1				3310113
669.9214 1	L2174744.62	1778364. 25	1. 14628 903		120.1001	8825.00
672.3213	1.121577.62	178 41 07, 25	7 96 77 12	-72177.70	8494.59	8829.91
474 7010		17074417 6	7117220 75	- 22225 94	2435 54	0004 34
C/4./212 1		1,9,000,000				04.16.54
677.1216 1	1.14979	17844589,75	7138349,81	-77710,74	9376 1	9782.51
670 5715	9941567.12	17964623.5	7159308.31	-22272.41	3316.97	8758.63
0174.721.5		1004560 35	7100000 65		0.057 50	0704 74
681.9214	99° H' 76•12	1994-1 1 20	1191344.51	-22313.22	5277+24	01-4.14
684.3354	9954189.75	79-4371-25	7251445.69	-77338.55	9197.7 ^	8710.70
494 7405	091 222.62	7914 98.75	7222445-69	-22371-21	8137.83	8686.52
689.1215	974 / 10 . 30	1104 4427.	1.41.11.427	/24 ***	8. 1H* 34	800/ +71
691.5215	3403315.1	17962633.53	7263782.75	22435.54	Rf 19.23	8638.57
602 0214	9639633 75	17081813 75	7786685 10	.77467.71	7959-51	9616.16
042.4/14	4423422.	179916156	1		7477421	
696.3213	958-474.11	1455643.25	73 51 Zu • 17		1894.55	8584.84
698.7717	9531430.17	13719779.75	2325714.75	-22531.50	7879.83	9565.54
0,00,012						
770 0404	2404763 75	10133445 5.1	373641 10		7799 19	8548.00
1011-2480		13 32 47367			7710 10	0.4017
703.5493	9422500.50	19357293.	366951+19	-22595.7	7719.12	4515.JZ
715.0402	9369237.11	18175743.05	387359.56	-22626.32	7658.94	8491.51
1. 2. 2. 2.				- 224 57 20	7500 44	8444 77
718.14-6	931 3887 • 75	19//44/22*/	* //12.81	-2203/+24	1340+64	5400.17
717212	074 117.97	18112005.5	427763.56	-22687.88	7539+21	9447.41
717 1914	03 5431 5	19130131	447009.91	-7771P-43	7478.07	9417.57
112-1215	••••	1913. 5.4	++ / + - / /	= , , , , , , , , , , , , , , , , , , ,		
715.5215	9151 67.51	191479 6.	468171.12	-22749.21	7418.44	9 465 • 21
717.9412	2105796.25	19165847. 1	109514.71	-27779.97	77 7. 33	8367.30
7210.102		10103430 75	E. 0.240	-1101/ 47	7206 73	8367.76
72. • 1400	9147.14.31.	14143424.74	- 3009+11	-22011 . 7	1240.11	337/ 620
722.7495	89863 1.25	19237 868.50	528559.6C	-27840.27	7236+28	8317.29
775 1404	9331461 25	10710147 27	548483 81	-22869.90	7175.54	32 91 . 84
12741-94	4-31-47.467		141483.01	22000 (2	7114 61	1744 44
727.5403	29765212	187347 0.74	PUBA20*10	-27890.62	114.44	1200 + 00
729-9214	9922176	10252115.51	597036 81	-22928.75	71 54.73	424].74
723 3354	87/ 4 780 0	19740172 35	4. 7034 13	-72059.23	22.5004	8214.29
1224 2224	1167 / 974	1020 112027	0			
734.7495	P711337.62	19295881.25	627617.81	-27997.73	6932.2	1147.04
737.1464	8454127.87	18372445.25	1647233.94	-23016.49	6871.33	9165.11
		103100(3.35	7444 700 40	-11045 10	1017 25	3130 66
139.5443	20(010-01	1801-6024 10	1000135023	- 4 3 · • · • 30	10100	31.27.000
741.9492	8545515	10335113.5"	76.85301.04	-23. 23, 91	5748, 19	3113.70
744 3404	9400 2 04 50	10251752	7705767.76	-771 17, 35	56P7.77	8087.86
144.24.24						0040 04
746.7475	P124517.37	19307235.05	1120120+12	<u>-212 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1</u>	2013.02	1.00
748.3496	8307614.11	18777799.75	77285-34.44	-23149-16	6585.72	8144.67
751 5403	00000443	1 1 1 1 1 1 1 1 1 1	7749407 76	-12186 52	45.12.05	8010.20
131.3423	412 34C1 . C	1 1 1	1.0.2.2.2.1			700/ 00
753.9492	9267787.57	19414283.	778740 .75	-23214,15	0442.70	1984
756.2496	9712 74.57	14470671.75	781 71 74 10	-23241.45	538° . 78	7958.13
750 7405		10111011	7031.001 54		6310 26	7031 08
178. 1499	8155 (TA+ 1	1943401	1951.414.46	-22200.20	0313.34	1711.440
761.1494	41 34 12	18461115.25	704 304 10	-22296.11	6257.61	7905.84
743 5403	4 44 200 31	13474049	7853537.75	-73723-16	6196.12	7879-47
102.7472	• • • • • • • • • • • • • • • • • • • •	19414			(10) (1)	7053 00
765.9492	7994393.69	18480745.00	7877025.06	-23380.07	6139.9	1822.128
768.3496	7332312.A7	195*4395.75	7896734.69	-73376.76	6177.53	7826.59
10003470						
77. 7405	7876170 34	19518825 5	7915696 13	-224 3-12	6112-70	7801.71
11/01/07/2		707170720	19-297-12		504 P 7	****
773.1494	/ 91 25 93 • 75	18533245.75	7924173.62	-23424.3	7797.1	
775.5493	7763775.16	19547447.75	7352797.19	-23455.12	5486 .78	7746.92
777 0407	770 74 53 40	10541501 75	7071256 04	-23681.76	5824.86	7722-16
111.747/	101 14 2.09	1001011020	1711-70074		8747 19	7603 85
780.3354	7551341.75	19575327.1	7000747.25	-27500+57	2/05+1/	1093.07
782.7495	7504564.44	LASAC163.75	8.57.87.87.50	-23532.22	57/ . 40	7566.64
785 1404	7530 50 15	1947 3743 75	0 7 7 4 5 4 4 A	-77657 14	5638-28	7639.74
102-1404	1127 77.12	107 6167017	5 20739.99	- 1 2 2 2 4 2 -		
787.5493	7481403.57	18516225.5.	9144855451	-22582.49	215.97	20.2101
789.0407	7426 967.62	18620521.55	8163193-94	-73617-46	5512.73	7585.85
	774 01	10443403 77	0.01000.10	- 734 77 44	6451 14	7868 60
192.3496	1.031 4. 924	1304/0414/3	6 6124 PTS	-23032.40	27210.27	
794.7495	7311425.50	196557/1.25	8059477.44	-73656.99	5338.76	7531.51
796. 7804	7777611. A	186.645 4.75	8111814.75	-77677.77	5346-16	7512.78
17002 070		10401014 75			6747 80	74 77 01
799.5493	1197750.93	1898-264.75	31 06 -17	-216"3+43	2201-77	
801.9402	7143841.25	18693824+5	9152477.19	-23729.49	5201.32	7449.49
804.3404	7183951.54	18776234-53	P171254 .C7	-73753.32	5138-59	7422.07
777402470	100101400		* 1 * 1 2 7 0 11 *	-27127031	E/ 76 90	7704 44
806.7495	7725817.62	18718491+25	9189035.31	-73776.93	DL 7.7 . 79	1 574 . 00
809.1494	5969727.12	1973 577.25	820 6748.56	-23800.41	5(13.07	7366.95
	411 25 PC 44	18745653.00	8774705 51	-73823 73	4051.37	12 20 . 62
BTT*5423		1977/707401		-1-02017		
813.9492	69 5378,12	18756359.00	8241976.06	-23846.82	4887.50	/311 . 67
816.3404	6799109.10	19766014-25	A259493_69	-23860.57	4824.59	7283.93
010.0490		10777617 34	8374041 10		4741 81	7284 17
818.7495	0141 147.25	10///71/427	P210941. 10	-23892.41	4101071	100014
821.1494	6683435.69	18788869.77	8294321.36	-23914.95	4698.65	7.28.27
822.8402	4424010.50	18800069-55	8311635 - 9	-23937.11	4635-61	7 200 - 34
02342473	0.02.0.2.0.00		475642774; 7 6336665 * 6	22077 24	4573 45	7179 98
825.9492	4549537.19	TAN11118*1.	8-28MH1+15	-23959.25	927 (+92	1116+27
828,3354	6511338.81	1#821955.0r	8345963.44	-73981.12	45.19.77	7144.55
A3A 74A*	4453674 47	18932745 25	8363176.40	-24032 00	4444 . 41	1114.27
6JC+.7495	042.24." +04_	17726197615	0707610907			10021
833.1494	6395790.00	18843363.00	9380221.12	-24024.58	4382.87	1087 .99
835. 5407	6338167.62	18853802.75	8397197.62	-24046-04	4319.78	7059.68
00000470		10044003 75	8414104.35	-24047 82	4256-41	7031 . 44
83749492	.02012279+22	1000-5720(2	07474796 <u>6</u>			1.1.1.1.40

(FT)

TIME (SEC)

Table B-1.Reconstructed Reentry Trajectory,
ECI Coordinates

7 (FT

4 (FT) XDOT (FT/SEC) 17

YDOT ZODT (ET/SEC) (ET/SEC)



TIME (SEC)	¥ (FT)	Y (FT)	7 (=T)	X007 (FT/S50)	VDCT (FT/SEC)	ZDOT (FT/SEC)
214-0234	18381314.00	11591455-12	2747131.75	-13-41.49	17970.64	11870.54
216.4233	18347934.25	11634442-12	3269435.37	-13111-15	17601.81	11831.95
220.4385	18318749.25	11704151.17	2294527.84	-12159.05	17854.47	11824.87
223.5996	18255292.75	11762412.62	7357253.72	-13278.62	17778_47	11879.62
225.9585	1 8 22 3? 54. 75	11905033-12	73P 584.16	-13737.47	17745.09	11871.71
228.3944	14101274.77	11 847561.67	2479899.#4	-13306.80	177-1-84	11796.01
233,1482	18126688.00	11932341.37	2421194.87	-13456.38	17653.11	11778.73
235.5986	18 194176.50	11-74649.62	2494733.53	-13573.67	17585.87	2377 . 69
237.9585	18261530.50	12216758.02	252297	-13632.48	17546.81	11762.06
247.7983	17995816.50	32152821.75	7551188,50	-1760.98	17517.69	11753.59
245.1982	17962749.00	12142665+62	26.7563.53	-134^7.91	17479."8	11736.98
247.5986	17979534.50	121 84455.75	7635726.67	-12866.22	17389.50	11725.44
249.9585	17945187.55	12726141.25	7663863.37	-13924-21	17349.85	11719.81
254.7993	17329-74.75	123-9226.00	2720173.53	-14745.39	17275.30	11772.13
257.1982	17795219.75	1235/624.75	2748146.01	-14/ 98.43	17237.6	11693.31
259.5956	17761398.51	12391935.25	2776214.62	-14156.71	17189.78	11684.31
261.3584	17603175-50	17432140+75	2804734+75	-14213.72	17140.54	11675-75
266.7953	17559856.50	12515262.62	2860229.41	-14328.89	17068-45	11656.49
268.4385	17675323.25	12542232.50	7979341.66	-14767.95	17641.77	1165.39
271.5586	17589799.75	12594004.47	2916338. R4	-14643.44	149R6.95	11637.81
276.3984	17523199.75	1201/110+2	2971051.75	-14557.39	14004 54	11678-10
278.7983	17485195.00	1271 6655.12	2999823.59	-14614.49	16863.39	11608.94
281.1982	17450053.75	12750275.87	3127672.12	-14671-11	16821.96	11599.11
283.5986	17414769.00	12799575.12	30555.7.67	-14778.07	157#r.25	11589.20
285.9985	17379355.25	12439526.12	31 973 3.41	-14784.55	15738.69	11579.07
288.3984	17343916.00	12379947.12	3111070,94	-14841-04	16656.79	11568.97
290.7983	173 5121.25	12919967-12	3135832.25	-14597.43	14637.79	11556.38
295.5986	17236339.75	12000712.5	7104255.75	-15:09.75	1657/ .19	11538.18
297.9985	1722-251.24	13(19479.12	3721046.77	-15-64.74	16578. 9	11527.73
300.3843	17164240.25	12075223-37	3249435.87		16485.77	11517.23
305.1982	1712/55%-55	131187786.67	33/ 6827.72	-15233.29	16650,00	11405.79
397.5986	17054544.00	13197781.75	3332408.87	-15788.88	16357,12	11484.87
319.9985	17117785.50	13236445.75	3359958.47	-15344.41	16314.19	11474.**
312.3984	1499-994. "	1327555.37	3367461.72	-15300.77] A77]	11457.97
316-4385	1401940 .75	13341174.07	1431754.21	-1492.81	16198.73	11444.17
319.5086	16 96 9417.00	133-2273.00	3469996.31	-1**65.74	16147.78	11429.38
321.9985	16831996.25	13437956-62	3497311,75	-1562	16046.88	
324.3984	15794444.25	13469535.17	2529544.FF	-15779.43	16010.34	11394.50
329.1782	16713946.25	17544274.25	2870303 -	-15783.01	15-65.17	11383.25
331.59R6	1658)091.75	13584646.03	36 16703.25	-15839.49	15921.16	11379.54
333.9085	16642917.25	13622802.00	3633779.56	-15992.80	15876.51	11359.63
338.7C83	103 9/11+3/	13698793.00	3488446.57	+15"-1.27	15787.5	11335.79
241.1582	165279 9.50	13736624.**	3715434 64	-15:55.01	15747.87	11323.52
343.5956	16459376.57	13774363.75	3747477.01	-151 8.91	- 14604.13 -	11311.43
345.9505	16457587.59	13819083.17	3796876.51	-162152.56	15658.18	11286-80
350.7993	16372749.12	13846893.01	34241 18.28	-14769.57	15562.75	11274.15
383 1003	14333436 87	13074103 87	2001153 70	-14222.64	18617.33	11241-40
355-5985	16794394.75	13961385.62	2878167 28	-16776-17	15471.93	11249.46
357.9985	16255229.87	13008461.87	30 5148.50	-14429.78	15426.14	11236.28
360.3584	16215537.75	14"35478.5"	2932099.12	-16482.15	15386.66	11223.39
362.7983	10177918.37	14772287422	3977398.76	-15555-00	15303.09	11211-497
367.5586	16 96797.5"	14145674.75	4 12769	-1644".4"	15242.37	11184.75
369.9985	16:55294.12	14192199+62	4: 3959*.22	-14492.93	15194-74	11171.28
372-3984	3671617425	14718613-62	4766389,31	-15745.03	15157.70	11155-20
377.1982	15935546.00	14291107-37	4114981.12	-16849.63	15756.96	11131.19
379.5586	15495-37.87	14377103.62	4164583 RT	-16911.57	ser 15 . 3	11117.48
341.07.2	35854894.01	14362735.12	4177934.12	-16047.59	14963.65	11164.19
354.3984	1231300546Z	14434755.00	4776479.54	-17:56-83	14869.19	11076-63
389.1982	15731796.42	14475343.87	42531 45, 56	-17105.33	14821.99	11962-57
391.5986	1559:658-25	14505904-62	4279557.19	-17159.69		11040.51
393.9985	35649425.55	145417-5.75	43757394 64	-17210.67	14727.77	11-134-02
398.7705	15567.54-25	14611356487	4759671 67	-17312.2	14432.45	11004.32
401.174	15525445.50	1464 5415.62	4385 168.44	-17363.14	14584.34	11991.90
413.5986	15483221.75	146#1771.12	4411741.01	-17414.34	14536.12	10977.59
403. 9955	12441300.20	14751313-25	4444741.81	-17515-32	14419.78	11948.40
410.7993	15357298.5"	14795016.25	4400619.10	-17565.61	14393.34	17 933.46
412.3652	15329749.25		45-7743.12	-17598.57	14359,97	10974-51
415.5703	15773237.75	14854357.59 14888601-28	4568874.0A	-17605.18	14245.30	10904-03
429.3706	15188199.87	14922739.62	4594993.94	-17764.91	14197.41	12874-01





TIME	X	Y	7	1007 (ET/SEC)	YDOT (ET/SEC)	ZDOT
(SEC)	(-;)	17:1	1417	(,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1 2 1 2 7 9 1 5 7	() () 3 (0)
422.7715	151455"5.12	14954754.00	4421 72.11	-17914.63	14148.91	10858.82
425.17.4	151(2693.75	1499/ 651.87	4647114.25	-17862.85	14' 79.45	10843.68
427.5585	15-159255.25	15-24827.75	4677425.5	-17962.10	14001 88	10012 22
429.3452	14973003.87	15091286.25	4724757.06	-19011.25	13952.53	1 797.95
434.7456	1497 7 1.25	15174719.62	475-1652.37	-18066-13	13913.17	1.78.18
427.1455	149372 .1?	1515Fr 35.12	47765 Q. P1	-18109.95	13853.47	1. 766 . 54
439.5454	14343791.52	1-191212.5	49 2329.69	-19157.89	13873.8	17 751 . 91
441.9453	1486 146.5	15224291.37	4828111.75	-13266.18	13753.83	1 7735.00
444.3184	14756835.50	15255860.37	4853567.75	-18203 20	13719.01	10719.29
446. 744	14711001.97	15274522462	48/99/4.8/	-18351.9	13613.19	17686.87
449. 149	14574419.62	15355371.67	402 877 57	-19209.11	17553, 20	10671.80
453.946?	14581236.25	15357833.75	4056451.81	-18446.87	115.2.77	1/-654.4R
456.3462	14535878.25	1542(184+12	4982 11.94	-18494.59	13452.71	12639.16
458.7466	14491476.87	15452415.12	51 7528.10	-18542.22	134 2.14	17621.92
460.3735	14461237.25	15474101,67	5724812.44	-18574.53	13367.50	10610.76
463 5742	14401481.00	15516865.87	5 5 5/25.47	-18647.68	13210.00	1 588.42
462. 9740	14 31 1 399. 7	1559 447.75	51 3474 17	-19731-79	17198.3	10555.03
47: 7744	14766079.12	15612083.01	F174784.81	-18778.79	13146.57	10538.09
473.1465	14227278.87	1-6477 4.67	5159762.25	-18974.83	131 96. 77	10 521 - 54
475.5464	14177145.25	15674572.02	5184092.50	-18871.43	13-44.57	17504.52
477.9746	14131743.87	157~6194.12	521-478,87	-18918.63	12007.66	1*497.28
48 3745	14 7859 5.42	15737313.12	5235526.31	-19964.77	1294 . 87	1.1469.78
482.7744	14 14 1936,87	15768209.17	576°732.19	-19057 00	12027 42	1 457 . 60
487.1744	139999107.70	15820015 75	5207/97.30	-191-7-94	12785-50	10457.87
480.0443	130 34/ 12	15860193.12	5376510.31	-19147.95	12734.17	10401.49
4070 - 05		1900 109012				• • •
407.34 4	1395712. 25	1 5 991 86 1. 75	576 596.37	-10197.90	12681.59	11382.78
494 7744	13 41 .720 .47	15971411.75	5385429.62	-19239.39	12629.31	1:364.99
497.1743	137645 ?. 62	15951657.87	541:493.25	-10284.87	12576.82	10347.22
499.5742	13718167. 1	15981778.00	54353'4.10	-19329.91	12524.32	17329.43
51.9746	13671713.75	16 11778.25	5461 77.17	-10374.85	17471.77	10311.31
514.3745	17575151.97	16-41645.17	54949 1.74	-19419.95	12419.14	10207+38
5 16.7744	13573512.51	16.01124 75	5505004 54	-10654.49	1/100-40	12243 60
511.5747	1324/30_4/3	613/489.25	5558714 31	-19553.63	12266.34	10238.70
513.0745	13477973.37	16150655.75	5583769.19	-19597.97	12207-39	19229.34
516.3745	1339.787.37	16199 87.75	56 7774.75	-19642-02	12153.97	10201.80
518.7744	13343505.87	14218192.25	5632235.62	-19695.9	121 7.76	10183.10
521.1743	12504500*15	14247149.75	565665?. 6	-19729.66	12547.38	1'164.75
523.5742	13241837.52	15276017+00	5681023.04	-10773.2	_11993.77_	
525.0746	13301383.03	63-4742.75	571 5355.81	-19416.73	11004 63	1:12/.27
525.5745	121/6057 50	14141705 P7	5753873 56	-1980 - 17	11932.76	10789.28
533.1743	13158230 17	1637 129.67	5778 44	-10946.59	11779,97	10 77 . 18
535.5742	1311110.10	1641 0307	58"27.38.62	-10080.44	11724.02	10051 . 12
537.0745	12952294.12	14446411.62	5926312.31	-7 32,26	1167(.91	10035-05
540.3604	12914441.87	164741.0 . 87	5851222.12	-21 74.55	11616.79	10012.76
542.7744	12865929.25	155 22 68.75	5 974370.94	~2(117.27	11562.31	9903.17
545.1743	12917599.25	16529851.87	580933- 56	-2.159.35		9974.99
540 0746	12723425 75	14504031 63	E044114 47	-2.243 64	11309 88	9934.74
552.3745	17671092.75	14612122	594 0033 44	-2 785-49	11744.11	9915
554.7744	7621259 17	16619281.	50037-4.60	-2-127.34	11289.27	9995.12
556.4146	12582976.50	15657766.12	610 9923. 16	-2' 355.57	11251.76	9981.77
559.5742	12525492.50	16693203.51	6 411 4.81	-2 410.17	11179.?9	9855 • 56
561.9746	12476451.51	16710072.75	6164777.87	-2-451.49	11124.39	9835.48
564.3745	12427322.75	167466 3.62	6189218.0	-? 492.48	11769.26	9915.43
566.7744	12 379 91. 62	16777102.37	6111849.69	-2(537.5	11014.05	9795.10
569.1744	32378764.87	16799468.20	6150767 4A	-7 513.9.5	17970.27	97754.59
572 9744	122/124 .7	168518*6.0	#197157_94	-7.655-14	1 847.47	9734.31
576 . 3745	1219 12 12	16977771.75	671 5494 37	-2 495.3	1 .791.64	9713.55
578.7744	1213.475.25	16902604.00	5225791.44	-2:735.43	11776.11	9672.12
581.1743	1238-664.27	16929317.5	4252119.10	-2 775.30	10686+20	9672.47
583.5742	12 1757.62	16754865.75	£275247.21	-2"815.18	1-624.21	9651.73
585.9746	11 99 745 . 37	169P5352	A 79815".2"	-7.854.9	10568.72	9630.93
589.36(4	11.95 944.25	17.3.757 75	A 3/ 1 5 7 6 16	-2 844.12	10455 01	0598 09
507 1744	11 97 176 97	17 55783 25	6767463.76	-2'972 97	10300.54	9567.93
595 574 2	11 779791 . 47	17 8 673.75	A 200 209 94	-21-11.74	11347.32	9546 . 89
597.9746	11 7293 9 37	171 .5434.00	441 779 . E6	-21050.62	17284.85	9525 . 51
620.3745	11578742.37	17121353.65	6436175.37	-21089.46	10230.11	9504.31
6 2.7744	11 528 82.37	17154534.75	A4F87 9.55	-21128.0f	17173.47	9487.77
634.4144	115034 0.25	171711075	647445	-71154.76	15134.78	9449.16
6.7 . 5742	11475544 07	17222193.5	6576055 35	-21214.58	11003 04	9439.99
612-3745	11474510 37	17251112-5	6549537_19	-21287-57	9944. "6	9396.43
614.7744	113734 3.)	17274913.5	5577 56 94	+21318.17	9889.00	9374 .78
617.1743	11322104.4	17702577 5	6=94=29.31	21355.63	9831.75	0357 05
619.5742	1127 0 . 5 '	173221/4./	6615949.19	-21392.82	9774.48	9331.^3
621.9746	112195 4.5	17345497.75	5439321.12	-2143 .26	9717.09	9309.22
624 3745	11169029+62	17768748.5	6461435.57	-21467.28	9659.51	9786.88
626.7744	11115466.(*)	1/391861.75 17414034 75	5527395+44	-21504.06	9007.24	9264.66
C29+1/43	11204014+14	1.41.050*(3	0.07.401.4	-21092a 79		7676,007





TIME	¥	۲	,	XONT	YOCT	200 T
(SEC)	(FT)	1=1)	(FT)	(FT/SEC)	LET/SPC1	(FT/SFC)
631.6742	11 13074.75	17437673.5	ATT#758.69	-21577.36	04F4.91	22.1.22
633.9746	1 961226.55	1746 77 74.50	£75 364.	-21613.78	9420,13	c107.77
636.36 4	109 9678.97	174928-3.25	6772791.07	-21649.67	9371.41	9175.57
e38.7744	1. 37/521+37	175 5754.07	5 744 A 34 6	-21580.23	4313.13	913/ 681
041.1494	1. 2. 2114.31	177(14' 3+7'	0710117.0/	-21(21,54	2107 75	712 + 77
445 0407	10 7/ 1344 47	17671683 76	4880331 44	-217-1-14	0130 41	0205 67
448 34C4	1 64 9001	17507633 / 5	6993411 40	-11010 37	0081 13	8747 27
450.7405	1 596543	17415145.75	40/3737.56	-21863.63	97 22. 77	9179.77
457.4733	1 55 7044 .75	1763-214.55	4918449-19	-21887.97	8981.98	21, 19-00
655.5715	31,07-65.0	17657974.5	6946358.12	-71937-95	895-6-43	3903 .47
657.9714	1 479786.57	1757 2773.4	4967913.41	-21947 63	R84.	897.37
659.3495	3 3861 2.11	1771 641.57	4999547.31	-72***2.53	A788.44	9946 . 84
662.7495	1/323156.75	17721462.55	7 1111 . 49	-27 36,93	8720.71	9923.38
665.1404	10280229.12	17747547.50	7732495.00	-22071.19	8670.07	9977.12
667.5493	10227219.50	17767241.25	7153829.37	-22195.33	8412.113	5575.73
669.9214	10174744.62	17783647.25	7574858.05	-22128.67	8553.43	5853.44
677.7213	1-121577.62	178-41 07, 75	7.96.77.12		8404.59	8829.91
674.7712	1 ER327.	17874412.5	7117737.75	-???"5.86	P475.54	8804.34
677.1215	1.214979.7	179445 83,75	7134349.81		9374.01	787.53
679.7215	0001507.17	1/004621.5	7150108.31	~27277.41	#316.97	0 (77.03
001.9/19	9999 /0.12 0854360 75	170-4371 75	7703444 40	-//3.7.//	8747429	014.14
484 7485	001 222 42	17014.000 75	7777448 40	-7777, 73	71°'.	0404 87
480.1714	8747110.54	17043253.5	7743 133 36	-776 7 76	0121400	50 6449
691.5215	7403715 1	17967433.5	774 3 747 . 75	-77435.54	6510.23	8638.57
693.9214	9639633.75	17981813.25	7784485-19	-27447-71	7959.51	9614-15
696.3213	9584474.77	14577-843.25	73 5129.17	-77490.85	7899.55	8589.94
698.7712	9531430.""	18119729.75	7375714.75	-77531.5	7839.83	9565.54
730.3486	9494757.75	19732455.5	7379643.10		7790,]*	8548.95
703.5493	9422522.50	19057293.03	7366 951.19	-12595.77	7710.17	4516.12
705.9492	9368237.11	18775743.0%	7387359.56	-27626.32	7658.94	8491.51
798.3495	9313887.75	18094055.00	7477712.81	-22657.29	7598.64	8466 . 77
710.7212	924 117.97	18112075-50	7477753.46	-22687.89	7=30.71	9447.41
713.1216	97 5621.5	18130023.0	7447099.11	-???1#.43	7478.07	9417.57
715.5215	0151.45*	141479" 6.6	7658173.12	-22749.71	7418.44	9307.51
717.9492	_9.195796.25	12165842.20	7494514.1)	-27779.87	7747.13	3347,33
727.3496	9141-79.37	19183429.75	7579559.07	-22810.7	7246.71	3347.26
722.7455	8986371.25	15701565-01	7128359.69	-2284	7250.20	4517+24
723.1494	5/31471.27	19712102-09	74683684471	-22000 63	7314 01	7271.04
720.0314	991072 412	10353115 53	7697036 81	-22028.75	7 64 71	8741.74
727 3254	8744780	10340373.35	74.78 4.12	-77958.75	6991 50	8214.20
734.7495	8711330.67	1020"_11+22 197958A1_75	7477677.81	-22947.77	6912.32	8191.64
737.1494	8655127-87	18302445.27	7647233.94	-23016.49	6871.33	8165-11
719.5493	8600855.87	1831#862.25	7666798.19	-23^45.38	561/.25	8139.55
741.9492	8545515.	19335137.5"	7/ 843-1.04	-23.41.91	6749.P9	5117.78
744.3406	8491 74. 51	14311253.**	77**747."6	-23172.35	6487.72	81-87.86
746.7495	9434617.37	1=307235.75	7725125,12	-77131.47	6676, AB	P67.76
748.3486	8397614.^^	1877799.75	77381-34.44	-73149.16	6585.72	5044.67
751.5493	8323461.06	18398747.75	7763697.75	-23186.53	65.11,95	9010.20
753.9492	\$267782.50	18414283.6*	7782401.25	-23214.15	£447.56	7984.22
756.7495	8212: 26.53	194204 73.75	741 7 74.10	-27241.44	538°.98	7958.13
758,7495	8156716.00	18444033.5	7821 091.56	-73748.9#	6319.34	7931.98
761.1494	411.0341+12	18461 5.25	744 192.18	-73746.11	4757.61	7075.84
763.5493	5 344 397.31	13474049.	7477774	- (20/2-10	5140-12	7953 00
783.9442	7941393.09	18480747.11	7477414	-33376 36	6129.9	7834 60
108.3490	1445414.41	142.42624.14	18401 44*04		£1,72+72	1828+34
770.7405	7876170 34	10510035	7015606.17	-23412.12	6-1- 7-	7801 30
773.1404	741 3041.76	18533245.75	7924177 47	-73470.13	5948 71	7773 17
775.5401	7763725.04	14547447.75	7352797.19	-23455.12	5466.78	7746 92
777.9492	7107403-69	19561501-25	7971 356.94	-23481.76	5824.86	7721.16
780.3354	7551341.75	18575327.**	7099747.25	-77506.60	5763.17	7693.55
782.7495	7594564.44	1858-143.75	R	-23532.17	57	7566.64
785.1494	7538359.25	185 2769.75	4*26454.44	-?3557.34	5638.28	7630.74
787.5493.	_7481492.52	10616225.53	9344755450	-23582.69	5575.97	7612.62
789.9492	7424 967.62	18629533.50	8%3193.94	-23677.46	5517.73	7585.85
792.3496	7368170.50	18642693.75	8781370+12	-23632.46	5451.34	7558.50
794.7495	7311425.50	196557 1.25	HUC 04.77.44	-73646.99	5368.76	7531.51
796.3896	7272411.16	196645-4.75	5111×14.75	-23677.77	5745.16	7512.78
199.5493	*197759493 7141045 55	180012000 7	9152677 10	-23770 40	5201.39	7440 40
0314945Z.	. (19/09/AZ) . 7083851 54	1075653455	P17274 'C+L7	-73763 37	272 1477 5134 KG	7477.07
804.7404	7074817 44	18716401.75	6180735.31	-73776.07	5076.70	7104 44
800.1497	5069777 17	1011107022	8706768-56	-73800.41	5013.07	7346.05
811.5403	6317584-44	19747553.30	8226705 5:	-77873.77	4051 27	7179 41
613.9492	69*5778.17	19784359	8741 976.16	-73846.82	4887.5C	7311.67
816.3496	57931:0.10	1 3766 - 14.25	A750403.40	-73960 57	4874.59	7282.93
818.7495	5741 797. 75	1 3777517.25	#276941.00	-23892.41	4761.51	7256.12
821.1494	6683431.69	18788869.11	5294321.56	-23914.95	4698.65	7728.27
823.5493	652611-50	19870069.57	4711435.19	-73937.11	4635.61	7200.34
824.0497	4549527.19	13011118.75	P328991.75	- 23959.25	4577.45	7172.35
878.3354	6511338. 91	19421055.1	R745757.44	-73981.12	451 9.7"	7144.55
830.7495	645347 .+2	18927765.25	8363175.6"	-745 2.89	4446.41	7116.27
833.1404	0395790.00	18343767, 1"	578 SZZJ.1Z	-24024+55 -24024-64	4382.97	7057.99
835.5493	0101117.62	8857872.75	859739746Z	-741:40a74 -74377 AA	4754 /8	1009.68
65769452	078 1076425	, MM64 193.75	57177 (0 477	= 4 = 1 + 1 + 1 + 1 4.	7420+9L	7-1 1La46





TIME (SEC)	Х (FT)	Y (FT)	2 (FT)	LETASEC	TOOT COAZY EE	ZODT SET/SECI
840.3496	672357P.56	19/74234.5	843.05	-74088.2	4197.04	7003.08
842.7495	5164744.44	11194221.03	1447727.87	-24109.5	4120,55	6974.49
844.3896	6125191.11	104059.75	3459146.12	-24173+0-	4086-35	6955.16
849.9492	5997 945 21	9 13267	1481-62.87	-24170.3	3938.83	6889.02
852.3242	5933517 31	1 22547 5	1513957.47	- 4190.0	2A76.17	6847.65
854.7246	5875427.60	ac 1 775. C	3531391.25	+24210.00	3812.37	6831.65
857.1245	5A17312.51	3941947.75	3546752.25	24229.51	374 . 54	6802.02
859.5744	575913462	4040767.53 2358534 EX	4563 44.17	*************	3671.14	67/9.10
864.3242	5642647.56	3967145.5	850542 0	-74287.45	3557.44	6716.39
866.7244	5584215.61	9975611.25	96115 16.87	-242 6.19	3403.47	6687.18
869.1245	547507	16003019.	AA2752\.5"	-74775.79	3429.7	6658.01
873.0244	540 0126.44	010 76.24	1450337.87	24361.70	3311.71	A599.AA
876.3105	535-972.16	03/7877.25	1675-51.57	24379.90	3238.21	6573.68
878.6963	5292796.69	: 215527.20	1497692.62	24397.69	3174. 75	6541.40
891.0962	5 7 7 4 7 1 3 , 2 7	73769.75	7-6355.87	24415.41	3110.33	6511.88
885.9743	5116749.75	19.77775.75	737653.5	24450-52	2981.56	6452.56
858.3242	5 \$ \$ 544.75	12044854.03	797103.62	24467.71	2917.47	6423.10
890.7246	4999 796.49	19751779.50	768485.12	74494.35	2852.99	6393.54
892.3984	4957814.56	19756517.50	10171.37	24496.3	2818,21	6377.71
897.8965	4373 17.07	10 71552 31	14.20.50	24534.1	7664.97	6304.62
901.2064	4764119.37	97786 5	20115.25	74550.3	2596.54	6274.83
902.6963	4715]91.37	999414.75	44139.5	24566.2	2532.29	6245.02
915.0962	45452-5.75	9005841 03	13073 25	24582.2	2467.87	6215.06
707 . 4700	430 / 19 • //			2437780		
019.0243	4577445.12	191 1616.51	388050.51	24613.1	2238.02	6156.40
912.2964	4469043.25	19127087.00	903513.7	24528.2	2274,45	6124,56
914.6963	440.9920.00	10112467.75	18176.1	24643.1	2209.75	6094.55
917.1.962	4791555.50	19122764 75	937766.01	74657.7	2145.02	6064.21
921.8975	42772 2.54	10127487.5	161 736.7	24684.9	2015.92	6013-53
924.2074	4173 . 10.28	10122442.75	1761 7. P	24701.1	1951.29	5972.96
926.7256	4113142.29	9127121.51	292574-31	24715.2	1885.84	5942.29
924.1255	1994347.44	1914125	114/98.62 118940 42	24729.17	1821.27	5911.79
933.8975	393 564' . 6	10140033.25	37864.5	-24755.96	1692.39	5857.97
936.2474	1976 217. 37	19153017.25	46859.5	-24769.12	1427.65	5827.35
938.6073	3816753.19	10157745.5	-A-9 87	-74782.31	1567.71	5789 . 62
943.5254	3697340.30	19164076.00	089604-00		1432.32	5727.42
945.9253	3537488.54	19158295.5	107312.62	-24827.26	1367.35	5696.66
948.3252	3577919.20	10171539.25	115947.00	-74832.57	1302.54	5665.83
95. 7256	3519785.81	1 1 745 P9	12051 1	-74844.54	237.53	5634.83
955.4976	3309677.66	1018 195 5	154251 71	-74867.77	11/8-33	5573.13
957.9253	3339286.77	101 92 796.5	169741.5'	.74879.27	1042.67	5541.58
960.3252	3279545.14	10185223.53	183775.1	-: 489P.44	977.46	5510.21
952.7256	32100 5.19	39187489.75	104194.3	-24971+51	912.52	5479.07
967.5254	10 23 78	1016557	2: 2147 A	-74077.99	782.41	5416-53
969.9252	2 4 4 7, 50	1 193355.71	02352 3 81	.24033.37	717.4*	5385.02
972.3115	2.98/ 896.50	10104001.2	9244116.5	-24943.70	652.5	5353.76
974.7256	292.669.16	194487.5	0241-12.1	-24953.47	587.04	5371.95
911.122	296 2771+39	11141613+24	2/***0.0	-24963471	741.89	5290.54
979.5254	2951849.41].].6005"2.	\$286395.87	24077.03	456.72	5259.00
981.9253	274.915.72	171 12.25	0208079.11	24262 52	391.4]	5277.36
984.3237	2420 020 44	9211576 51	9311486.00	24991+50	326.42	5195.54
988.3652	2579942	C231C67.75	33373 68.	25106.48	216.41	5142.03
991.5254	241 1800 41	52 2514.25	0743551 .	2 17.85	130.40	5162.16
993.9253	744 1849 64	102 2751 5	134 753,12	23-24.69	65.44	5768.29
996 + 2252	2323675.	192 2752	0384030 47	25142.47	-65.15	5036,27
1001.1255	2262565 "4	102 2517.25	120401	5050.39	-130.42	4972 .41
1003.5254	220.438.44	19277125.75	4 2795.27	:5-57.78	-195.72	4940.34
1565.9253	214 203.1	1577.75	*47 *633.17	25: 65, 30	-761.11	4938.19
1010.7254	2110017	37 11	444 13.15	75 72.49	-791.87	4843.73
1013.1255	1950741	10108002.25	445414.67	250 86.26	-457.75	4811.31
1015-5254	1909578.64	10107817.01	1467117 . C	25542.97	-572.38	4779.33
1017.9253	183930 .55	19176485.01	1478544.12 1443835 45		-587,73	4746,98
1022.7256	1 71 8 787 76	10103940 75	15 1174 71	-25111.36	-718.65	4681-94
1-25.1255	165 9516.12	1 21 91 445.72	1	-75117.16	-783,92	4649.56
1027.5254	159323/ .er	19169587.0	1573491.75	-?51??.57	-849.15	4617.12
1017 1051	147762014	118/4/1.5	1544537	-75127.89	-914.69	4584.Z9
1034.7754	1417767.9	182765.75	7556382.5	-25138.7	1 45 57	4519.07
1036.2652	1 374 46.54	0191115.7	7567777.71	-25141.18	1:97. 9	4496.60
1039-5254	179667.19	10177474.	9577916	-25147,31	-1176.24	4453.79
1041.9253	1236250.91	9171474.5	- H35 65 77	-25151.63	-1241.72	4421.00
1046.7256	1115496.36	1916 12 58 . 0	9619629 12	-25159.49	-1372.54	4355.13





TINE (SEC)	X (FT)	Y LETI	Z (ET)	KOOT (FT/SEC)	YDOT LET/SECJ	ZONT (FT/SEC)
1049,1295	1 755113.30	19164885.25	962 3041.50	-25143.44	-1438.21	4327.17
1651.5254	994717.47	19151355.5	263 23 74.87	-25166.91	-1513.45	42#9.31
10 53. 975 3	924315.71	19157668.75	964 76 29.12	-25176.05	-1568.78	4256.28
1056-3752	9739%***	19153827.50 10140834 50	965 9694,25	-25173.4"	-1634.12	4273+20
1061-1255	753053.06	19143667.33	900070240	-25178.75	-1765.04	4157.06
1063.5254	692673.56	17141752.5	0587855.1h	-25151.22	-1830.51	4123.90
1065.9004	532815.34	19124928.25	9693613.12	=25113.62	-1895.17	4090.93
1068.2866	572719.51	19132328.25	87F-3332.75	-25185.24	-1960.23	4758_04
1073.1036	451469-17	19127217+2"	971 9704.97	-25188 87	-2591.57	3991.30
1075.5505	3911 16.49	19117477.75	3729745.12	-25190.38	-2156.79	3957.40
1077.9004	33 15635	19117723.5	972 87 33, nn	-75191.79	-7222. 72	3974.22
1080.3003	27-31-31-37	19176811.25	1149195.62	-251 92.75	-2277.65	3897.83
1084-3403	165316.63	19397347.75	3763686.25	-20143-02	-2397.67	3834.59
1087.5005	86700.79	10380634 50	1775734.12	-25194.67	-2483.67	1790.27
1089.9004	28236,12	19083595.25	978479 .25	-75194.76	-7549.13	3744.85
1092.3643	-37778,54	10177393.25	9793746.***	-751 94.75	-2614.54	3722.22
1097.1006	-1=3170.06	19064535_01	9811474.00	+25194.24	-2745.31	1655-47
1099.50 5	-213632.92	19157868.51	982 32 18.50	-25193.53	-2810.29	3621.93
1101-8726	-273392.71	19051125.50	987876.42	-25192.65	-2875.00	3588.71
1104-2725	-333851.21	19144147.51	097737.37	-25391.47	-794 .21	3554.73
1109-1016	-1-7 5.27	19750929.27	985433 .75	-25148.80	-3171.80	3485.55
1111.59 5	-515922.02	19922184.25	9862657.37	-25187.22	-3136.87	3457.57
1113.907.4	-575366.78	19114577.75	087:002.50	-25285.47	-32" ?• 14	3416.68
1116.2066	- 63 54 52 62	190^6859+25	9579(19.87	-25183-39	-3267.18	3354.88
1118.4724		14062047.50		-7*18*.97	-3331.01	3351.06
1123-4722	- 417 397. 30	18982682.50	990 2975. 17	-2-178.52	-3396,93	3376+94
1125.0725	-977820.45	18974793.50	993 3915,37	-25172.83	-3527.33	3248.77
1128-3003	-979929.76	18965650.00	991 9667 .67	-25169,84	-3593.43	3214.30
1130.7072	-30933.99	18956949.0	9976333.62	-25166.57	-3558.43	319.12
1135.5005	-1120119.66	19751003+75	993142 15	-25154.02	-3731.87	3157.17
1137.96.04	-1180494.04	18929943.01	994 8861.07	-25155-76	-3853.87	3077.05
1140-3063	-1246 858.87	18920576.25	9956234.62	-25151.98	~ 3918, 99	3142.95
1142.7562	-13(1213.55	18911093.00	9963466-00	-25146.63	-3984.02	3078.43
1147.5005	-14219-1.72	1921401401401	9977743 78	-7-141.52	-4"49.15	7974.71
1149.9024	-1482222-36	15551724 25	00P4 756 17	-25137.2	-4170.15	79.5.73
1152.3003	-1542531.22	18871596.75	9993697.37	-25127.23	-4244.09	2877.85
1154.7702	-1612877.59	18061333.57	9998535.50	-75121.77	-4319.16	2836.12
1127-1000	-1003122.73	12050517.25	10005331.87	-25116.14	-4373,89	251.68
1161.9004	-1793646.45	18829617.51	1-194683.67	-25104.14	-4507.57	2737.61
1164.2865	-1842543, 31	18518783.50	11025163.05	-25-97,94	-4568.28	2699.09
1166.7002	-1064171.30	1897679.75	19^31532.87	-25/191.52	-4633.41	2663.11
1169.1005	-1964332.50	10766174 67	10037896.00	-75" 84.65	-4698.22	2628.43
1173.96 4	-7 -847/1-87	14772619.02	1.4787337.62	-25.7.62	-4877.75	2592.02
1176.30-3	-2144859.22	18761954.25	10-56433,37	-75(63.34	-4897.37	2524.34
1178.7(^2 -	-22(\$999,59	1875(135.5	10067449.75	-75' 55.71	-4957.72	7489.46
1183.50/5	-7246"9".31	18741069.25	10-66513.37	-75050.71	-5001.16	2465.88
1165.9074	-2385322.67	18713745.25	10179998.75	-25032.26	-5151.12	2419+90
1185-3613	-2445287.81	18701365.75	31 18568-1.51	-75-23.95	-5215.4P	235%.10
1190.7002	-2505432.28	18530711.75	10291278.50	-25715-17	-5280-03	2315.16
1195.5005	-2000-58,14	18663066.30	10102773.42	-2599663	*5344.60	2289.03
1197.9034	-2575451.19	18449997.25	10107569.50	-24988.36	-5473.71	2279.98
1206-20-3	-7 7454 19.66	18626783.75	1-112-31.5	-74079.19	-5537.86	2175.14
1202.7572	-74 5345.59	19673416.07	1118nn7.50	-74969,55	-56*2.44	2140.03
1203-1100	~2925158.91	18596214.25	10123104.12	-24959.59	-5666-71	2104.77
1209.9004	-2985023.13	18582383.25	10173338.75	-24939.22	-5795.21	2014.67
1212.2866	-3044521.53	1856 84 78.00	10137852.12	-24928.97	-5859.43	1999.66
1214.7072	-7174576.75	19554259.""	17147635.87	-24918.46	-5923.81	1944.33
1219-5075	-31799/10/2	18759961.75	1873"8,67	-2495.7.57	-3987.86.	1020.00
1221.904	-3283575.19	18510913,25	1156398.25	-74885.05	-6116.17	1459.53
1224-3003	-3343683.06	18406159.00	10160816.50	-24873.54	-6180.37	1873.47
1226-7022	-3403363.03	18451249.25	10165153.00	-24861.78	-6244.17	1787.97
1231-50-5	-3999155622	18451048.25	1.103563.32	-24253.57	-6787.04	1763.45
1233.90.4	-3517244.09	18435599.0	1-177642.12	-24875.73	-6436.79	1691.81
1236.3113	-3641808.09	184200 76.00	10181635.87	-74812.95	-6501.07	1646.47
1230.7012	-37(1341.59	18404400.25	10185544.62	-24800.31	-6563.66	1611.01
1243.5005	-3820328.1A	18372586.07	10104-09437 17103138-12	-74774.43	-90/7.61	1575.74
1245.9004	-3879768.10	1835(451.01	1:196761.75	-24760.79	-6754.96	15/4.77
1248-3603	-3939175.29	1834(163.5)	1. 20. 3330.50	-24747.29	-6818.51	1469.33
1250.7002	-3998549.91	18323723.25	10203814-12	-24733.58	-6882.30	1433.78
1255.5005	-4117211.12	18290381-25	10207212+07	-24705.49	-7009-76	1398.00
				the second se		

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TIME (SEC.)	X (FT)	¥ (FT)	7 (FT)	XDOT (FT/SFC)	YDOT LET/SEC1	ZDOT (FJ/SEC)
1257.9504	-4174494.62	18273483.5"	1 753.12	-24691.09	-7 72.80	1327.69
1260.2866	-4225235.87	182565275	1.214077.87	-24676.54	-7125-97	1291.80
1262 . // 02	-4294926.44	1873923 .75	1. 2520.24 25	-24601+33	-7199.78	1255.87
1267.5205	-441 3236.69	19204265.0	1 225911.12	-24631.2"	-7326.41	1184.67
1269.9114	-4472335.75	1318(757.4	1 22861 . 37	-24615.85	-7389.45	1148.96
1272.36 3	-4531387.37	14163407.""	1.231375.	-24656.01	-7452.63	1113.30
1276-3154	-442:116.75	18136762.75	1.233675.37	-24573-63	-7558.70	1053.73
1279.4756	-4707729.00	18114746.5	1-210031.0	-24551.96	-7641.16	1006 . 72
1281.6755	-4765631.56	18096372.7'	17 241974.25	-24535, 48	-7774.21	971.99
1284.2754	-4875494.37	19 77768	1.0743591.27	-24518.89 -24502 24	-7/67.23	935.04
1289.0752	-4943 00,12	19 4 185	1 2470 7.47	-74484 97	-7892.81	863.44
1291.4756	-5101951.81	18121164.	1 249937.75	-24467.61	-7955.74	827.82
1293.8472	-5059959.00	1807223.	1 251858.87	-24450.14	-8(17.62	792.27
1298.6753	-517782-12	179622 .9.	1.25551.12	-24414.48	-8143.45	72.1.20
1301.0752	-522630.31	1704350	1 257105.75	-24795.99	-82 6.14	584.48
1323.4756	-5294928.50	17923817.5	10 258745 62	-74377,01	-9268.57	648 . 55
1305-9755	-5411533.25	17983949.75	1.261728.12	-24359.15	-8393.11	612.08
1317.6475	-5469553,31	1786 3847.5	1 263 62.62	-24321.88	-8454.97	541.43
1313.474	-5527211.25	178474P1.7"	1' 264318.75	-243 2.54	-8517.15	505.36
1315.4756	-5584809.31	17977773.7.	17 765571.87	-24782.85	-8581.14	459.08
132	-57 3 357 12	17781242.0	1 767581.27	-24243.49	-8704.60	397.34
1722.6753	-5761515.19	17761277.75	1 769401.75	-24223.56	-8766.44	361.33
1-242496	-53' 2"61.12	17745563.5	1:269075.62	-24209.24	-88(9,77	336.18
1327.7564	-5974 996 . 27	17718531.5	1 27 19.75	24183.73	8897.37	291.16
1329.2905	-5721573.44	17721722.5	1 27 554.12	-24167.27	8937,15	262.37
1337.159?	-5991845.12	17675077. 75	1 77145	-24142.33	-9010-95	219.30
1336.0555	-51 5657.81	17632425.	1 777124.47	-24099.89	-9134.3	147.13
1338.80 4	-6153177.60	17614773.7	11 27738 .75	-74" A2.61	-9192.72	179.14
1241.7.01	-4777775.10	17598289.25	11 77657.87	-74:55.7	-9257.77	75.04
1346.55%	-6337599.5	17543655.00	1 272945 75	-24012.78	-9386.14	3.24
1 14A . 49"2	-6383642.19	1752+204.25	1 777923.75	-23994.73	-9429.67	-25.07
1351.7594	-6452748.75	17498273.5	1' 272697.25	-23968-10	-9512.66	-69-17
1756.1762		17452534.75	1 272182.62	-21922.36	-9674-95	-141-02
1358	-6612361.37	17622403.6	1 271832.0	-229.3.92	-9674, 9	-171.32
1367.0956	-5433767.75	17475484.5	1 271323.87	-23875.64	-9747.96	-213.56
1362 8016	-6729494.94	17384049.5	1077091.62	-23857.05	-9795.92	~242.30
1367.4974	-594700 19	7376457.7	1 2/0555.01	-238.9.44	-9917.57	- 314 . 47
137 . 5452	-4912000.06	1731 742.73	1 269579.04	-23781.21	-0900.00	-358.21
1372.4902	-405754.01	17291764.25	1 267977.12	-2376 .98	-10138,73	-39672
1377. 2254	-7 72-41.59	17242827.7	1 765971.25	-23711.30	-10161.15	-459.86
138: 1953	-7130920.04	1721 36 65.25	1 244444.97	-23681.49	-10233.21	-5/2.69
1382.1353	-712575 .94	17103764.53	1 263441.12	-23661.18	-1/281.76	-53? .^6
1394.9055	-72*1185.94	17164259.25	1 74 714.37	-23610.17	+1-370.07	-5/4.90
1399.7954	-736.5494.94	1711427	10259025.25	-73579.21	-11473.90	-647.19
1391.7354	-74174 9.1?	17 930-4.5	17757641.57	-73558+45	-10522.19	-676.30
1394.6772	-7480726.12	17063265.50	1 255615.75	-23526.61	-11594.78	-719.91
1396 . 5256	-7525370.12	17-431 7.	1 254221.87	-775 5.73	-10647.00	-749.45
1399.4375	-7439893.75	15201342.25	1 75 474 87	-23452.37	-10762.56	-821.25
1414.2383	-77 5596.12	16 961 9 95. 51	1 7481 0.87	-23410.60	-10833.70	-864.47
1476.17-4	-7751324.62	16 93 94 1 9. 25	17246211.50	-23397.7	-10881.51	-893.56
1410.0396	-7918236. 6	14 3 R1(5.5)	1 742536.75	-73364.0	-11001-26	- 345 . 77
1413.8294	-703 300 34	14956261.75	1717 17 17	-23359.24	-11671.04	-1009.00
1415.77.5	-797=414.56	16933815.25	1 227 30.55	-23286.66	-11118.67	-1938.35
1418.6242	-8142144.69	16801820.00	1.234.0	-???5?.86	-11189.48	-1081.20
1423.4775	-3154537.04	16767101.87	1 728501 77	-23195.21	-113-8.27	-1154-30
1425.376	-9198422.25	1677594 . 75	1 224373.17	-23172.24	-11354.60	-1182.62
1429.2773	-9265726+62	14692972.75	3 222879.37	-23136.95	-11425.57	-1276.31
1437.2114	-3111457.37	16670689+30	1: 72: 475+37	-2311-14	-11542.77	~1298.67
1435.0112	-8421248.50	15615343.87	1 214279.87	-23053 59	-11569-55	-1327.58
1437.8774	-8497772.75	16582 73.25	1 21 411.75	-23 17.95	-11659.02	-1373-81
1439.8115	-9531768.37	36559623.53	1. 2. 3459 43	-77993.27	-11795.87	~1399.90
1444.6113	-8641594.75	16572964.5	1 21 939 50	-22931.94	-11821.70	-1472.01
1447.4775	+97/ 7650.62	16468982.25	1 196558.75	-22894.97	-11890.65	-1515.01
1449.4453	-8752696.62	14445577.37	1103544.25	-22869.48	-11938.11	-1544.86
1454-2456	-8862315.56	16387954.5	1.145950.75	-22866.31	-12053.31	-1616.76
1457. 776	-892695 .25	16353773.75	118132 .75	-22768.57	-12120.72	-1659.32
1459.1454	-8971627.62	16329825.75	1(178^?6.50	-22742.10	-12167.67	-1689.88
1463.8452	-9389630.12	16271157.00	10169747.50	-22677.25	-12281.85	-1769.71



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Table B-1.Reconstructed Reentry Trajectory,
ECI Coordinates (Continued)

TIW (SEC)	X (F1).	¥ 1531:	2 (ET)	X90T	YDOT (FT/SEC)	ZDOT
1465.7896	-9174696.75	16747225.25	1* 165795.62	-77650.89	-12327-93	-1709.90
1470,5894	-97122.3242	16187781.87	10157530.75	-27584-42	-12441.06	-1867.20
1473.4795	-9799471.17	16151727.25	11152-05.75	-72544.05	-12509.01	-1905.77
1475.3895	-9341508.25	16127799.37	10149419.25	-27517.24	-12553.77	=1.934=27
1478.2703	-94 4516.12	14093415.42	1'142755.87	-77476.39	-12621.48	-1977.63
1487.8545	-9621167.63	15956405.37	1*123141-1*	-72337-53	-12844.16	-2121.37
1492.6543	-9728112.50	15937587.87	10112786.62	-22266.31	-12954.64	-2193.11
1497.4995	-9835821.50	15944544.10	10101995.00	-22193.62	-13065.59	-2265.58
1499.4325	-9575595,62	15519244.37	10097277479	-22120-21	13174.47	-2137.05
1504-2724	-99849 2.37	15756149.57	1 . 85393. 87	-22599 30	-13218.55	-2365.91
1507. 195-	1 24 3175-12	15716165-62	17/79542.62	-22544.33	-13283.30	-2478.97
1512.2524	1151566.12	15449327.75	10066937.75	-21964.74	-13398.68	-245%.77
1516.5454-	1255712.50	15591556.37	10056129+25	-21995.79	-13494.45	-7547.69
1518.7124	1-3122.62	15512701-87	11153569.25	-21#6P.85	-12547.63	-2561.78
1520.97"5-	1.35 255.30	15537122.87	17-44952.50	-21825+82	-13595.49	-2613.98
1524+1212-	129256.4412	15445256.45	10030746-37	-21737.22	-13706-53	-2693.30
1528.3472-	10512984.12	1543/ 805.75	10025004.50	-21701.46	-13752.48	-2724.62
1533.522.2-	19562383+87	15420692.12	10019013.12	-21664.53	-13799.37	-7756.88
1533.7254-	1.500668.25	15356295.12	16 1110.37	-216^9.15	-13867.67	-2814.25
1536.5293-	1 77 2203 97	15796654.97	0797937 6	-21532.98	-13957.57	-7867.40
1540.1606-	1-768146.75	15766863.25	9991787.87	-21494.67	-14001.01	-2898.63
1543.3716-	.) - # - 7 - 7 - 12	15221799.00	9982415.37	-21435.81	-14066.37	-2945.47
1242.2452-	10953519.02	15191242.75	8612385	-71395-34	-141-9,76	-2411, 10
547.6465-	37073063.25	151672-1.75	448967 .CZ	-21355.35	-14351+62	- 50 ⁿ i - 61
.553.1522-	11243677.02	15264702+62	9957211.75	-21251-11	-142*6.97	-3765.87
1555.2103-	11 189639.50	15053E(3+07 15023320.75	9946499,75	-21208-45	-14298.27	-3116.77
1559-5122-	1118-564.87	14002213 75	9872078.37	-21122.80	-14375.86	-3178.12
1561.67'4-	312261 4.62	14961137.77	9974-95.67	-71 78.78	-14419.""	-32" # . 44
1564-86 4-	11707736.37	14915-41.5	00007741.75	-21712.71	-14477.07	-3257.43
1569-1475-	11383130-0.0	14952811.62	9901715.25	-27927.36	-14553.86	-3309.47
1571.3335-	11429815.75	14820954.37	9894449.25	-20975.51	-14592.33	-3338.17
1574-5356-	11495549.25	14774139,12	9883692,62	-20804.96	-14647.54	-3367.21
1578.70*5-	11563868.12	14743 67.87	9576532.5°	-21.757.45	-14687.67	-3407.30
1590.0326-	11623195.62	14640 77.75	941818.12	-2 659.55	-14755.53	-3467.22
1584-1353-	1169422*.75	14632753.62	985 1666.00	-20584.72	-14806.72	-3507.02
1586-2*44-	11737788.50	14671341+00	9843227.00	-27533+16	-14839.89	-3525.50
1500.5352	1187547 .12	14577713.75	9878 37 37	-7" 427 .75	-14905.14	-3575.17
1593.6973-	11 86 7 00 7. 97	14405473 37	041665 . 67	-2-347.52	-14950.74	-3611.68
1595.8545-	11 733751.62	14458185.10	OR 8842,75	-2 291.57	-14981.57	-3636,39
1600.1732-	12 2 246 25	14303049.37	95:115 .07	-2-2:2:3.45	-15038.28	-3684.34
1603.3254-	12 184 974 .75	14745734.25	9781177.75	-20092.46	-15(79.67	-3719.25
1615-4546-	17127341.37	14313754.75	9773477.17	-71733-85	-15165.65	-3741.39
16-0 7334-	172178 6.75	14241465.12	9767118.07	-19974-82	-1137-40	-3765.10
1612.8975-	17775457.77	147116 3.87	9745292.25	-19821.07	-15190.35	-3816.94
1615-0215-	17317687.37	14149731.37	9737156.87	-19758.75	-15211.74	-3837.47
1617.1475-	12359639.10	14134353.75	9729043,25	-19693.63	-15233.35	-3957-69
1619.7083-	174-1927.50	41-3565.75	977 - +++ 12	-19628.49	-15253.69	-3877.01
1622.4976-	12464566.87	.4054723-12	9718211.87	-19531-63	-15242.84	-3906.76
1624.7474-	12547743.00	13990606.08.87	9700032.12	-19463.47	-15299 .9 9	-3924.99
1624. 97. 4-	125#4357.4	13957159.37	9683136.37	-19326.49	-15332.90	-3961.12
1637-1 619-	17440865.51	137" P214. R7	PA7'459,17	-19218.71	-15353+83	-3987.16
1634.1965-	17721746 13	13875561.25	9661967.0	-19145.17	-15365.85	-40:1.75
1639.4574-	1270 970 67	13794*#2.37	964 3805 62	-19955.45	-15387-14	-4735-62
1641.6167-	12831494.75	13741284.37	9632053.62	-18875.13	-15393.42	-4049.03
1643.7456-	1267203	13728503.60	9623419.12	-18793.00	-15396-15	-4061.77
1047.577-	12771177.77	1264/793.47	94/1793 76	-19594-67	-15207.57	-4088.96
1651.2143-	13 113	13613472.87	9502035.12	-19407.16	-15396.20	-4094.04
1653.3115-	13 49945.75	13581223.50	9584339.75	-18410-48	-15391.47	-4116.75
1077+4736-	12147695-17	13290747.87	4277457.87 9562161.26	-18327.14	-15387.78	-4115.73
1665 .7744-	131861MP.75	17446471.5	0553588.67	-18592.35	-15370.96	-4132.29
1662.9116-	12774756.77	11412579.87	9544751.62	-17999.77	-15362.32	-4177.33
1668-2134-	1331955' .97	13352197.67	9572793.05	-17759.92	-15237. 01	-4146.59
1672.466 3-	13394651.37	13287019-25	9505151_50	-17557-13	-15317.38	-4148.19
1677.9135-	134P7878.12	13215257.37	2482972.5P	-17297.52	-15269.02	-4147.44
1677.94 4-	13524516.87	13172814-75	CA74157 . AL	-17191.92	-15246.56	-4145.47
1684,2134-	17507744217	1514413.07	990734 's 75 9456488_87	-1/084-37	-15225.80	-4142.75
1687.4136-	13651578.87	13159159.50	9443216.25	-16812.50	-15165.90	-4135.08
1649.5415-	13647217.37	13426928.75	9434417.57	-16698.56	-15141.14	-4129.00
1691.6665-	13722592.75	12994762.75	9425646+37	-16580.37	-15118.80	-4122.37



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Table B-1.Reconstructed Reentry Trajectory,
ECI Coordinates (Continued)

TIME	X (FT)	Y (ET)	7. (ET)	1907 (FT/SEC)	¥907 (FT/SEC)	200 T (FT/S FC)
1693.7334-1	3756736.12	2963535.25	9417137.67	-16781 27	-15(73.43	-4115.87
1701.6724-1	3885454-25	2843965.12	9386475-00	-15963.07	-15^25.12	-4117.39
1703.5654-1	3915550.25	2815544.62	9376679.15	-15832.07	-15000.76	-4119-04
1706-6274-1	3963710.25	276.9672.00	9364 42.17	-15624.47	-14961.68	-4134.92
1708.7915-1	1007357.75	2737336.25	9355177.56	-15472.14	-14972.55	-4157.78
1710.92 4-1	4131134.00	12705614.87	0746271	-15167.25	-14820.75	-4101.47
1715.2456-1	4195738.2	12641526.75	9328094.00	.15717.75	-14749.92	-4211.58
1718.4355-1	4143291.75	125946 3.50	9314632.25	.14797.59	-14623.79	-42?8.58
1720-5952-1	4175099.62	12563195.87	9305573+62	14649.35	-14529.47	-4225.04
1722 . 7722-1	4237119.97	17532397.00	9287512.67	14345.40	-14734.27	-42 ** + 27
1728 0 723-1	4282622.75	12455238.5	9274775.75	141-5.14	-14187.16	-4127.69
1730.1953-1	4312393.12	12425833.37	926551.62	13939.9"	-14079.13	-4091.73
1732.3223-1	4341864.87	12396008.25	9256839.00	13772.71	-13965.81	-4354.78
1737 6726-1	4414410 50	12222101 27	9244102+10	-13345-13	-13650.7	-9045 26
17 39. 795 4-1	444	12293245.75	9227115.37	-13168.29	-13578.72	-3.925 . 27
1741.9224-1	447 375 .75	122646 9.27	9219697.12	-12087.67	-13302.70	-2884.10
1744-0732-1	44981 78.12	12235952.00	9210384.75	-12814.14	-13253.30	-3843.19
1749.2554-1	4019104.02	121444/5.87	010344 .23	-12335.69	-12892.69	- 1/14.11
1751.2734-1	4587982.55	12142202.03	0183294.37	-12155.73	.12754.57	
1754-2295-1	4573515.67	12104012.11	9172578.97	-11985.18	-17549.54	-3615.80
1759-2725-1	4587276 . 37	12-42497.53	9154659.67	-11419.83	-12205.57	-3477.15
1761.1655-1	4713714.77	12019511.50	9148140.87 9137025 37	-11230.74	-12963+4	- 147 . 56
1766-0864-1	4757752.37	11960943.87	9131656.75	-17717.7	.11737.94	-3276.19
				10404 65	11/15 54	- 3 7 7 6 4 1
1771.0202-1	4/78824.75	11947/44.37	11/719/*	-11140.75	-11430.99	-32/0.41
1776-0723-1	4459733.87	11846942.37	9199797.25	-0561.98	-11077.24	-3147.59
1777.9653-1	4376929.37	11926149.12	9693834.50	-9235.91	~17895.56	-3141.35
1780.9883-1	49:4657.00	11792637.37	9084364.62	-9014.81	+10613,38	-3174.02
1782.9956-1	4977547 59	11772543.37	0.71509.50	-88 585.16	-1-174.79	-3:41.33
1797.3086-1	4959557.12	11728664.12	0165132.62	-4350.1.	-0047 - 3	-2955.85
1790.4722-1	4985438.70	11697725.12	9055873.62	-8002+62	-9612.44	-2874.44
1792.5952-1	15002169.12	11677562.75	0040083.37	-7757.95	-9381.46	-2724.41
1794.7222-1	5918437.75	11657861.00	3744293.12	-7512+54	-9144,30	-2020+12
1800-0723-1	5157727.50	11610564	913 835 37	-6919.21	-9531.14	-24-45
1802-1953-1	15171459.25	11592727.12	0025823.62	-6682,74	-9278.51	-2321 . 1
1804.3223-1	15085421.50	11575382.51	0121973.50	-6446.03	-9024.33	-2237.85
1876.4736-1	5099734.75	11558385.25	9715747.75	-6219.45	-7776.18	-21-7.30
1811.4873-1	15128794.97	11525845.12	00/5021.12	-565(.6)	-72 3.55	-1966.18
1814.51^3-1	51454 4.62	11490525.87	941 1145.87	-5235.11	-69 2. 9	-1854.78
1816.4414-1	15155486.50	11486386.12	9996637.87	-5174-19	-67.6.17	-1776-18
1819.4272-1	1517 207.62	11456771.75	9991487.62	-4754.45	-6946 27	-10/5.24
1823.3354-1	15187861.62	11447364.87	8985139.87	-4285.72	-5059.44	-1501.54
1826.3154-1	15200146.12	11424745.67	8081437.5"	-1959.14	-5765.57	-1548.64
1828.2876-1	1527752.50	11413562.25	8977494.75	-3755.44	-5555.38	-1 521 - 82
1831.3105-	15219694.75	11397241.62	8972885.67	-34R7 19	-57.62.45	-1417 83
1835-4482-1	15237376.37	11376443.62	8967*37.75	3132.21	4825.8	-1357.87
1838.6274-1	15241920.75	11361552.25	8962908.00	-2872. 1	4540.35	-1245.12
1840,791 -	15747939.75	11 351 974-17	8961293.75	7697.7	4757.87	-117 .97
1842-9862-1	5253397.97	11342978.67	eg#7911.12	2510.01	4187.14	-1103-88
1845.0483-1	5258628.75	11334113.62	8955588.87	2337.01	4717.22	-1044.31
1848-2275-1	15765640.37	11321713.37	8952432.25	2009.13	34783.00	-962 . 10
1850.3124-	15269914+02	11313972.62	8422423+67	1970.04	2479,73	-947.78
1854.5786-1	15277697.62	11209135.62	5946842.37	1403.07	3236.13	~797.34
1857.7466-	15282779.37	11288866.12	9944424.75	1521.41	3145.3	-727.63
1859.8745-1	152859^3.37	11282302.12	9942927.25	1414.87	-3/24,11	-681.83
1862.0044-	15288817+87	11269894.50	3991321452	1224.28	2811.81	- 595 . 02
1867.2725-1	15295166.37	11261341.25	1938426.25	1112.48	2653.53	-5 39. 33
1969.32 3-	15297349.75	11255999.75	3937356.87	1029.94	7567. " 9	-505.02
1874.51(3-	153' 2279.97	11243257.37	9034933. (-869.92	-7366.67	-479.4
1876.5615-	12304677.87	11233764,87	8933278.00	-764-04	-2236.40	-371.91
1861.7476-	15307917.12	11226932.50	9932180.12	-695.48	-2140.09	-332.81
1583.7964-	153, 93. 162	11272609.00	8931527.07	-65 .12	2 8 . 4	-3163
1845.8882-	1531 7635 . 25	11218312.62	9030809.17	-671.87	2: 27.43	-269.53
1868.0803-	15312511 42	11208174 42	9929530 . 41	-589.34 -574 SK	1921-72	-245 - 71
1893.1665-	15314925.62	11204103.12	8929276.50	-569.51	1890.84	-245.05
1895.3364-	15316159,87	11200031.62	8928478.87	-568,16	1861.76	241.26
1898.4735-	15317939.51	11194247.0/	8977716.25	-566.36	-1826.02	-244.90
1900.5215-	15419173.87	1119 1526.8	HUZI16.12 8925924.87	-568.85	1847+13	-241+77
1933.8633-	15338775.75	11135568.57	8919986.00	-615.54	1402. 5	-171.88
1939.0054-	15341947.87	11127952.12	8919152.25	-618.20	1470.22	-152.40
.1941.0635-	15343223.00	11124932.75	8918849.12	-620.91	<u>1463,91</u>	143 - 17





Table B-1.Reconstructed Reentry Trajectory,
ECI Coordinates (Continued)

TIME	*	~	-	* 0.07	MOOT	TOOT
1100		1	1		1001	2001
L'ART -	PETT.	11.11	LEIL	FIZSELI	IF IT SECT	しゃりくろもしま
1944.1646-}	5345147.37	11120417-62	3918477.25	-42*.24	-1452.67	-141.13
1946-2056-1	5345417.62	11117449.75	918128.[[-624.5	-1448_76	-132.54
1948.2983-1	5347726.37	11114472-37	:917856,50	-+26-17	-1444.47	-126.85
1951-3643-1	5349649.50	11110004-75	1917475.75	-628-39	-1437-37	-120-88
1953.4502-1	5357 960. 25	11107013-12	1917774.17	-478.28	-1431.05	-121-43
1055 4055-1	5 25 3 745 63	11174/80 37	2014071 87	-474 43	-1423 60	-174 81
177267703-1	777224747	111 4 64.37	1110711.001	-0/0+07	-1-22.00	-124471
1420-0(.32-1	J2247AA*21	11.99084.12	441034/.1/		-1912-23	-120-21
1960.55(4-1	5355495_37	11096795.75	2916316.87	-633.55	-1415.2	-137-98
1962.6982-1	5355920.37	11093922.37	8916943.50	-640.99	-1401.20	-134.68
1965-8032-1	5358787.75	11289588.12	#P15614.67	-639.14	-1390.65	-142.14
1967.8506-1	5360100-75	11.086743.75	8015377.75	-643.47	-1387.89	-136.60
1960.9414-1	5361450.33	11.393866.75	8915 48.37	-647.57	-1385.77	+132-14
1073 5034-1	5343436 6	11070415 50	8014445 43	-445 57	1777 11	-127 03
171340039-1		11074012625	1-1-0-7-02	-0-2-33	-121/+11	-12-472
1913-0-919-1	2-20-119-1:	11.10/95462	0919 1 'Sall'	2042.47	-1364.17	-100-14
1977.1416-1	5366(97.75	11773947-37	8914111.CC	-639.10	-1363.26	-129.27
1980.2036-1	5368163.37	11069785-37	8913717.37	-644.83	-1253-32	-127.79
1982.3252-1	5369420.01	11066921-12	8913449_25	-634.05	-1349.59	-125.01
1954.3804-1	5375726.01	11-64154.75	P913194.37	-636.91	-1347.4R	-123-11
1989.5674-1	5 174734 . 21	11 357232.25	8017566.**	-678.68	-1276.70	-126.97
1002 7114-1	8376480 4-	11051750 00	8013035 50	-438 63	-1314 77	-176 40
	23/303-40	110-11-59.	1917 274			
1948, 8402-1	2214481+6.	11.44975.0020	4011384.31	~0.54+72	-13°Z+00	-122.02
2000.9546-1	5381284.0V	11042293.67	8911138+25	-631.69	-1301.12	-115.47
2004-0864-1	5383266.5(11038230.62	8911780.25	-634.45	-1293.66	-112.21
2006-1372-1	5384559.11	11035587.57	891 547.75	-676.73	-1284.74	-174.49
2008-2244-1	5385035.3"	11032957.57	801 1348.12	-697.7*	-1245-66	-76.89
2011. 2866-1	5388174 41	11070714 75	8014150 02	-777 79	-1100 20	
2013 3344 44	528047F AT	11024705 #2	012044 02	1 1 4 4 4	-1100 34	
2/15-5/10-1	23845(2.8	11-120(22+2)	0.41.46.00*61	- /53.74	-1190.34	-41.73
2015-4243-1	5391222.21	11024285+07	8909982.87	-755.87	-1156.38	-47.11
2018.5225-1	5393612.5	11 22 64 7. 62	8939891.12	-767.17	-1162.38	-19.09
2020.5713-1	5395236+37	11/18279-12	# 31.986F .62	-797.95	-1144.65	-2.95
ZC 22.6245-1	5396869+25	11(1592).12	6009974.12	-792.62	-1148-77	8.21
2025-7222-1	5399334.37	11012365.62	8909893.87	-798.98	-1146.96	2.58
2027.7715-1	54C+075-62	11010011.75	8909880.50	+832.84	-1150.65	-12.70
2020 8433-1		11007407 47	8000847.47	-876-67	-1152.29	-23-44
202700033-1	CT_20270((11.0.4070 47	80/0778 75	-9/5 10	-1151-11	-18.32
ZF-52-9229-1	2417124462	11.0.41 1.0.62			-1154 (3	-11 77
	54/15795.62	374.36 (4*42)	84 4141681		-11:	~11431
2037-0635-1	5428444.25	1. 999293. 75	89. 9727. 97	<u>+877.57</u>	-11-54	
2040.1646-1	5410927.37	10995703.47	8909712.50	-8-0-87	-1167+17	-3.19
2047-4033-1	5416714-37	11987235.00	8909627.87	-798-04	-1151-04	-19.64
2040.45.12-1	541 3351 .12	10084974.87	8999591-75	-801-13	-1151.19	-16.13
2047643/2-1	241322646 E453084 87	1.002433 43	1000561.50	-794.04	-1157 - 46	-17-93
20314 4937 1		1 742021842	0000533 35	-70(-1140 8	-11 .72
2034-6135-1	********	1	87:9727427			.15 .99
2056-6504-1	5424:07,25	1-974763.17	8 3 94 94 A	-794.75	-1143.74	-17.31
2058.7412-1	5425724.87	10974266-04	8909466.87	-791.54	-1149.25	-12-12
2061-8032-1	542 9147.75	10970777.62	8909442.12	-799-98	-1155.32	-4.08
2061.8506-1	5479771 . 37	13966614-00	8969431.25	-795.11	-1153.62	-6.51
2048 0414-1	8431476 76	1 944661 17	10004-00-53	-797-02	-1154-57	-14.28
200747414-2	5433870 7E	1.043483 82	9010373 47	-799-31	-1163-33	-9.83
SC04*10034+5	7452579-75	1. 40.472. 7.			-1144 34	-7.68
2071-3-1	543.351.Z	1. 2011 2.2 . 5	40 01 04 04 21		-110-4-2-	
2073.1416-1	5437192.87	1-957645.62	94 9331.62	- 194+43	-1174-10	-14.49
2076.2036-1	5439625.37	11954135.75	8909283.12	-789.37	-1158.41	-17.29
2078.2915-1	5441277.12	10951747.87	8979255,87	-792.86	-1148.95	-9.73
2080.38 4-1	5447038.17	1-040373.0"	99:9747.75	-797.45	-1167.77	-3.87
20.82 4714-1	544673 PT	1 1044649.01	8959737.12	-8:2.56	-1165.16	-1.68
20020 7214-1	27772278 453 84472788 52	1-04775 75	80(0331 67	-789.38	-1151.76	-8-17
2002-2013-1	290 / 17 9 /		27 2221.02	-701 71	-1161 84	7.79
2087-6172-1	544 50 43 . 24	10440444 13	84142173.27	-191.11	-1157.04	-11 67
2089.7114-1	5457358.3	10938525-62	8999164.00	- 170.32	-1130	-11+73
2092.8115-}	5452819.6	10934951+12	80-0136-37	-791.57	-1147.00	- 19 • 8Z
30.04		12020/04 22		-700 44	-1126 -1	
2794-3673-1	7434429 . 4	1 19 326 5. 75	Bra.4034+25	- 100.00	-11-14-14	-71 - "4
2096.9546-13	54 <u>56(96</u> +6;	11930211.75	8919155.25	-794_95	-115(-16 . 51
2100.0112-1	5455538.8	17926670-00	9909313.5 0	-803.10	-1166.92	-10.83
2102-0962-19	5467203.50	10924253.00	8958967.07	-793.64	-1151.52	-14.56
2104-1543-1	5461874.12	10921898.25	8908950.37	-781-25	-1136-74	-21 -00
2107 7485-11	544753 57	1 019369 43	80/8801 47	-788-90	-1144.73	-16.05
3300 3044 11	/		AD. 3071006	-704 36	_1163 55	-12 -
2109-2904-1	24025/4.15	1. 416 17.37	5 ML 55 51 61114		-1177.77	-13.446
2111.3545-1	2907225.87	10913652.12	5905527.07	-109.16	-1197+95	-17.27
2114.4482-1	5469943.37	10910330.50	8908765+87	-786.63	-1173.59	-22.79
2116.4566-1	5471560.75	1097791.50	8906721-00	-792.65	-1150.29	-21.07
2121.6484-1	5475611.6:	10901914_09	8908596-62	-779.95	-1131.41	-27.21
2123.4714-1	5477101 A	1 180 CA 14 . 15	99 4547.25	-782-94	-1127-68	-71 -56
2128 8322 1	5481741 4T	1003763 87	80.8443	-701 34	-1140 64	-11 17
2120-0772-1		1 073/01 607		770 71	- 1136 70	-11.17
4130- 9176-1	295.2369425	1 891393	7-7 5951.0Z	-1/0, /1	-1157. 71	-14*45
Z1 36-0615-19	5456918.25	10885510.37	8908324.00	-788.68	-1149.49	-23.00
2138.1123-1	5468538.25	10883158.37	89:1276-87	-791+28	-1144. ³ⁿ	-27.94
2140.1992-19	5490178.37	13562783-12	8908221.75	-789.56	-1132.00	-33.00
2143.2474-11	54976E 8.42	1-877274-03	4904131.25	-788-29	-1133-33	-28.37
2145. 3854-11	5494755.87	10874803.37	8978078.25	-793.27	-1142-37	-27.55
2147.4904.14	5405803 AA	1/1073010 43	BOC 811412-11	-707 41	-1154 24	-14 41
ALTIAT207.1		L'ATERICAR	77 2 22 1	-700 40	-1141 22	-10 -01
2177.7 390-1	>=>======	1180 3960.25	5451457457	- 1-4(******	-11-1.22	-17.50
2152.5896-19	5499971.50	17566631.87	8977942.25	-793.25	-1140-41	-24.49
2154.6733-1	5501631.87	10864247.62	8907898.25	-793.56	-1142.91	-25.18





Page B-12

Table B-2a.Reconstructed Reentry Trajectory,
Special Parameters

	35/	INT & REENTRY(ESPOD'				
TIME FROM RETROFIRE (SEC)	INCETIAL VEL. MAGNITURE (FT/SEC)	PFLATIVE VEL: MAGNITUDE (FT/SEC)	INFETIAL FLT. DEATH ANGLE (DEGREES)	INFETIAL HEADING ANGLE (DEGREES)	ALTITUDE LEELTI	GEODETIC LAT. (DEGRECS)	GENDETIC LONG. (DEGREES).
2.225	25350.5	23975.0	36	_61_1 <u>C8</u> _	957112.0	817	19.987
4,667	2533 .7	23046.3	90	A1 "03	957 39 7	735	27.124
9,906	25251.3	23976 7	- 126	61.174	955788,7	- 573	29.396
12.427	25223.4	23878.8	152	61.117	956632.7	402	20.531
14.326	25199.	23814.1	187	61.132	956493.0	431	20.633
16.076	25170+2	23795.0		61+1*2	956269.5	- 349	29.769
21-906	25102.1	23717.5	? 7	41.11	955732	188	21.038
24.422	25293.7	237 9.2		61.11?	055470	1~8	21.173
26.77	25193.9	237.9.4	~.283	61.11	955198.5	745	21.277
28.876	25094.3	23759.8	287	63.111	954875.5	115	21.545
31.047	25.95.1	23710.4	~ 795	61.112	954230.5	.127	21.681
36.422	25005.4	23711.7	298	61.113	\$53958.7	.276	21.813
38.37	25:05.7	23711.4	- 21.2	61.11	353652.7	.379	21.917
40.876	25096.1	23711.7	~.306	61.114	953371.5	.419	22.051
43.390	25096.5	23712.5	- 313	61.110	952639.5	• 499	22.102
5^ 37	25:97.6	21713.3	72	61.125	9521 29.2	.7??	22.557
52.911	25007.0	7.717.7	- 3?4	61.127	751674.2	.813	22.693
55.432	25098.0	23713.7	327	61.124	051317.5	-897	22.828
57.941	25098.6	23714.3	332	61.126	950958.Z	1.043	22.902
62.795	25099.4	23715.2	339	61.131	951253.0	1.119	23.221
65.19*	25: 99 9	23715.8	742	61.134	960899.1	1.195	13.349
67.524	2511-2	23716.1	746	61.137	242537.2	1.273	>3.479
70.02	251**•7	23716.6	240	61.14	1491 <u>76+/</u>	1.35	!3 . 677
72.423	25100.9	23716.8	353	61.143	948811.5	1.426	23.735
76.4 2	25111.0	23717.9	- 359	61.149	948195.5	1.554	23.803
79.595	25102.3	23718.2	364	51.1*4	947699.7	1.655	24.118
81.996	25102.8	23718.8	367	61.15P	947320.5	1.732	24.246
84.423	25103+2	23719.2	371	61.167	946933.5	1.809	24.376
50 • 197 89 - 724	25195.7	23719.8	+,5/4 	01+10/ 61-172	946551.7	1.963	24.513
91.574	251 4.6	7172.7	- 281	61.174	945754.2	2.039	24.761
94.23	2510.5-1	23721.2	235	61.187	945357.5	2.116	24. 889
96.396	25145.6	23721.7	289	61.JRT	944971.7	2.192	25.(16
98.795	25106-2	23772+4	393	61.19	944557.7	2.258	25,145
103.595	251 4.9	27723.1	- 4	61.2.7	643749.2	2.421	25.402
105.996	251 7.6	22722.7	- 413	61.2"9	043325.(2.499	25.530
108.367	<u>251_3</u> _(23724.2	4 .7	61.216	742922,	2.574	25.657
112.523	251 5+4	23725.1		51.222	942491.	2.572	25. 198
115.595	25139.6	23725.8	417	61.235	941643	2.814	26.044
117.996	25110+6	23726.3	421	61.24?	941 ?11.7	2.987	26.173
120.396	2511.5	23776.8	425	61.249	94 775.5	2.957	26.201
122.195	25111.5	71777 0	- 429	61.761	040037 0	3.085	20.4517
127.624	25112.1	23728.5	435	÷1.271	939443.2	3.187	26.689
130.023	25112.6	23720.0	439	61.779	978097.7	3.264	26.817
132.4?3	25113.2	23779.7	43	61.787	938546.5	3.34	26.946
134.795	25113.8	777. 6	445	61.275	938639.5	3.472	27.073
1210172	2 . 2 . 7 . 2				• • • • •	7. 4 7. C	7 • • • • •
139.595	25114.9	23731.3	• 453	. 61. 312	937167-2	3.568	27.331
142.027	25115.5	23732.0	- 454	61.171	936634.7	3.045	27.401
146.823	25116.5	23733.2	463	51.338	935751.7	3.798	27.719
149.224	25117.1	23723.7	467	61.347	935274.5	3.874	27.848
151.624	25117.7	23734.2	471	61.357	934793.7	3.950	27.977
153.996	25118+3	23734.9	474	61,367	734315,5	4.726	28.174
158.873	25110.2	22726	481	61.386	(1111) 7	4.179	28.364
151.224	2512 (23736.6		61.307	937837.5	4.255	28.493
163.624	2512 .5	23737.2	- 488	61.407	922239.5	4.331	28.622
166.023	25121.1	23737.8	491	61.418	931838.3	4.409	28.751
100.425	25122+8	1_017	- 498	61.439	930831.7	4.559	29.008
177.472	25122.8	22729.6	5 1	61.447	93 485.	4.61	29.095
175.624		_2374(+3	- 535	(1.462	179799.	4.712	29.268
178.023	25124.3	23741.1	519	61.473	929285.5	6.789 A 044	29.397
187.873	25124+9	23747.3		51,4955 61,496	424158.7	4.804 4.040	29.654
185.224	25126.2	22743.1	- 519	61.505	a777 15	5.16	29.785
187.624	25126.8	23743.7	52?	61.521	127173.	5.092	29.915
190 . 23	2512 . 6	23744.5	536	61.534	26637.5	5.167	30.134
192.423	27128+1	23745.7	727	01+390 61,550	201349.0	7+243	30.374
197.224	25129.4	23746.4	537	61.572	525(11.0	5.395	30.433
199.624	2513	23747.	54	61.585	\$24461.7	5.471	33.563
202-023	2513(.5	23747.5	544	61.590	973979.;	5.546	30.693
204.409	21131.3	. 23148+4	547	01.612	977 356 . *	5.627	57 . 877

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TIME FROM RETROFIRE (SEC)	INFETIAL VEL- MACHITUDE (ET/SEC)	AGNITUDE (FT/SEC)	INTETIAL FLT. PATH ANGLE (DEGREES)	INFOTIAL <u>NTADING Angle</u> (DEGREES)	ALTITUDE IFEETL	GEDDETIC LAT.	GENDETIC LONG. (DEGREES)
216.823	25132.0	23749.1	-1550	51.626	922794	5.698	30. 952
2.09.224	25132.0	22761 6	- *57	6] . 645	077731.0	5.773	31.042
214 23	25134.2	23751.3	565	61.669	921096.0	5.925	31.342
216.423	25134.6	23751.8	564	61.683	9271523.2	6.940	31.472
218.79R	25135.5	23752.7	567	63.697	919953.7	6.775	31.600
220.435	20100.0	23122+	574	61.727	919557.7	h+127	31.059 31.861
275.990	25137.4	23754.7	= 77	41.743	919775.2	6.31	31.991
228.358	25138.2	23755.5	585	61.75	917616.6	6.377	32.121
232.798	25138.9	23756.3	-,594	61.774	917023.5	6.452	32.251
235.599	2514(+4	23757.8	-,Kan	61.805	915828.0	6.603	32.512
237.997	25141.2	777FP. 6	574	61.821	11.5725.2	4.678	32.642
240.398	75141.R	72750,7	597	61.939	914610.5	6.753	32.773
245.198	25143.3	23760 A	-+0%10 +,674	61.871	91-397.5	6.913	33.034
247.599	25144.5	23761.5	607	51.888	912781.2	6.979	33.165
249.997	25144.7	23742. 3	61)	61.975	012162.2	7.54	13.295
272.354	20147.3	7767.8		61.941	911543.7	7.204	33,422
257.198	25147.1	23764 6	(21	61.977	010785."	7.279	33.658
259.599	25147.8	- 73765+4	624	61.975	909652.0	7.354	33,818
261.997	75149.4	23746.0	-,627	63.994	0.14(16.2	7.478	33,949
266.793	25155+0	7.7.7		67.131	C17735	7.578	34.711
268.438	7515 .7	7744.4	535	62.43	97794.5	7.679	24.371
271.599	25151.7	*375°.4	44`	67. 68	or +441."	7.778	34.474
973.090	75152.2	71760.0		67 387	005780.5	T 807	14.475
276.39*	25353	7	647	4 1 4	015134	7,877	34.736
278.799	25154.	6°12226		47.125	004475 F	7.951	34.868
281-198	. 25154.7	27772.5	-,453	47.14F	903814.2	8.776	34,999
285.999	25156.3	73774.7		62.165	907481.0	8,175	35.130
288.398	25157.1	22775.0	667	67.705	0^18^0.7	#.249	35, 394
291.799	25157.8	7775.7	467	67.775	201134-7	A. 324	15.525
203.109	25158.7 35150 F			47.744	97,454.7	e.394	35.657
297.999	25161.5	23778.5	676	62.287	809091.2	9.546	35, 921
300.344	2*151.3	23770.3	68"	62.205	898417.5	5.620	36.052
312.798	25147.1	7378-1	682	62-339	A97712.5	5.695	36.184
307.502	2010(**	23781 7	054	47 372	997-19.5	9.759	36.316
3.0.003	25164.6	23792.7		47,705	P9562 .7	4.917	36.501
312.398	25195.4	22793.5	69*	67.417	894017 n	8.991	36.713
314,798	25144.1	71784.7	698	62.439	R94715.2	0.765	36.845
310.500	75159	7776 7	- 7 - 5	67 484	997787.7	9.212	37.110
	/ ··· · · 7	5.744 <u>1</u> 5	- 715	17.17		0.201	17.243
224.230	25169.6	23797.0	711	47.5	891751.2	9.357	37.375
376.194	7517.6	23734.4	-,714	67 574	89:478,7	9.431	37.508
311.599	25172.5	22701.8	- 72	62.5	899174.C	0,580	\$7.773
313.971	75172.2	27791.f	- 774	02.614	P=F441.7	S. 454	37.936
336.398	75172.0		7.7	4 7 4.4 R	9977 6.7	2.727	38,739
1.9.7.4H	25 <u>1</u> 7- 1 1	5.1.14.2	/ 1	57 . 512	F+DF•7	9. M 21	38.172
341.198	25175.8	21774.3	737	52.697	886226-5	9. R74	38-305
343.577	25175.0	13775.3	7-4	7.771	835441.5	9.947	38.438
345,000	75177.6	>=764.1	7 . 2	62.744	E84733.7	• ?	38.571
340+354	25178.4	23776.9	746	* £ + 171 67.796	883229.2	10.166	38,794
353.128	2-187	73798.P	749	47.821	PR7477.7	10.239	38.971
355.500	25191.7	22200.0	**?	52.847	A41711.7	14.31Z	79.145
24' 200	7#187.7 7#102 1	,	755	(7,877 (7,877)	SR 048.7	. 395	19, 739
362.799	251 84	7 . 7 . 7	751	4 2.025	879413	14,531	39.536
354.438	251 94.6	72913.3	764	67.043		581	39.597
367.599	751.35.8	738~4	747	47.077	977853.5	17.676	39.774
307.999	22195.5	218 5.6 738 6.5	777	n 44,414 413,4131	8771 84.5 8763 3.2	740	39.978
374.798	75188.7	239.7 5	- 774	- 7 - F A	A75518.5	10.894	40.176
377.125	251 P9. P	278 P.6	- 779	f3, P5	87473.5	0.966	40.310
379.599	25199.5	728°0.4	783 - 785	57.113	R77939.2	1.039	47.444
394.398	25107.4	23811.3	788	63.168	877348.2	1.183	40,713
186.798	25103.7	22612.6	797	1 2.196	971548.2	1.255	47.848
399.198	251 34 4	23933.5	795	43.774	RT: 745.0	1.327	40.982
301.509	25125.5	23914 6	-,798	63,253	860038,2	1.399	41.117
376.384	25197.5	23916.5	813	63.711	868322.0	.1+*[1	41.386
378.771	25179.4	73417.5	876	63.319	867=11.2	1.614	41.520
4-1.17	25129. 1	27818.4		62.769	844497.7	1.656	41.655
407.500	2520-+5	22812.6 22827 A	R12	63.297	845841.7	11.758	41.792
	176 1+7	alian 🔹 🍽	· • G* 6	المكاتبة منتعين		· · · · · · · · · · · · · · · · · · ·	





Page B-14

TIME FROM RETROFIRE (SEC)	INCETIAL VEL. MAGNITURE (FT/SEC)	FELATIVE VEL. MAGNITUDE (FT/SEC)	INTETIAL FET. PATH ANGLE (DEGREES)	THEFTIAL HEADING ANGLE	ALTITURE [FSFT]	CENDENIC LAT.	GENDETIC LONG. (DEGREES)
428.398	252.2.4	23821.6	-,918	63.457	864212.2	11.902	42.162
41 - 799	25213+2	73977.4	-,827	47.407	943279.7	11.973	42-198
415.570	25215.4	73874.6	- 877	47 548	861775 5	12.115	42.250
417.971	25205.4	27825.6	- P31	63.578	84 98 7	12.156	42.603
429.371	25217.2	23876.4	P 33	63.679	861138.7	17.257	42.739
422.771	25229.5	23877.8	P34	63.643	850193.	12.329	42.874
425-17	252 9+2	73978.5	-,839	63.671	P59345.2	17.495	43.010
427.599	25215.5	73.87 0	- 845	A 7 777	957494	17,471	43.148
432.345	25717.6	23832.1	847	63.745	A55797 2	17.617	43.417
434.746	25713.5		85	63,707	854937.F	12.682	47.553
437.146	25214.5	23834. 7	-,853	57.829	854071.0	12.753	43.690
479.545	25215.8	73835.7	455	52.843	8532-4.2	12. 974	43.826
441,045	75714.5	73836.1 32837 3	-,859	63,894	957335.7	17.994	43.963
444.774	78219.6	73838.7		47.959	850579.7	13.036	44.738
449.174	75219.0	23939.5	-,848	63.903	849701.7	13.175	44.375
451.545	25220.8	23849.5	-,871	54."?5	848831.7	13.176	44.510
453.946	25221+9	23841.4	273	54. 5	947048.7	13.244	44.647
456.345	25.222.0	27 94 2 . 5	-, 674	64,103	847" 47. 7	13.316	44.784
458.741.	25226+1	17842.0			846174 T		44.921
463 575	25226.4	27846.7	- 894	64.196	844378.0	13.526	45.198
465.975	75277.3	23847.1		64.231	P43481.5	13,596	45.335
468.375	25.229.5	23948.4	-,895	44,745	PA752: .7	13.455	45.473
471.774	15229.5	22340.4	49?	64.300	841477.2	13.735	45.611
473.146	75732 A	32 95 0 5 5	POA	64.334	947791.5	13.814	45.747
475.545	25231+7	23851.6	998	54,349	839877.7	13.873	45.855
4/7.975	2573241 75732 P	71047.		· · · · · ·	82835	17.044	46.024
48	25234.9	77855.1	- 9°4	4441	438-34.7	14.013	46.163
492.174	75736.3	21856.4	- 919	64. F14	834100	14.151	404 371
497.574	25237.4	23857.5	712	54.556	835276.2	14.220	45.578
489.746	25238,3	23858.5	14	54.585	P34361.5	14.288	46.714
497.35	75229.5	12RE0.7	-1236	44.627	R73477.7	14.357	46.854
404.774	25247.46	23861.8	-, 970	44.450	R32401.5	14.475	45.993
497.174	25241.8.	. 27962.	-,923	4.4.694	. P21559.(14,495	47.132
499.574 503 075	2524 (# P	23865.2	- 029	44 771	930671.7	14.554	47.771
5.4.75	25245.3	73865 4	-,031	64.010	828746.5	14.733	A7.540
5 6.774	75745. 7	23965.4	- 937	54.P47	877795.7	14.769	47-689
5. 8.374	75746.9	27867.1	-,935	£4. 97?	R77165.1	14.914	47.781
511.574	25248,6	23959.2		44,973	P75999.	14,005	47.967
513.975	25249.9	2287.3	-,942	64.061	924944.5	14.973	48.107
515.177	10201	23971+3		65.000 45.000	#23C4#	15, 41	48.247
521.174	25253.1	2207104	- 049	45./78	922 48 5	15 176	47.574
523.574	25254.1	>1674 7	- 152	65.117	8711 4.5	15,744	49.666
525.975	15255.5	77874 1	- 254	15,151		3 = 33 2	AB 877
578 375	CE051.4	23677.1	477	65.196	R19169.7	15,370	48.947
53 774	25257.9	23878.5	96	65.226	918197.	15.446	49.087
523.174	25259.	23870.7	943	65.276	917777.7	15.514	49.228
537 075	753/3 5	73007 2		48 357	816744 T	15.741	97.505
54 . 74	25343.5	22892.7	97 -	45.307	514787.7	15.714	44.734
	- / •	•	•		•••		
\$42.774	252 63. 7	23824.5	673	65.438	A1 3204.7	15.782	49.798
F47-574	25266 2	22021	- 078	2 F 8 3 7	P11330 7	14,442	49,931
549 C75	-5-47 3	13400 7	- 00	65-562	81 375.7	15,092	53.214
552.375	25258.5	11904 5	- 987	45.67	8 0770 7	16.348	50,755
554.774	25259.8	2380" R	084	45.646	A18331.7	15.115	50,497
556.415	25277.5	23901.A	087	55.674	8 7547.7	16.157	50.593
550 574	25272.5	2°2°2		4 5 • 72Q	B 4774.5	16.747	57.780
561.075	25277 5	77894.8	cai	55.777	915319.5	16.313	50.922
566.774	25275 0	73977 1	- 009	-5 650	AC2200 7	15.579	51.754
569.174	**277	72909.7	-, -	65.01	9-2-84	16.511	51.348
571.574	2577P 3	27870.4	-1 - 7	45.943	8 1269.5	16.576	51.490
572,975	75279.4	8. "P\$¢	-1, 15	65.987	8 25	14.442	51.632
576.375	75257.6	120.1 0	-1-19	66+131	799778.7	16.7.7	51.775
578.774	25232 . [227-3,3	-1. 1	F.F.#174	799223.7	14.773	51.918
541.174 543.574	75247.2	73075 9	-1. 12	55+138 44 143	797177.2	15.838	52.060
585.975	75225 R	73977.7	-1-17	50+10/ 56-217	795116.7	15.915	52.344
588.367	74295 P		-1.	.4.757	794 87.7	17.032	52.488
50 . 774	75269.2	710 0.7	-1." ??	46.705	732 44 5	17. " 9R	57.633
593.174	25289.5	73911.3	-1.24	66.341	70215-	17.162	52.776
595.574	25203.7	73912.3	-1, 26	66.787	790957.7	17.227	57.919
597.975	25292."	23013.6	-1.220	55.432	790019.7	17,291	53.063
619.075	25273.5	73014 7	-1 34	55,574	787833 7	17.176	>3.277
6 4.415	75205.7	710.7	-1.135	A	787111.7	17.444	53.550
517.574	25297.2	23910	-1. 32	66.616	785716.2	17.548	53.638





TIME FROM RETROFIRE (SEC)	HEPTTAL VEL. HAGNITUDE	LATIVE VEL. AGNITUDE (ET/SEC)	INCOTINE FLT.	TAUERTIAL HEADING AND IDEGREESI	ALTITUP" (FFET)	ECODETIC LAT.	GENDETIC LONG. (DEGREES)
6.39.975	25298.3 -	23922.1	-1.041	65.662	784659.2	17.612	53.783
612.375	25229.0	23971.7	-1. 41	66.7.9	783634.7	17.675	53.927
614.774	2531.	23972.8	-1, 45	56.755	78223647	17.003	54 314
617-174	253:2+3	23924.1	-147.	AL 857	74/4/8.2	17.866	54.361
614.574	25334 0	73976 9	-1.757	66.897	779339.5	17,930	54.506
521.47/3	25374-1	33 978 1	-1.055	66.945	778747.5	17.993	54.650
625.774	25307.3	1020	-1 57	66.993	777193.7	18.056	54. 796
629.174	253 9.8	7107(P	-1.059	67. 41	776117.5	18.119	54.941
631.574-	2531 1.1	72932.2	-1.251	67.189	77503945	18+192	55.086
633.975	25311.3	23033.5	-1.63	67.138	773958.0	19.244	55.232
636.360	25712.5	23034.6	-1. 366	67.186	772881.5	19.357	55.376
638.774	25313.9	23936-1	-1	67.235	.771789.5	18.359	776723
641.149	25312-3	22020 0	-1 77	67 222	749422.5	10.607	55-813
645 040	25317 0	2204. 2	-1.75	47.382	748530	19,556	55.959
648.250	25 31 9.1	23941.4	-1.077	57.43?	767434.7	18.619	56.105
651.753	25320.7	72943.1	-1,079	57.48?	766337.2	18.679	56.252
652.423	15321.5	23947.9	-1. 791	57.517	765570.2	19.727	56.354
655.521	25323+1	22045.4	-1.083	67.582	764147.7	18.61	56.543
657.921	25324.4	23947.0	-1.185	67.432	763/43.5	14.864	56.690
650.350	25325,8	23949.3	-1-189	57.683	761074.7	18.926	50.838 F(085
667.751	25327.1	73040.7	-1.000	57.754	767515.7	18.457	50,703
665.149	25323.5	23941.2	-1.00/		759500 7	10 110	57.200
667+549.	2223.1	23952.0	-1. 04	- 5/ * . S'	757497.	19,169	57.425
677.371	25332.5	77055.3	-1, 10R	7.010	754760	19.73	57.573
674 721	75334.5	73054 8	-1.15	57.95	755768.5	10,10.	57.721
	- <u>-</u>	Sector Production					
4 77 122	75335 3	73059 1	-1 172	19 517	754175 7	10 351	57. 84.8
679.571	2733743	22722011	-1.1-4	48. 15	763733.7	10,411	58.016
681.921	25337. 9	22951 8	-1.1.5	3P.147	751877.7	19.472	58.164
684.335	25329.5	77 967 4	-1.119	68.200	75.777.7	10.532	58.313
686.75*	25349.7	23963.7	-1.111	68.253	749509.5	19.592	58.463
689.122	25342.0	23965.1	-1.113	69.376	748479.0	19.651	58.609
691.521	25343.4	23966.4	-1.114	68.259	747243."	19.711	58,758
693.921	25344.7	23967.8	-1.117	60.413	7467 4.7	10,771	58.937
596.321	25346.2	72960.4	-1.113	58.466	745/ 44.7	10.831	59.155
69 <u>8</u> 721	25347.4	.23975.1.	-1.121	58.•5 <u>2</u>	743071.5	10,940	59.214
7137 540	73545.D 35354 5	2397148	-1.12!	68. 50	745145+5	14.424	54.575
705-349	25351.8	23075 1	-1 127	60.683	74:467.0	2 . 67	59.454
778.35	25353.1	73376.4	-1.129	69.739	739315.5	126	59,873
710 771	25354.6	73978 A	-1.131	AR. 707	738175.5	2 .154	59,951
713.122_		22970.2	-1.132	FR 947	737-19.7	2 .247	61.111
715.521	25357.3	23980.8	-1.135	48.073	735861.7	27.311	60.251
717.049	25358+7	?39#2.2	-1.125	68.959	73469P.7	2 . 359	67.473
720.35	25350+1	23093.7	-1.139	69.714	733526.?	20.417	6P. 553
722.75	25361.8	23935.4	-1.14	69.17	732742.	2 . 475	67.773
725 140			-1.147	40,174	711108 7	7 533	60,854
727.049	25254+4	22049.1		50,183	71 21.02		51+1-3 5
727 225	23-02, 2	22001 1	-1.149	40 205	727401 7	7 775	01.175
734.753	75768.0	77007 7	-1.145	60 353	77651 5	23 763	61.572
737.145	25371.1	73064	-1,151	40.470	775334.5		61.638
739.543	24371 7	12005 4	-1.153	49.444	774156.2	7 . 877	61.765
741.049	C5372 G	11036 0	-1,155	40.574	777975.5	2 333	61,911
744.352	25374.4	23975.3	-1.157	69.582	721792.5	21.995	62.063
746.750	25375.7	12000.6	-1.152	40.44	77 6 17.7	71. 45	62.214
748.349	25776.6	74***.7	-1.161	49.678	10917.7	21.084	62.316
751.547	25378.7	24112.8	-1.167	40,754	10232.5	21.150	62.518
753.949	25380.1	24714.3	-1.364	69.P14	717 41.7	71.215	62.67C
756.350	25281.6	241.5.9	-1.166	69.873	15849.	21.271	62.823
755.72	22253.0	24 11 7 . 2	-1.149	. 60.937	14654.7	71.376	62.975
743 543	25306 5	74.71 7	-1 1 71		17750	21.499.2 01.499.2	63.128
765.949	25337.5	76.111.0	-1 173	7 1 10	711550 5	71.407	63.633
768.350	75368.7	74113.1	-1.175	75.169	709855.7	21 548	63.584
770.75	75391.4	74 14.0	-1,176	7 . 779	739651.5	21.673	63.739
773.149	25391.6	24-16.1	-1.178	7	7/ 7445.7	21.657	63.893
775.549	25303.1	24 - 37 -	-1.1A	7 . 749	7 6737.	71.712	64-046
777.949	9 394.9	26 19.5	-1.191	77.41	7-5- 27.5	21.757	64.270
78:.335	25395.1	24 21.9	-1.143	7.47	7.3822.7	21.871	64.253
782.750	25397.6	24-72.3	-1.185	70.521	707601.2	21.875	64.597
785.149	25398.9	74 77.6	-1.196	7 597	751385.5	71.029	64.661
787.549	25405	240 25.3	-1.199	7. 653	70-168.	21.983	64.815
703 36"	294 1.8	74 76.8	-1.199	7. 714	6 9F 94 9 7	27.137	64.970
704 757	1291 366 75435 r	74.79.4	-1.177	7-,776	6 97777.P	77.97	65+124
796.390	25494.1	24331	-1 194	70 897	105444	22.144	65.279
799.549	25617.0	24037 0	-1 1 3A	70.047	072000." 404051 7	22.15	07.574 48 800
801.949	25409.4	24.34.5	-1.198	71-124	697877.5	22.13	070790 65.762
604.350	2541 . 5	74 76	-1.100	71. 87	691597.	27.356	65.898
876.75	25412.3	74 77.5	-1-2/1	71.149	69.759.5	77.4 9	66-053
809,147	25413.8	24030.	1.213	71.212	6891 75.	72.461	66.209





TIME FROM	INCREASE VEL.	PELATINE VEL.	IVERAINT ETA	INTERIAL	ALTITUDE	GEODETIC LAT.	GENDETIE LONG.
RETROFIRE		MAGNITURE	PATH ANGLE	HEATING LNGLE	IFEET)	(0500=64)	(DEGREES)
(SEC)	(+)/5/()	t+ (75c()	(1 + 6+ 8 - 8)	(.intherid)			
811.549	25415.4	24-45.7	-1.2"4	71.275	487899 F	22.613	66.364
813.949	25414.5	24- 42. 7	-1.716	71, 222	426651.7	77.545	66.520
P16,35/	75419.7	74.47.4	-1.2.7	71.412	AR5411.7	22.617	66.676
918.75	25419.5	24045.3	-1.7.0	71,4+4	+.8417C • C_	27.643	66.832
H21.147	25472.8	24 48.3	-1.717	71.504	F 52976.5	22.121	67-146
875.949	15474.2	24 40 R	-1.213	71.653	68:475.1	22.873	67.301
82P.375	25425.9	24:51.5	-1.215	~1. 772	6791 94 .7	27.774	67.456
83.750	25427.4	24153.1	-1.716	71.783	677037.	22.925	67.614
933.149		74-54.4	-1+218	71.057	A75655.5	72.075	67.771
835.549	2543	24/50+3	-1.270	77 087	67-432.	22+175	67. 928 68.085
840.75	75433 5	74 150 4	-1.772	77.748	672920.2	23.127	68.242
942.75	25434 0	24 6	-1,773	72.114	671661.5	23.177	68.490
844.70	25436.1	24 47.	-1.774	72.150	6758°°.7	23.711	68.537
847.549	25438.2	74- 44 .7	-1.226	??45	6691 <u>41</u> .	23+276	69.715
849.949	75410.7	247 45.7	-1+725	72.312	667876.Z	23.325	68.873
854.775	22441.7	74 48.0	=1.231	72.444	665357.2	23.474	69.187
857,125	76444 3	74 - 7	-1-732	77 511	464 00 *	73.473	69.346
AEC. 574	-5445.7	24 77.	-1.773	77,578	662818.5	23.522	69.574
861.024	25447.3	34°73.5	-1.725	77.645	++1546.7	23.571	69.663
864.324	25443. C	74775.2	-1.236	72.712	660273.7	23.619	69.021
866.775	2545127	74 76.4	-1.237	77.780	658908.7 487700 F	23.657	69.98F
904 <u>12</u> 5 971,524	~~~~	24.38 3	-1.747	77.014	156444-5	23.764	7:179
873.074	71454 C	74 1 4	-1, -41	77 004	155165.2	73.811	70.458
876.211	25455.6	27.02.2	-1.47	73. 11	657201.2	23.959	77.616
878.696	25458.1	24 . 94. 9	-1.247	73.12	652616.5	27.916	70.775
881. S	25457.6	24.04.7	-1.745	20,100	451335	23.953	70.934
807.574	754-1-1	74 97.R	-1.741	73.253	FE 133.7	24.00	71.496
885.024	2545245	14 39.4	-1.247	73.327	649744 7	74. 48	71.256
866.726	2542445	741 37 4	-1.742	73.445	644145 7	24.094	71 577
892.798	25467	74 01 0	-1.251	77.514	645265-5	24.173	71.689
895.497	2544 7.	74 74 .	-1.255	73.444	647505 E	74.233	71. 996
907.804	~54 ^{**} •*	74'07.7	-1.254	73.674	64737	24.279	72.057
922.294	2:472.2	24:00.4	-1.255	7 2 . 744	641114.5	24.324	77.217
012.696	23473-P	241	-1,756	73 914	6397^6.7	24.37	72,378
0(7,07	747544	741 14 2	-1.7*7	73 054	C384 5.	24.41	72.549
9.10	75479.4	741 5 7	-1,259	74. 77	135701 7	74.536	72.864
912.296	254 4.	24] 7.4	-1.76	74 CR	4345 2.5	24.551	73.124
914.656	25421.4	241 0.	-1.26?	74.148	433198.2	24.505	73.146
97. 705	75437.0	2411.4	-1.253	74.24	631291.7	24.647	73.347
919.4C?		?411?.3	-1.264	74.211	621584 F	24.684	73.509
21.877	25436+7	74112.0	-1.745	74.293	420274.7	24.728	73.672
974 774	25420.4	74117.1	-1.547	74 #72	A 744 37 3	74.014	73.000
937 1223		24112	-1. + B	74-1-1	475774 5	74. P6	74.151
931.525	25402.8	2412	-1 740	74.673	£24 1 .2	24.000	74.324
C32,007	75434.7	74172.1	-7.275	74.745	47770.7	24,945	74.435
236.297	25405.9	74173.7	-1.271	74.417	671393.2	24.099	74.648
041 234	25,00	74125.5	-1.577	74 26	£7 75.7	25. 41	74.811
047 575	TEET E	24178	=1,774		A17410 F	75.116	75:139
	•••	•		•	•••		
945.525	25512.7	24127.5	-1.775	75,111	416-97_E	25.159	75.393
749.775	746 4	24132.2	-1.75	75,105	£14774	25.2	75.467
951.775	755 5.4 J	24173.0	-1.777	75.750	411440.F	25.242	75.63r
953.125	255.7+1	74175.5	-1.278	76.373	612123.5	. 25.284	75.794
057 076	755.97	74137.1	-1.275	75.4^6	61°811.7	25.325	75.957
877.927	2557 . 1	7414	-1.78	75.44	6 -408.7	25.417	76.787
367 776	35613 6	24147.1	-1, 292	75.61	6 48 7 8	75.448	76.457
955.125	25515.7	74147 3	-1.787	75.7 4	4 \$475.7	25.438	76.615
°57.525	25.515.8	24145.5	-1.784	75 701	A 6143."	25,529	76.781
949.975	25518.3	24147.1	-1.784	75.956	6 Tane.7	25.569	76.946
972.317	25521+1	74148.0	-1.2A5	75.031	671490.7	75.618	77.110
979.175	20021+4	24157 + 3	-1.286	76. 83	508708.E	274047	77 443
070.525	25574 7	74153.7	-1.799	74.150	F97459_5	25.727	77.637
981.925	25524.5	24155.4	-1 -180	74 , 775	594119.5	25.765	77.773
984.375	25577.0	24157.	-1.789	76.311	594778.2	25.815	77.939
786.725	75529.7	24158.4	-1.291	76.387	593435.2	25.944	78.135
986.265	25530.6	24159.R	-1.791	76.440	F02517.5	25.970	78.218
991.575	75537.P	74162.1	-1.702	76.54]	59''47" 560471 F	25.920	78.437
993.025	25534. H	24254.2	-1.794	76.605	ERRIELE	27.094	78.778
998.726	25537.0	24167.4	-1-294	76.772	586706.2	26.034	78.936
10^1.125	25539.5	24169.	-1.295	76.849	585257.5	26.071	79.103
1003.525	25540.9	2417 .5	-1.296	76.927	58407.5	26.139	79.270
1005-925	25547.7	74172.3	-1.204	77.005	582657.0	26.146	79.437
1078.325	25544.3	24174.)	-1.707	77. 787	581375.0	26.18?	79.604
1010.776	25546.1	24175.0	-1.798	/ • 161	57945Z .r	26.213	19.771



-CONFIDENTIAL

TIME FROM RETROFIRE (SEC)	INFRITAL VEL. MAGNITUDE (FT/SEC)	PELATIVE VIL. MAGNITURE (ET/SEC)	INFRIJAL FLT PATH ANGLE (DEGREES)	INFPTIAL HEADING ANTIE IDEGREESI	ALTITUPE (EFET)	GEODETIC LAT. _[DEGREES]	GENDETIC LONG. 1986REESI
1013.125	25547.6	24177.4	-1.299	77.239	578597.5	26.255	79.939
1115.575	75549.4	24170.1	-1.700	77.317	577242.7	24.291	50.176 80.274
1(17.925	25552 6	7419.5	-1.305	77.676	574538.7	26.343	87.441
10 22.726	25554-2	241 4.3	-1.31	77.553	57-172.2	26.399	80.610
1(25.125	25555.9	74196.1	-1.302	77.632	571P13.2	26.474	80.778
1027-525	25557.4	24197.7	-1.772	77.791	569(93.5	26.504	81.114
1037.325	75551.6	2410.1 0	-1.74	77.87	567731.5	26.535	81.283
1234.726	25562.4	24102.8	-1.304	77.951	566369.0	26+573	81.451
1 36.365	25563.4	74172 8	-1.705	78,005	565437.5	26.596	81.567
1741.925	25557.4	241-9.	-1.306	76.189	562276.2	26.675	81.958
1-44. ??5	25540 r	24109.7	-1.2"7	78.27	561917.5	26.7°A	82.127
1146.726	2557.45	24211.2	-1.37	78,757	550543.7	26.74?	82,296
1.49+122.	2257244	747 4 8	-1.308	78.511	556A76.7	76.917	#2.635
17 53.925	21 575.5	242' 5.5	-1.269	78.592	555437 °C	26.847	82.875
1056.325	25577.5	24279.4	-1.3.9		554067.0	26,873	87.974
1~58.774	15579.1 25580 K	24211.7	-1.310	78.826	551324.2	26.977	83.314
1067.525	25592.2	24213.4	-111	78.017	=49051.7	26.968	83,484
1465.941	25594.1	74215.3	-1.311	78.998	548592.7	27,000	83.653
1068.287	25595.3	24716.5	-1.311	79.079	547226.2	27.062	83.993
1 73.131	2777/42	2422 7	-1.31?	2.743	F44457.7	2793	84.164
1-75.5	25522.4	74221.0	-1.313	15.326	5431 ar . 7	27.123	84.335
1077.910	C5592.3	24223.9	-1.313	~~ <u>,</u> 469	541713.5	_ 27.154	84.575
1080.300	25593.9	24225.5	-1.314	70,495	540235.5	27.194	84.677
1 97.7	75575.6	7477.1	-1.214	70,573	538057.2	27.714	R4.848
1 87.512	22529.5	7473.7	-1-314	79.739	576198-0	27.273	85,190
1089.901	0560015	24272.5	-1.315	79.921	534817.5	27.302	85.362
1792.51	2=6~2.2	24734 . ?	-1.315	70,004	533436-2	77.331	85,533
1094.700	25617.9 75675.6	74714	-1.716	70,097	537154+5	27.389	85.877
1.00.21	° ≖6 °7 . ?	747-9.4	-1.316	9.345	570287.7	27.417	86. P48
11-1.673	256: 8.9	24241.2	-114	87.237	52792' . ?	77.445	86,218
1174.272	2561 .4	74747.7	-1.217	Pr.371	526535.7	77.472	86.391
11	75612+4 25613-6	74744.3	-1.31P	80.400	523748.7	27.528	86.737
1111.5	25615.E	7474R 1	-1.219	P .574	522342.5	27.555	86.910
1113.97	75617.4	7475.	-1.319	91.65A	521975.5	77,592	87.082
1116.237	25619.1	14751.7	-1.319	P* ,747	518216.5	27.618	87.476
1121. 72	75677.2	74755 1	-1.318	8. 911	516828.2	27.651	87.599
1122.472	25623.9	24754.8	-1,319	e: _ee5	515439.2	27.687	87.772
1125.573	25625.5	74759 <u>5</u> 74742 5	-1 210	91. 81	514 49.7	27,717	R7.945 88.120
111 . 7	24.410.22	4767.7	-1,-14	41.052	513253.2	27.755	88.293
1132.233	2563.0	24743.7	-119	R1.34 A	517726.5	27.780	88.409
1135.5	<u>~~6</u> ~~.3	24265.5	-1.319	e1.423	518471.0	27.813	88.441
1127.00	25633.9	74767.7	-1.37	P1.503	515407.3	27+835	58.814 PR.958
1140.7		2277. 1	-1.37	P1.679	5 4794.	27.886	89.162
1145.273	54638° 0	76777.6	-1.32	P1.765	5°29°5.5	27.910	89.336
1147.500	7564 . 6	24274.2	-1.32	31.851	501576.5	27.933	89.510
1149.97	75447.4	14274.1	-1.1	91.937		27.957	89.684
1152.71	7566L,7	14778.1	-1.30	P2.723	402717.5	77.9R1	89.858
1157.11	25547.6	74721.6	-1.375	87.195	495976.7	28.025	90.207
1159.537	75440.1	24292.1	-1.32	R2.283	494531.0	28.647	90.382
1161.900	25657.9	24704.0	~1.320	87.369	493135.2	29+069	97.557
1166.777	75464.3	74739 5	-1.37	87 543	4 7 342.5	28,113	90, 936
1169.121	25455.5	242.77	-1.21	PT.AT	488045."	28.134	91.781
1171.5	25657.6	24777.	-1.37	97.717	487547.7	28.155	91.257
1173.992	25650.3	24223.6	-1.32	87.801	486150-	28.176	91.432
1179.7	25667.4	24777	-1.27	82.079	493354.2	28.717	91.782
118".24"	75663.R	247.78.4	-1.3?	63°.3'B	487398.5	28.231	91.972
1193.500	.25656.1	243	-1+37	83.154	481557.	28.257	92.134
1188.333	25657.8 75669.4	243 2.6	-1.72"	H 5. 247 83, 329	477759_0	28.277	42.309 97.485
1196.700	25670.0	24315.9	-1.719	83.417	476365 .	29.315	92.661
1193.1.1	7º 672.8	C	-1.719	87.515	474066.5	28.334	92.837
1195.57	25674.3	74309.5	+1.310	83,503	473561	75.353	93.013
1200.300	25677.9	74313.2	-1.319	83.770	471760.5	28.389	93.365
1202.700	25679.7	24315	-1-319	83.858	469361.5	28.407	93.541
1205.101	25681.2	24314.6	-1.319	R3.947	467966 • 1	28.425	93.718
1207.500	75687.9 25696 A	24319.4	-1.319	84.735 P4,174	456559.7 465159.7	28.442	93.894
1212.287	25696.3	24321.0	-1.318	34.212	463766.5	28.476	94.246



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TIME FROM RETROFILE (SEC)	INFETIAL VEL. MAGNITUDE (ET/SEC)	FELATIVE VEL. MAGNITUDE (FT/SEC)	INSETIAL FLT. PATH ANGLE (DEGREES)	INFETIAL HEADING ANGLE (DEGREES)	ALTITUDE (FEET)	EFODETIC LAT.	GENDETIC LONG. (DEGREES)
1014 710	55486 1	26272 0		0/ 3/3			0 / / 3 /
1214/123	25690.7	24325.5	-1.717	R4, 201	46-954.5	28.519	94.611
1219.1.77	25691.2	747-7.1	-1.717	R4 479	459555.5	28.525	94.778
1221.	25692.9	24378.9	-1.217	P4, *6 R	458154.7	28.541	94.955
1224-330	75694+6	24335.7	-1.217	84.657	456753.7	28.556	95.132
1220+120	25697.6	74333.7	-1.316	84.818	455305 3	25+272	95, 399
1231.57	25600.7	74336	-1.316	84.976	452557	28.601	95.664
1233.901	25771. t	24337.0	-1.716	P5. 15	451149.7	78.614	95.841
1236.300	257.3.1	24320 4	-1.715	95.1.4	440747.	78.63	96.018
1238.700	25704+7	243 +1 • 2	-1.315	85.194	448345.5	29.644	96.196
1241-154	25730.3	24345.0	-1.316	85.374	440044.0	28.674	90.313
1245.90	25759.7	7, 34 . 5	-1.314	95.463	444141.7	19.685	96.729
1248.31	25711.5	24343.3	-1.313	85.553	44774 . 7	28.699	96.997
125 .7.	_25713.2	24357.2	-1.213	85,641	441239.5	29.711	97. PR4
1253.1 1	25715."	24352.3	-1.313	85.734	439937.7	28.773	97.252
1257.91	25718.4	24355.6	-1.312	95.914	437136.5	28.747	97.618
1241 .787	2572 . 1	74757 2	-1.711	94 613	43 - 747.7	78.759	97.796
1267.777	75723.7	24350."	-1.211	R£.004	474374.5	29.771	97.975
1245.1 1	2=723.4	2476 . P	-1+211	R4.185	432033.7	_28.782	98.153
1267.5	25725+1	24357.5	-1.210	86.275	431532.7	28.793	98.331
1272.30	25728.2	24365.9	-1.709	86.456	428732.0	274713	98.688
1274 7	25721.1	74747.7	-1.3.8	R6.547	477331.7	78 874	98. 857
1276.315	25731.3	24369.1	-1.708	P6.6/ B	47639	28.831	98.987
1279.476	25733+2	24771.1	-1,307	Pf. 727	474547.	28.843	99.272
1281.875	25734. 9	24372+9	-1-327	26.813	423148.C	24.853	99.471
1284.775	25736.7	74374.9	-1.7.7	86.019	42174A.7	29,862	99,580
1246.447	25.745.2	743 0.0	-1.375	87.001	421755.1	78,971	99.759
1291.476	25741.9	24380.2	-1.3'5	87.192	417552.2	28.888	100-116
1293.847	25743. ?	24381.7	-1.305	A7.272	416170.2	78.895	100.293
1296.275	25745.0	243 92 . 4	-1-304	97.364	414755.7	28.973	100.474
1298.675	257 <u>56</u> C	24335+4	-1.773	P7.455	413758.5	28,911	100.653
13-3.474	25757.2	74388.9	-1-302	87.438	417563.5	28.975	101.012
1305-875	25751.7	24397.5	-1.301	87.729	4(9166.7	28.932	101.191
13-8.261	25753.6	2439?.5	-1.311	87. #20	477778.7	28.939	111.369
1310.647	25755.3	24394-2	-1.300	#7.911	4*639*+5	28.945	101.548
1313-047	75756.8	243 35. 4	-1.200	R#_TC3	4-4095.2	28.951	101.727
1317.975	27777.4	74290.4	-1.79P	PP4197	4 7189.7	78.947	1/2.788
1320.775	25761.9	24471.2	-1.297	88.278	411794.1	29.967	102.268
1322.675	25763.6	24473.7	-1.296	RR.360	300390.7	24.972	107.447
1324.35	25754.6	244 74 . 12	-1.296	8P.433	298427.0	28.975	102.572
1327.291	75768.7	744 7	-1.705	PR. 548	306658 3	26.084	172.042
1332.159	25770.1	74410.4	-1.233	PA.731	103001.7	· · · · ·	15 3-157
1334.092	25771.3	24411.2	-1.203	88.815	397774.0	28.991	103.302
1334.059	25773.3	24413.7	-1.792	98.015	39111(.5	78.995	103.517
1338.891	25774.5	24414.5	-1.201	49,989	389991.2	28.998	103.661
1343,493	25777.6	74410.0	-1.299	80,173	38771 5	29.113	104-021
1346.56	25770.E	2447 .1	-],798	80,787	185540 F	70, 174	1 4.236
							·
1351.353	3/51+1	29421+5	-1.285	27+355 80-447	384432.	29.007	104-381
1257.291	5794 E	74475	-1.786	39.541	381655.0	29, 11	174.741
1356.159	.5785.4	24427.	-1.285	99.65	770004.7	29.12	194.956
1358./ 97	-5787.9	24478.5	-1.285	59. 774	378886 .7	29.111	105.101
1365.996	25789.P	24436.6	-1.294	89.835	377202.7	29.013	105.319
1365.795	22/91+1	74434 1			376108.5	20.014	175.461
1367. 59"	25794. 3	74435.2	-1.291	or	173120	20, 14	105.822
1371.595	25796.3	24427.4	-1.29	· . ? · ·	371664.5	79.13	196-040
1377.49	25797.5	24438.7	-1,279	00.276	371 572.2	29.113	106.142
1377.325	25794.4	7444" . 8		90.388	368898.7	29.112	106.400
1399.195	25612.9	74444 7	-19870	911+46Z 00_571	-0//81.5	29.011	106.741
1342.135	25834.5	24445.6	-1.2**	91. 646	365119.7	29.9.7	106-907
1354.006	258:6.0	24447.6	-1.274	9. ,755	367374.4	29.055	107.122
1386.936	258 7.2	24448.9	-1.273	90.830	362259.2	29.013	107.267
1309./95	25816 4	24450.8 26482 3	-1.273	99.440	360616.5	29-030	197-482
1394.637	2291.00	74474.1	+1+271	91.125	379503.	78.908 78.004	107.628
1396.534	25813.4	74455 5	-1.269	91.198	356749-2	28.991	107.989
1399.437	25415.3	24457.5	-1.268	01.316	355-86.5	29.987	108.207
1401.371	25816.8	24459.1	-1.267	91.384	353979.r	28.984	108.352
1474-235	75818.5	2446*.9	-1.766	91.494	352 337.2	78.975	108-568
1409.039	2753787	24416.7	-1.267	01.678	349501 7	25.975	108.713
141 .970	25822.8	24465.5	-1.263	91.752	348487.7	28.965	109-074
.1413,838	25824.5	24447.3	-1.261	01.442	346851 .2	28.959	109.290

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TIME PROM RETROFIES (SEC)	INFOTIAL VEL- MAGNITUDD (FT/SEC)	RELATIVE VEL. MASHITUDE (FT/SEC)	DATH ANGLE DATH ANGLE (DEGREES)	INFRITAL HEADING ANGLE (DEGREES)	ALTITUDE (FEET)	CODDETIC LAT. (DEGREES)	GENDETIC LONG. (DEGPEES)
1415.771	25825.R	24468.6	-1.261	21.937	345747.2	28.954	109.435
1418.438	25877.7	14471 7	-1,240	97.17	344111.7	79.943	119.796
1423.478	25837	24473.0	-1.257	2.232	341253.2	79,035	110-015
1425-371	25431.7	74474.7	-1.256	92.204	340275.5	28.930	110.157
1428-277	75834 6	24476.7	-1.255	92.415 97 ACO	338621.7	28.921	119-376
1433.778	25 935.2	74470.6	-1.253	92.599	335893.Z	28.907	111.737
1435-111	25837."	7449".5	-1.751	92.473	334795,5	29.971	110.882
1437.877	25838.6	244 92 . 3	-1.249	2.783	333170-0	78,891	111.097
1439.812	278254	24444, 7	-1.748	97.857	337455.7	27.374	111+245
1444.611	25841.7	24495.6	-1.246	93.741	329356.?	28.867	111.674
1447.478	25842.1	744 37.1	-1.744	93.151	327736.6	29. 856	111.819
1449.445	25944.1	24499.7	-1.743	73.776	376674.5	28.949	111.067
1454.746	25846.2	24490 5	-1.749	97.419	323015.7	28.829	112.328
1457.478	25847.1	24401.5	-1.238	93.515	322325 .7	28.817	112,541
1459.(45	25847.R	244 92 . 3	-1.236	03,503	321212.5	28.808	112.688
1463.845	75840 6	74404.7	-1,734	776	318514	29.797	113-049
1465.790	2585 . 4	244 95.1	-1.233	02 851	217472.5	28.778	113.195
1468.646	25851.2	24496.	-1.232	93.961	315826.5	28.764	113.410
1470.589	25851+6	74495.5	-1.237	04 145	214731.2	24.755	113.773
1475,300	2763242 7F857.7	-4407.0	-1.227	04.718	312745.2	29.730	113.916
1478. 770	25,853,5	74408.7	-1.275	C4.379	31-431.7	29.715	114.133
1487.080	25852.7	24400.1	-1.723	94.511	317752.5	28.689	114.493
1497.854	25854.Z	24499.9	-1.222	94.693	315092.5	28.663	114.851
1492.654	25 85 . P	244 30.4	-1.717	94. 874	3 2475.2	28.635	115.211
1497.53	25957.4	744 97.4	-1.212	95.767	299738.5	28.605	115.574
15-2.299	25852.2	74498.4	-1.217	95, 743	297083.7	28.575	115.934
1504.232	25851.7	24408.	-1.279	95.316	2967 16.2	28.562	116.078
1507.100	25851.0	24407.4	-1,207	05.426	294434,7	28.544	116-293
1512+752	75947-6	744 75. 7	-1.212	95+672	291597.5	23.509	116.840
1516.545	25846.2	24493	-1.2.1	95.785	200230	28,479	117.000
1518.712	25845.1	24401.0	-1.199	95.866	288050.0	28.464	117.162
1520.871	25843.4	74497.5	-1.198	95,949	286867.5	28.446	117.323
1526.223	25836.5	74435.7	-1,197	06.147	283043_0	28,498	117.772
1528.347	25836.7	744 43.4	-1.191	* . 232	292783.5	28.392	117.881
1531-533	25873, (2449.0	-1.189	06,315	291534.6	_ 28.376	118-044
15:3+735	25878.9	24475.3	-1.186	96.517	279854.5	27.351	118.253
1538.029	25=25.6	24469.2	-1.182	96.600	277527 7	28.317	118.603
1540.103	7501E 7	74462.4	-1.170	06.691	276376.7	28.299	118.751
1543.377	258 7.4	24455.5	-1,174	04.P 4	274646.5	20 273	119.070
1547.667	25794.7	74447.7	-1.169	95.967	277347	24.23	119.370
1553. 52	75775 P	24424.1	-1.153	97.172	25945R."	78.19	119.720
1555.216	25747.7	24415.7	-1.160	97.254	268314.0	28.171	119.880
1557-345	25759.2	744 5.P	-1.157	97.417	76719.	28.157	120.108
1561.67	75730.4	74339	-1.15	97.494	264 9.18.7	28.11	120.358
	·						
1564-860	25723.5	24372.3	-1-144	97.417	263235.7	28.08	120.594
1567. 71	25712.1	74751.	-1.14	~7.496	262318.2	28.06	124.753
1571.332	25667.9	24376.7	-1.120	97.8F1	759P77 5	28.023	121-072
1574.536	25657.5	24315.7	-1.123	97.967	258225.7	27.993	121.307
1576.654	25657.3	243 7.5	-1.119	98.142	257141.2	27.973	121.463
1580,034	27625+7	24 24 (+ 5	-1.114	98.116	756052.7	27.951	121.620
1594,175		76744 .7	-1.1.7	69, 303	25335- 7	77.893	122.013
158£.254	25579.5	24238.1	-1.398	OR. 375	252298.2	27.877	122.168
1588.391	75559 r	242 18.6	-1,003	98.447	251222.2	27.555	122.324
1593.697	25516.7	24156.4	-1.079	99.519	251158.7	27.800	122.481
1595.054	74423 4	24117.4	-1. 75	98.700	247541.7	77, 773	122.859
1597.995	25459.B	261 10.7	-1. 69	98.772	246511.C	27.755	123.024
10' +133	25325.4	24. 44. 4	-1.085	3P.845	245464.7	77.731 77 402	123.180
1415.455	25359.4	74 18 1	-1.149	99.173	242915.2	27.+ 1	123.565
1697.599	25339.	33080.0	-1 42	99.091	241903.7	27	123.720
16-0.733	253 7.	11950.5	-1	00,159	74- R95 . 5	27.4	123.074
1012+497	25267.4	27772.F	-1, 79	14. 41	239417.5	27. ***	124.172
1617.147	25194.6	77.845 1	-1.18	09.396	237456.7	27.	124.497
1619.298	25159.3	238-9.7	-1.12	99.465	236473.	27.5	124.561
1622.498	25105-3	23755.7	-1.002	N9.564	235024+2	27,48	124.790
1674.749	20 05+3 25124-0	21/10.K	+,977 +,991	94.620 00.60t	274196.5	27.453	124.938
1528.071	24596.0	73476.4	984	97,761	232193.7	27,414	125.243





TIME FROM RETROFIRE (SEC)	INSPTIAL VEL: MAGNITUDE: (FT/SEC)	RELATIVE VEL. MAGNITUDE (ET/SEC)	INTETTAL FLT. PATH ANGLE (DEGPTES)	INFETTAL HEADING ANGLE (DEGREES)	ALTITUDE 	GEODSTIC LAT. (DEGREES)	GENDETIC LONG. (DEGREES)
1632.061	24919.8	2357".5	077	99.855	231785.0	27. ???	125.468
1634.197	2487?•°	23527.4	971	99.916	22986 .7	27, 157	125.015
1636.212	24923.5	23204 0	055	150 (66	2776 4.5	27, 201	125.558
1641.616	24742+1	21341.3	- 047	1 . 125	226691.5	27.255	126.140
1643.746	24631.6	23282 4	941	13.185	225801.0	27.247	126.238
1545.874	24571.4	23222.2	-,933	17.241	22497 5	27.215	125.435
1549.57	24478.4	23120.2	<u>.</u>	1	222749	27,151	126.815
1651.216	24412.7	27 6	- 016	1.447	221911.2	27.126	126.950
1655.474	2424010	22927 2	- 0^2	101.409	221056.2	27.130	127.198
1658.652	24171.6	22822.4	8 91	101.577	219812.5	27. 61	127.215
1665.774	24197.2	22748.		1	218002.5	27.036	127.459
1662.012	24122.1	??(??.9	1993		218172.2	26 044	127.060
1668.213	13870 . 8	2749.4		1.5	21626 .7	74_077	128.102
1670 . 34	0. 23745+9 . 03867-8	22313.4	- 884	101.868	214554	24.994	128.243
1677.913	23442.4	22 77 8	896	100.967	212547.1	26.829	128.596
1679.94	22240.8	··· •1	294	111.709	211753.2	24.803	128.736
1692.56	23256.5	210 6.7	997	1 1.142	21 942	26.777	128.875
1684.204	2216 .5	7191.9	239	1 1.7 21	21' 148.7	26.751	129.013
1497.414	23116.6	21664,7		1.11.150	300104 6		129.221
1689.541	22916.2	21000.7	077	1 1.179	207384.2	25.651	129.493
1691.001	2271.2	21359.0	- 945	1.1.103	2^6583.5	26.535	129.674
1696.654	20533.1	21212 6	-1. 35	1 1.217	2 = 10A.C	26.611	129.818
17-1-672	273 C.O	2 5.5 . 2	-1.211	1/1.280	2 3174.2	26.541	13n.122
17:3-545	27125.6	21.945.1	1 .2.9	101.304	2,5163*.	74.519	130.239
1706.627	22024.4	2:673.9	-1.431	101.373	201551.7	25,483	130.427
1778.792	71992.6	2 6 4 7 6	-1.579	1 . 441	1003	76.457	137.559
1710-97	21/55.4	2"764 9	-1.716	1/3 626	104500 7	76.41	137.098
1715.246	21455-5	2117.3	-1.78	111.742	195155.5	26.391	130.947
1718.436	21279 A	10881 2	-1.827	1'1.911	192076.5	26.343	131.135
1722.595	21067.9	19712.7	-1.930	162.561	191404.5	26.317	131.261
1722.722	7 894.4	10538.7	-1.817	1 2.163	197 5 .5	24.291	131.384
1724 F 74	27.5.8	19357.7	-1.8.7	1 7 89	189611.7	25.266	131.507
1728 . 72	2.427.1	19279.8	-1.822	1 2.1 5	195120 5	26.229	131.658
1727 222	2123	18690 8	-1.780	1 2 135	183771 5	26.179	131.075
1734.474	19821-1	19477.6	-1.763	1-2-161	197475.7	26.155	132.042
1737.671	195.3.6	18155	-1.751	1 2.2.12	18 454 5	26.119	132.215
1739.795	19293.3	17974.7	-1.741	1 2.224	170177.5	26. 95	132.327
1741.922		177.9.5	-1.734	2.247	177210.4	26. 71	132.439
1744.073	11924.5	17475.9	-1.722	1 2.266	176660.2	26.49	132.550
1747	10773 7	1/1/// /	-1.70B	102.027	172722	25 001	132.813
1751.277	1 999.1	14640.0	-1.709	1-2.279	177620.1	25 071	132.911
1754.229	17654.4	167 7	-1.72	1 2.265	171 27.5	25,941	137.054
1759.272	17672.0	15722.	-1.777	1:2.106	1493 5.7	25.880	133.291
1761.166	16837.64	15497.2	-1.802	172-153	167286.0	25.871	133.378
1764.198	16473.9	15172.9	-1.012	102.045	165628.2	75.847	133.513
1768 073	15043 (14671.1	-2.14	111.861	16734 . 2	25.8.7	133.693
1771.029	15612-8	1475 9	-7.545	1 1.794	14127 .2	25.78	133.818
1776.77?	14047.	17617 5	-7.773	1-1.024	157448.	25.737	134.014
				·			
1777.965	14689.0	13770.4	-3.435	102+051	155813-0	25.7?1	134.089
1783.989	14 771 . 3		-7.652	1 2.77	153 73.1	25.696	134.275
1782.005	11077.5	1767 3	-3,735	1 2.396	151229.5	75.69	134.280
1787.309	13327.2	11087 6	-2.790	102 450	147776 7	25.445	134. 358
1790.472	12822.6	11475 7	-3.843	102.271	144 554.5	25.621	134.543
1792.595	12474.7	11124.6	-2.901	1 12.126	142739.2	25.6.4	134.614
1794.7??	12122.5	1 773.9	-7.039	1.1.088	14 039 5	25.501	134.682
1796.003	11757.4	1 474 7	-3.090	1.1.800	130125.5	25.576	124.749
1822.072	11244.3	0904 0	-4.17	1 1.766	136572.	25.556	134.843
1802.105	1.499.2	0530.5	-4.851	111.761	1340 7.2	25.543	134.003
1906-474	1' 35'•2 1' 191. A	9103.4	-4. 95	101.642	131441 7	25.53) 25.510	1 34.962
1809.516	2.EPA7	A.2.2 V	-4.29	1 1.477	124001+1	224215	1370118
1811.497	C 37 . 1	A-10 A	-4.331	1.1.377	127096	25.411	135-142
1814.51			-4.665	1 1 87	175074.2	25.477	135.21
1816.441	8613 . 9	7262.7	-4.945	10- 838	124778.5	25.468	135.252
1819.427	8172.7	6921.6	-5.591	100.488	122071.7	25.455	135.314
1821.301	1878.1	627.9	-6.1/3	11.2 • 3.26	12.1486.2	25.448	135.351
1826.715	7163.6	5818.8	-7.47	1. 7 3 3 1	118/82.7	25 420	115.440
1828.289	4876.3	5534.7	-7,927	1	114200.7	25.423	135.472
1831.311	6463.1	5125.2	-9.427	105.61.3	111334 7	25.413	135.519
1833.321	6191.1	4855.1	-A.687	10.607	1 194 17.7	25.416	135.548
1835.449	5910+1	4575.4	-8.947	1	107458.7	25.400	135.577
1838.627	5514.8	4181.3	-9.42	100.067	104555.0	25.391	135.617
1840.792	5253.8	2921.5	-9.974	00.575	1 2 5 9 8 . 5	25.386	135.642
10421000					1: 7.1.7	25.391	135.664



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Table B-2a.	Reconstructed Reentry Trajectory,
	Special Parameters (Continued)

TIME FROM	INCRATAL VEL.	RELATIVE VEL.	INFRIAL FLT.	INFOTIAL	ALTITUDE	GEODETIC LAT.	GENDETIC LONG.
RETROFILE	MAGNITUDE	MAGNITHOF	PATH ANGLE	HEADING ANGL	(FEET)	(DEGORES)	(DEGREES)
(SEC)	(FT/SEC)	(FT/SEC)	(DEGREES)	(DFGREFS)			
1845-048	4763.4	3436.4	-11.74	96.901	98729.6	25.377	135.686
1846.228	4432.2	3154.5	-12.10	99,213	OF 8 72.7	25.371	135.716
1851 - 115	4719.7	2911.3	-12.533	97.885	07670 5	25,367	115.733
1852-441	5517.2	2753.4	-13.575	97.467	91 937.0	25.364	135.750
1854.579	3826.8	7517.4	-13.657	97.039	#0097.2	25.361	135.765
1857.747	3569.9	7757.5	-14,499	96.374	97167.0	25.358	135.786
1859.875	3417.6	2112.2	-15.158	05.876	85752.5	25.356	135.799
1867-004	3254.0	1967.3	-15.415	95, 155	83374.5	25.354	135.810
1864-135	3115.1	1833.6	-16-142	04. R12	81516.7	25.35?	135.821
1867.772	2973.6	1654-1	-16-899	34 . 220	79823.2	25.35	135-835
1869.320	2808.1	1547.4	-17.387	93.495	77593.6	25.349	135.844
1874-517	2557.7	1323.2	-18.611	97.130	72796.	25.347	135-862
1876.562	2457.6	1744.6	-19.035	91.549	71137.5	25.347	135.268
1878.448	2395.8	1176.	-10,459	71,037	69443.7	29.747	135.874
1981.749	2274.7	1083.6	-21 (39	90.73	67176 1	25.347	135.881
1983.796	2212.1	1075.9	- 2" - 375	P9.511	55639.7	25. 747	135.896
1885.888	2147-5	976 .	-21. 64	89.303	53848.7	75.347	135-890
1885.989	2061-2	939.8	-25.659	A4.377	61551.5	25.347	135.895
1891.030	2020.7	874.8	-21.579	88.102	60085.0	75.347	135.899
1893.167	1937.9	84P. 9	-7: 554	P8.710	58581.7	25.349	135.902
1895.336	1961.4	871.5	-21,353	PR. 317	57 87.7	25.348	135.905
1898.474	1077.5	79. 7	-25,105	8P 455	54 C4 C .	75. 749	135.979
1900.521	1917.7	772.4	-10,978	RA. 790	53470.0	25.349	135.912
1905.748	1852.9	727.3	-19.598	P9.442	50292-2	25.349	135.918
1933.863	1673-3	455. B	-14.83/	90.794	15659.	75.357	135.941
1939.015	1612.2	470.1	-14-215	89.388	33597	25.352	135.044
1941.63	1596.6	419.3	-17,954	R9.175	377AC .7	25.350	135.945
1044.165	1535.8	470,4	-13-75%	80.204	316-1,5	25.351	135.947
1946.276	1553.2	431.2	-13.436	89.000	10841.5	25.351	135-948
1948.255	1579.4	3 74 . 8	-13.237	PA. ##]	30078.2	25.351	135.949
1951.364	1573.4	735.8	- 12. 08.	R8.775	*8987.5	25.351	135.950
1953.450	1567-6	38 6	+12.0.7	28.957	P24F.7	75.351	135.951
1955.499	1567.5	376.3	-12.91	PO. C15	:75=3.0	25.351	135.952
1958.614	1555.1	367.0	-12.640	89.219	76467.7	25.352	135.953
1960.650	1547.0	360.4	-12.568	89.566	25771.0	25.35?	135.954
1967.698	1544.7	354.1	-17.204	89.741	75" 95 r	25, 352	135.955
1965.803	1537.1	340.6	-17.731	91.100	241 58.2	25.35?	135.956
1967.651	1535.9	_ 342.9	12_(65.	89,905	23413.5	75,357	135.957
1969.941	1534.8	337.0	-11.825	89.925	22739.0	25.352	135.958
1973.003	1526.5	330.8	-11.747	89.939	21791.7	25.352	1 75. 959
1975-091	1519.7	322.8	-11.549	99.945	21139.7	25.352	135.959
1977.142	1511.2	327.5	-11.725	89.936	2 512.7	25.357	1.35. 960
1980.204	1504.5	311.2	-11.373	° ° ° 67	1958A.5	25.357	135.961
1982.325	1496.3	312.7	-11af13	CC. 840	18954.6	25.352	135.062
1984.38)	1491.0	3.74.2	-11.784	PQ.91*	18347.0	25.352	135.962
1989.567	1477.9	294.1	-11.15'	07,937	16837.5	25.352	135.963
1973.711	1.455.	284.5	-10.932	91.265	15669.0	25.357	135.964
1998.896	1454.2	. 277.00	2		14330	25.352	135.965
2001.955	1451."	275.5	-1(.700	07.771	13677.7	75.352) 15. 9 65
2024.285	1445.7	266.5	-1 51 9	80,004	12830,0	25.35?	135.966
2005.137	1433.1	267.3	-1483	47.10	12296.	25.352	135.966
2018.225	1423.5	197.3	-7.165	P* - 54	11*33.5	25.352	135.966
2011.287	1439.7	112.4	-4 /473	80.996	11393,5	25, 352	135.966
2-13.772	14' R. (P4 .]	-7.794	or, 'n7	11392.2	25.352	135.966
2515.424	14 7.3	AQ. 5	-7.517	0.154	1.008	25.352	135.966
2019+522	14 4.	47.2	-1.483	o. vo	S 1.	25.352	135.967



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TIME FROM RETROFIRE (SEC)	INTPITAL VEL. MAGNITUDE (FT/SEC)	PFLATIVE VEL. MAGHLTUDE (FT/SFC)	INTETIAL FLT. PATH MOLI (DEGREES)	THEOTTAL HEADING ANG'S (DEGREES)	(FEET)	COULTIC FULL. {DECUEUS}	GEODETIC LONG. (DEGREES)
2020.571	1399.*	27.8	800	80.754	1.778.7	25. 352	135.967
2. 77.675	1395.1	28.7	776	CO. 795	1.7.4	26, 362	135,967
25.25 . 777	1397.9	24.5	- 526	PC 6. 7	1 65 -	25, 357	135.967
2077.771	14 3 1	3 /	- 914	0. 101	1 1415.5	75, 352	135.967
2020.843	14 4 7	37 6	- 013	91.476	1.571	25 352	135 067
2032.022	14 CA P	33.3	- 828	25.436	1 515.7	25.352	125.968
20 35	1404 5	37 6	- 0 4	0 . 97	10461.5	25.352	135.948
2027 342	14 7 8	A 26	- 971	00.079	1 415.7	25.352	135 948
2046 145	141 4	37.5	~. 897	PQ.778	1. 346. 7	25.352	135.968
2.47 613	14) 8	33.4	-1-14	9-411	1 174.2	25.352	135.040
2 49 45	1477 6	21.7	854	0. 327	10131.5	25.352	135.560
27.51 600	1207 0	20.2	- 097	91 113	11 195 2	35 361	135 040
3/ 54 4 14	1305 5	7.3 5	-1-044	01.047	10008.2	26 361	135 040
20 84 453	1307.4	75 7	- 977	91,287	004 5	25 361	135 040
2058 741	1305 5	20.4	-1	2 70	C012./	25 351	125.069
2041 9 3	14	11 2	- 093	89.717	0839.2	76 351	135 060
2042 851		29.6	- 866	69.897	9701 7	75 261	135 070
21.45 041	14 7.7	37./	- 954	01.194	9745 2	75 251	128.075
2000 123	1411 5	39	- 679	80.081	9472 7	25 351	135 070
2071 (41	1413.9	39.4	- 877	20.93	3424.7	25 35	126 070
20 73 147	14 4.1	31	P4 7	G* . 2= 3	0591.7	26 381	135 070
2076.204	1295.4	77.		C' 384	9517.7	75,751	125.070
20 78 292	1396.1	25.2	- 870	91.10	9475.0	25, 351	135.071
2090 390	1413.5	41.1	- 944	80.721	9470 2	25.261	135 071
2082 421	1414.8	39.2	- 725	49.734	9386.7	25.351	125 071
2085.567	1125.0	77.5	- 0.7	09.979	9322.7	25, 351	135 071
2087 417	1207.7	27 2	- 843	90.047	9777 7	25 251	135.071
2089.711	1475.A	9,65	015	or an	0232	25.351	135.971
2002 012	120/ 2						
2092.012	1394.2	2	472		15.	-5.341	135.972
2006 055	1100 5	· · · · ·	054		0114.2	75.751	135.972
2100.011	129747			00 000		/	135.972
2100.011	1417.5	41.0		9		22-321	135.972
2102.090	12-5.6	<u> </u>			964.0	(2•22)	135.972
2114.174	1379.3	27.57	-1. 18	90.470	1915.5	25.351	135.972
2100 204	1400 7	20 4	- 863	01 035	107	22+222	115.972
2111 364	1200 4					75.75	137.972
21110 204	130744	75 1	- 707		84.30	22. 221	145.072
2114.407	120	27.11	- 026	9 AD / L	9456 9	27.171	135.972
2110.444	1374 8	· · · ·	-1 (10	9 741	0002+1 0535 5	204 171	135.972
2122 47	1349 4	25 0	- 451	00 401	827040	27.321	135.973
2129 973	1305 7	33.7	- 779	07 144	9400 3	274.72	132.972
2120.013	1374 6	75 4	- 077	00 40 9	0766 7	25.351	135.072
2136 62	1724 7	21	- 020	05 570	9744 7	75 75	137.973
2138.112	1391.4	27.4	- 797	90.472	9190.7	26.350	135 073
2140.199	1375.4	32.7		00 010	8154 7	25.151	177.7/5
2143.297	1393.9	20.0	- 729	00.056	8505.7	25,351	126 073
2145.701	1799.	21.0	- 964	07 414	0 5/ E	274 27 7	137.973
2147.439	14:3.2	78.9		01.345	8713	72427	177+973
2151.541	1389.3	22.5		01.585	7045	27.349	1274913
21 52 581	1380 4	26 5	- 621	97 824	7037 5	36 340	132.973
2154.472	1301 4	29.2	- 660	00 821	700/ 7	75 240	1224 713
	127180	10 • C		· • • • • • •	1 7 Y 1 1	£ 24 349	1334913





TIME FROM RETROFIRE (SEC)	FELATIVE FLT. Path Angls (degpets)	PELATIVE HEADING ANGLE (DEGEEES)	INERTIAL LONG. (DEGREES)	GEOGENTRIC LAT. (DEGPEES)	RADINS TO CARTH CENTER (FFFT)
2.325		59.766	10.007	812	21882839.2
4. 367	1 44	50 351	7.125	- 730	71882769.7
0.016	-,134	50. 754	2.43	- 549	21887577.7
12.422	165	50.765	2 541	489	21892369.
14.326	103	50,270	2.403	42#	21992?30. 2
16.976	229	50.797	2".84"	-, 347	21852008.2
15.396	- 754	TO 354	7 945	- 187	71HR1755-7
74.477	-, 207	50.74H	21.275	-117	7188117
26.37	- 3"	50.740	71.3#7	- 745	2198-929.7
28. 976	304	F9.749	21.531	.024	7148^614. 7
31.394	-• 3° 8	59,740	21.676	- +114	2169/297. 7
37,047	- 712	50 75P	21.477	- 195	71879971. "
78.37	-, 210	F.9.75	27. 77	.736	21079397.7
47.876	373	F9.2F7	27.221	.415	21 879159. 2
43.396	327	50,257	22.366	.495	21878726.0
45.942	231	59.755	274513		21478373.7
57.011	- 347	59.765	22.014	. 797	218774-1.7
55.432	- 746	50.767	77, 50		71877142.7
57.947	251	50. 155	23.274	. 557	21976687. ^
60.422	355	59.247	23.346	1.036	2187431R. "
62.795	m.358	50.77	23.483	1.111	21875948. 7
67.674	- 344	50,574	22.761	1.764	21475244. 2
74	37	50, 181	23,800	1.241	21874878.7
72+423	374	50,294	24.03R	1.417	21874549. 7
74.823	278	53,794	74.176	1,403	71874136.7
76.477	- 78	E 0 204	74, 154	1.54	71873#8%.7
81.996	-, 380	50.3	24.589	1.7?	21877998. 2
84.423	? 9 ?	50,215	24.729	1.707	21877675.5
56.795	756	59,21	24.866	1.473	21877717.7
89.274	4**	60,115	25.1%	1,05	21 A 71 91 7. 7
71.524	- 409	ED 325	25 782	2.1.2	71971014
96.396	412	= 9, 31	25.419	2.177	71475611.2
98.795	415	FO. 338	25,557	2.252	21970200.2
101.195	42	59.343	25.696	2.329	21 869785. 5
103,535	427	50 554	25, 934	7.4.5	21859365.5
108.367	- 431	E9.342	26.11	2.556	217559444
114.423	- 474	59,369	24.751	7.434	21868783.5
113.195	428	50.776	26.3AR	2.709	21 857655. ^
115,545	- 15	50,384	26.527	7.785	2196721 P. 0
117.994	- 45-	50 708	74 8 4	7 027	21 466 777.
122.795	- 453	F9 4 5	75.747	2.13	21955583.1
174.422	- 456	59.411	27.137	3. * 4	21865575.7
127.424	461	=0,473	27.272	3.166	21864959.5
130.727	464	F0,431	27.36	7.242	218545/39.7
134.705	- 471	50 449	27.536	7. 102	21959 47. 7
137.19*	- 676	50,4FR	77.77	3.46 P	·1843.13. >
139.595	479	59.467	27.914	3.544	21 962639. ^
147. 73	-,497	50.477	70,744	3.623	23867155, 1
146.873	- 49	7 44 6 70 5 0, 404	7. 177	2.777	21851187.7
149.224	- 404	K0 5/ 6	2R 471	3.84P	7186 698.7
151.424	4	50.516	28.51	3.074	21867275.0
153.996	501	59.57	28.74R	3.090	23859714.0
156.419	5.5	50 5/ A	79.44	4 ° 7 K	23359211.0
161.224	517	50,559	77-166	4.777	21958195.7
167.524	516	50 \$71	29.3.5	4.3 3	21857684. 3
166.023	520	E0.587	29.445	4.77R	718571 AR. 7
16*.423	74	50,503	29.554	4.454	21456649.7
177.433	577	50.41A	29.721	4 . T. P.	71856132.5
175.474		50,43	3 . 17 9	4.74	71855771 0
178.023	- 539	57.647	1 .14.	4.746	21854537.7
180.423	- *47	50.455	3 . 28	4. 531	71854- 34.0
182.923	546	59.667	3 . 47	4,.907	21853450.0
195.224	55'	50,4P1 60,404	1:550	2, 207	71852914.5
196.123		77460114 50,718	3. 936	T.122	71851614 F
192.423	- 55	59.771	1.074	K 71 R	71951250.4
194. 623	554	50.735	31.117	K. 2#4	-1453743.5
197.224	568	59.749	31.257	5,250	11855137.5
199.624	571	59.747	21.377	5,434	71840471.7
204.400	70	59,703	31,476	6.534	7194843(_3
	• . •	- • ·		· • · · • ·	





TIME FROM	PELATIVE ELT.	DULATIVE HEADING	INFRIAL LONG.	GEGORNIRIC LAT.	PANINS TO
(SEC)	ATH ANGLE (DEGREES)	AtigLC (DEGETES)	(DEGREES)	. (DEGREES)	EARTH CENTER (FEET)
2:6.323	592	E Q . Q . Q	31.R14	5.66	21947849.5
219.274	5°5	20°653	31.754	5.735	21847268.5
211.674	590	59,878	37,04	5.817	21 846684.2
214.222		50,940	37.376	5.961	21845504.5
218.798		F. 0 0 0 4	32,515	6.035	21844915.5
22 . 438	601	57,896	32.61	6.CA6	21844506.7
227.598	/	50.017	37.705	£.185	21843714.2
225.000	()	59.034	32.035	6.254	218431-8.5
225.372	61	50 547	33,216	6.544 6.640	21842494.2
233.198	621	59,984	33, 356	6.484	21841269.7
235.590	62	s	33.406	6.559	21940649.5
217.390	67	5.11	32.637	6.634	21840025.7
24 . 208	6.72	5 • 37	12 010	6.718	21839398.7
242.138	- 639	6 73	34. 58	C • / 7 + 6 - 858	21838133.7
247.599	- 643	61.01	74.199	6.932	21937495.5
240.000	646	6.1.7	24.34	7.77	21836854.5
252.394	450	4 . 1 2 R	34.40	7. 91	71836213.5
254.799	557	5-147	34.471	7.156	21435561.2
257.194	077	5 +100 63,195	34.977	7.305	21834969.7
261,000	664	£ .7`5	25,144	7,379	21833594.7
264.399	647	1. 775	35.185	7.454	71832937.5
244.796	671	4 . 74 -	35.376	7.528	21832266.5
24 R. 639	672	4	35.473	7.570	21831809.5
271.535	478	4°.795	35,478	7.67	21831924.5
271,930	631	61.216	36.75	7.751	21837248, 5
276. 379	~. * 94	4 .777	JE .901	7.R25	21829569.7
27 P. 70 F	- • F 9 F	6	36 . 32	7.800	21928885.5
281.128	<u>491</u>	6 . 369	34.174	7.077	21928199.2
28:+799	608	6°.41°	36.457	8-121	21826815.5
298.398	- 7 2	47.434	36.500	P.195	21826118.7
207.730	7 5	4 .LEE	26.74	8.769	21825418.
207.100	7 9	A".479	24.842	P.343	21824714.7
295.590	712	6 • F .	37. 74	8-416	21924006.7
301.364	/15	0 •1/5 4 .F45	37.307	R.563	21822585.7
3 7.798	- 723	50	37.45	8.637	21821863.7
3.5.130	724	4	37,507	P.711	21871142.7
3 7.500	700	5-+615	27.714	8.785	21820418.2
3	732	4	37,376	8.855	21819690.5
312.309	7**	5.467	38,18	8.932	71H19959.0
316.63P	7×1	6 7 7	38,758	0,755	1917770 7
310 500	744		19.445	9.352	71816745.2
321.000	75:	6	33,589	0.275	181600.5
324.000	75?	6 .78ª	10.11	9.208	1815252.2
376.779	756	A	38.972	9.371	21814591.0
331 630	- 760	A	39.310	0 517	21912088 0
337,007	75/	A	10.3	C FC	21812226.5
376 739	749	6.614	20.444	9.643	21811461.7
33F. 70P	77?	4°.078	10,507	9.736	2] 81 1693 . 5
141 IAF	77/	4 - 04F	39-731	0_8,°0	218)9921.7
343,570	70	6 6 1	10 974	9,892	718 9146.5
345.000	97	41. 10	4 . 17	0.055	718'8368.5
248. 394	785	~]• ~ 44	4.120	10.027	21 97591.7
350.798	700	61 • 7 7?	4:.3^4	16.176	21 905802.7
353.109	7^?	£1.000	4- 447	10.745	218-5014.7
357.000	.739	*J.154	4 . 734	1/ .317	21814429.5
241, 290		41,192	A	1 . 19	219 347-1.7
362.792		41.211	41.72	1 . 462	218 2830. 5
364.439	8(P	61.230	41.12	1.511	213 228 . 2
367.599	<u></u>	41.247	41.31	15.676	21811216.7
392,330	815	61.796 41.005	41.454	11.679	21799591.7
374,799	871	61-354	41 747	1	21798774 5
177.178	- 625	41.784	41.494	1.895	11707953 7
379.590	87 R	41.413	42.30	11.957	?1797129.5
381.97	831	61.442	42.173	11.537	21796312.0
384.308	A74	51.473	42.310	11-110	21795472.2
3R6.79P	A37	51,573	42.454	11.192	21794638.7
389,198	244	61.564	4/.K~B 42 753	11.325	21792961,2
391.291	- 847	61.595	47.804	11.397	21797118.0
396.384	850	61.625	43."42	11.465	21791277.0
399.771	P53	61.657	47.196	11.529	21797432.2
401.17	857	61.689	42.331	11.610	21789579.2
403.509	850	61.775	43.478	11.687	21759713.2
415,597	- ** ·	01.104	41.071		2110102400





TIME FROM RETROFIES (SEC)	PELATIVE FLT. PATH ANGLE (DEGEFES)	VDEDEELS) VNCF2 VEF2ALAL HEPDING	INTETIAL LONG. (DEGREES)	GENCENTRIC LAT.	PADTHS TO SAPTH CENTER
40 8. 398	856	61.784	43.759	11.F24.	21736991.7
416.798	P50	61.817	43.914	11.805	71786124.2
412.365	F7]	41,010	44.10	11.047	71785559.2
417.970		61-015	44.7 7	12 1/7	21783571 2
42(.371	981	6119	44.495	12.178	21782643
422.771	R84	61.001	44.641	12.249	21781761.7
425.17	FA7	57. 14	44.787	12.319	2178-877.7
427.509	PO1	47.49	44.974	12.301	21779980.0
429.942	-, 201	42 NA	45 334	12.459	21779170.2
434.746		67.15	45,37	12+22	21777319.5
437.146	-,•)?	42,145	44,516	12.670	21776477.0
436.545	***	52.770	45.643	12.741	71775417.2
441.545	0.9	67.754	6. 8.9	12.811	21774611.5
444.21E	C17	57. 789 47 33E	45,254	17, 99,	21772770 7
449.174	=_•~1∵ =_918	62-361	46.751	13.771	21771864.7
451.546	921	62.397	44.397	17.50	21770957.2
453.546	<u>9</u> 23	67.435	44.544	13.14	21771 36. 5
456.746	576	57.440	46.691	13.23-	?*759117.7
458.747	- 020	57.5	44 030		21768156."
467.574	936	52.5B	47.135	12.439	21766312.9
465.975	- 030	£2.616	47 297	12.5°A	21765276.
468. 775	041	67.654	47.43	17.578	71754477.1
471 . 774	045	67.491	47.57F	12.647	21743495.
473.144	* 4 7	70° 448	47.724	12,12	2176256 • 7
475.546	953	52.765	47.872	12.764	21761612.7
485.375	- 556	57, p: 5	40.171	12.954	2176 65 . 7
482.774	- 050	52.202	48.310	17.973	21758740 3
485,174	- 942	A2.921	48.456	14.161	71757780.5
487.574	96*	42.060	48.615	14.129	21756818.0
489.946	967	62.090	49.763	14.196	21755863.7
492.36	97]	42, 38	49.911	14.2f 5	21754899.5
407.174	- 574	63 110	40, 161	14, 134	71753012.7
499.574	- 970	63,158	49.358	14.470	21751967. 2
501.975	987	63.19*	49.518	14.538	21750982.5
554.375	995	63.339	49.657	14.676	21749099.7
5.6.774	987	63.78	40.8.4	14.674	23749014. 2
515 574	- 003	53.7 A	40,0-2	14.710	21748356.2
513.975	- 904	43.473	5-254	14 877	71744730.7
514.375		67.444	R 4/ 4	14,945	21745042.5
53 8, 774	-1-002	63,496	5 554	15.012	21744-47.5
521.174	+1.174	43.477		15,287	21743 .39.5
523.574	-1.67	43.66	K . 9K4	35.347	71743574.3
528.375	-1-512	63.455	51-154	15.281	71740015.0
531.774	-1-015	£7.607	R1 7-5	15.348	71730001.0
537.174	-1.(18	62.74]	51.455	1= 415	21737954. 1
575.574	-3.+ C3	43.7P%	51.5"6	15.492	71736964.2
537.975	-1.(??	63.877	51.754	35.548	21735047.
24 3 • 36.7	-1.726	64. F /	21.3.4	15+614	71734923. 1
542.774	-1.029	63. 015	52. 58	15.681	21733889.2
545.174	-1.071	A3.059	5°, °, °, °, °, °, °, °, °, °, °, °, °, °	15,740	7173285A 7
541.514	-1,014	56. LT	22 • 10 F 7 . F 7 7	17.814	21731926.7
552.375	-1.039	64.107	52-663	15.946	71779751.5
554.774	-1.647	44.127	57.A1F	14.12	21728712.0
556.415	-1-044	64.147	52.91B	16.157	71727096. 5
55 . 574	-1. 48	64.227	57-118	14.144	7177641 P. "
561.975	-1.1.5	44.77 <u>3</u>	53.77	16.71	71775569 1
204+312. 566,774	-1.CTZ	09.314 64.765	53.574	16 241	71773447.7
565.174	-1.057	64.41	53 774	16-476	21722405_0
571.574	-1.061	44.457	57.970	16.471	21721 345. 0
573.975	-1.(63	44 . 513	54. 31	16.536	21721282.1
576.375	-1. tt	54.55	54.197	16.677	1719216.5
578.774	-1.648	54,507	54,326	14.657	71719144.7
2814174 583,574	-1+1/1	F4. 544	544434 54.441	10.704	21716704 F
585.975	-1-76	f4. 74	54.734	16_R61	21714079 5
588.366	-1.(70	+4.787	4.947	16.975	71713854.5
596.774	-1.781	44. P26	55.101	16.900	71712768.7
593.174	-1.083	54. 994	55.254	17. 14	21711685.0
595.574	-1.085	44,C77	55.478	17.11P	21711598.7
591.975	-1.001	54.981 (5.02)	50.561 55 715	17.182	217 951 2
602.774	-1-/04	65.70	55.840	17,31/	217 7374 7
604.415	-1.005	65,113	55.074	17 354	217 6575 5
607.574	-1.158	65.17B	56.177	17.43P	7. 5120. 7





TIME FROM RETROFIRE (SEC)	PILATIVE FLT. PATH ANGLE. (DEGREES)	PELATIVE HEADING ANGLS (DEGREES)	(MODE TOS)	GEOGENERIC LAT. (DEGREES)	RADIUS TO GARTH CONTER (FOOT)
6:0.97F	-1-101	65.228	56,301	.17.51	217:41 27. 5
612.775	-1.1.7	45.273	55.494	17,545	217 2923.5
614.774	-1.145	45.779	·· · · · · · ·	17.629	217 1816.7
617.174	-1.119	65.779	55.795	17.691	217107CR.0
619.574	-1.110	65+4:5	57.104	17.817	210992000
621.975	-1.114	5.531	57.259	17.88	21697366.0
624. 774	-1.117	65.527	57.414	17.043	214 95747.
629.174	-1.120	65.676	57,569	18,375	21695125.5
611.574	-1.122	65.68	\$7.725	18.768	21694002.0
673.975	-1.125	45,727	57.98	18.13	21692875.7
636.360	-1.177	65.790	-H. 35 Te 102	18.197	21691754.9
678.774	-1,128	65.937	58,346	18.316	21680494.5
64] . 149 443 546	-1.124	45.046	-B. F. 7	18,378	21698359
A45. 949	-1.136	55.090	10,45P	18,44"	21697221.
648.35/	-1.139	66. 757	5.814	18.501	21686195.2
657.75	-1.141	66.1.6	18.971	18.563	21694937.
652.423	-1.143	A6.143	13.363	19,65.4	21684138.7
455.521	-1.146	00 • / 1 / 46 2 66	10 430	18.746	21681506.7
6774 927	-1,147	44.771	50 597	15.6.8	71681341.7
662.750	-1,157	56.275	50.754	18.869	216701 95. 2
645.140	-1.155	56.43	59.912	18.63.	21678 29. 0
667.54°	-1.157	56.495	5. 140	18.99	21 47 68 49. 7
669.921	-1.159	66.539	£°	10.111	21675721.2
677.321	-1.1/1	60+001 44 450	6 54	10 171	21673391.0
674.1.21	.=1.103	00+1.5	0 • <u>2</u> +	_ * 7 • 1 * 7	(1979-1 9 -197
677.122	-1.166	66.705	63.597	19,231	21672222.2
579.521	-1.169	66.752	6 . 355	17.201	21671 51.2
6R1.921	-1.173	56. PT R	A1.17	19.351	21649478.7
684.332	-1.174	00+0/9 44 031	01+1(2 61-337	19.471	21667511.5
689,122	-1.177	66.997	61.483	19.53	21666345.5
691.521	-1.170	67. 44	61.647	10.580	21665163.5
602.021	-1.191	67.111	01+874	19.648	21663979.2
696.321	-1,197	67.150	51.955	10,7**	21 66 77 92, E
698.721	-1.185	67.216	62.124	19,767	21661603.7
702 540	-1.190	67.333	A2.444	17.00	21659204.2
765.949	-1.192	67.101	67.573	17.043	21658010.5
71 8.35	-1.194	67.449	42.763	20.7 2	71656812.7
71(.721	-1.104	67.5.7	67.021	21 . 50	21655677.7
712.122	-1.107	47.566	41. 01	23.110	21654425.7
715.521	-1.202	67.625	63.741	25 +176	21653721.2
72.0 350		67.745	A3-563	20 - 292	21651793.0
722.75	-1.2' 6	67.5 4	63.723	21 25	21640587.5
775.140	-1.2.8	67.864	63.094	24. 41 7	2164837".2
727.549	-1+21^	67.074	64. 44	76.454	21 54 71 55. 7
729.921	-1.217	57.094	64.21?	20.521	71645953.7
732.335	-1-213	68,744	64.365	25.578	21644728.Z
737 140	-1.21*	69 166	64.689	2 . 602	21642278.5
730 540	-1.210	59.728	54.95	27.740	21641 54. 2
741.940	-1.722	49,795	45. 11	2.6.2	21639827.5
744.35	-1.224	69.25)	65.173	21 + 862	21438598.5
744.75	-1.225	68.413	65. 274	2' 018	21637367.7
748.340	-1.227	59,454	£= 447	2 . 95	21634546.7
751.549	-1.229	68.537	A5.659	7].(7)	2163497 % 5
756 353	-1.237	48 447	65 083	21 141	21437475.7
758.756	-1.235	68.774	A6-145	21,196	21631184.7
761.149	-1.237	69.797	44.3.9	21.252	21629942. 2
763.540	-1.238	68.053	46.471	21.377	21628697•7
765.949	-1.240	68.524	54.634	21.352	21627451.5
768.351	-1.242	48.979	65.797	21-417	21626203.
773.140	-1.744	AU 17 4	6f + 76/ 47 - 123	21.47 <u>)</u> 21.574	2162495344
775.549	-1.240	50 + 10 C	67,29/	51+7/5 71_58f	71477447 7
777.040	-1, 740	69.235	67.45	71.434	21671191.5
78(.375	-1.2*1	40,007	47.417	21.69B	21 6 1 9 9 4 1 . 7
78~.750	-1.253	60.754	47.778	21.742	21618674.5
785.149	-1.7*4	49.479	67.942	73.796	71617413.7
10 (+ 34 1/ 789,040	-1.259		68+1°5 68-970	21+75	2161017"#2
702. 15/	-1.267	49.575	68.425	21_054	21613618.5
794.75	-1.242	A.0. A.01	58.599	77.1	21612349.7
794. 395	-1.263	17.776	49.712	77. 44	21611481.7
799.549	-1.244	C, 973	58.779	27+115	216 9817.0
8(1.949	-1.256	A 9. 40 \	69. 194	22.16	21638533.2
0114.151 BCA.750	-1.270	ere 45 f	A 7.759	22+ZZ'	216-5081-0
8 0,149	-1.272	7	69.59	22.325	216" 47" . 5





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TIME FROM RETROFIRE	FLATIVE FLT.	PTEATIVE HEADING	INTETIAL LONG.	GEOCENTRIC LAT.	PADTUS TO
(SEC)	PATH ANGLE (DEGREES)	(PEGPETS)	(DEGREES)	(0567775)	(FEET)
811.549	-1.273	7 .159	60.755	22.277	21613419.5
812.949	-1.775	7.075	166.27	22.429	216 2136.7
816.35	-1.774	7 .703	7 07	77.49	21500564 3
821.149	-1.29	75.429	7.419	274527	21598277 7
927.540	-1.781	7 . 497	7 . 595	72.635	21596988.2
825.949	-1.28?	70.566	71,752	22.680	21595697.0
826.335	-1.784	7	LIS	22.736	21594411.7
R37.75		77.2	71.45	22.787	21593110.0
935.149 935 540	-1.200	7 043	71.410	22.889	21590514.5
837.945	-1.230	77.011	71.596	72.938	21589217.5
840.350	-1.292	71 001	71.753	22.988	21587916.5
847.75	-1.293	71,051	71.021	23+F3P	21586613, 7
844, 37	-1.294	71.00	77. 35	23.077	21585722.7
847.545	-1.296	71.10	77.256	23.147	21587604 7
857.374	-1.795	114/01	77.50%	21,235	21581401.7
954.725	-1-201	71.44.3	77.758	23.294	21580090.7
857.125	-1.372	71.474	72.027	23.233	21578778.7
85°.524	-1.704	71.545	73. 05	23.391	21577464.7
861.924	-1.7.5	71,617	73.264		
864.374	-1.326	71.684	73.432	27.478	215/4435.2
840.125	-1.300	71.833	73.77	23.476	21572195.7
R71.574	-1.310	71.0*5	77.94	27. 627	7157 1874.7
873.924	-1.317	71.077	74.1.5	23.67	21 569552.5
876.311	-1.313	77.40	74.277	23.717	21568236. 7
578.696	-1.314	77.177	76.446	23.764	71566918.7
881, 124	-1.814	70,105	74.414	73.Pll	21565592.0
887.574	-1.217	-2, 2A2	74.788	23.85P	?) 564748. 2
885.924	-1.719	72.243	74.958	23.91*	21562918.7
968.324	-1.37	77.416	75.128	27.951	21501585.0
807.308	-1.321	72.547	75-417	24.030	21569325.2
895.497	-1.724	77.437	75.527	74. 89	21557611.5
897. 976	-1.375	212	75.9 8	24.135	21554764.7
901.296	-1.326	77,786	75.079	24,10	21554976.5
907.696	-1.727	77.951	76.150	24.226	21553587.2
97.54 196	-1.328	72.416	74. 121	24.271	21072297+2
9 1.976	-1.371	73.787	76-555	74.761	21549546. 2
912.294	-1-372	73.142	76.935	24.4FR	21548217.2
914.676	-1.372	73,739	77. 77	74.451	21546871.7
917.196	-1.275	77.913	77.179	74.494	71545524.2
910,407	-1.336	71, 180	77.351	24.538	21544175+7
921.827	-1 775	73 543	77 696	74.50/	1541474.7
974.776	.1.770	7- / -	77.97	24.67	2154116.5
125.125	1.247		70 .43	74 .71 3	21538763 5
031.575	-1.243	7*.774	78.215	24.756	21537399.0
032,807	-1.342	73.PEC	79.386	74.790	21536759-0
936.297	-1.347	73.077	74.559	24.F41	21534702+2
9484097	-1.745	74 59	78.95	24-917	71532623. 0
043.575	.1.747	74. 147	70	74.959	21530609.0
		•	·		
945.925	-1.348	74.247	79,255	25.011	?1579?47.5
94 5. 375	-1.740	74. 718	79.470	25.152	21577884.7
PF 726	-1.250		70.4.3	75.794	21576571.0
955.498	-1.171	74,552	70, 743	25.176	21 7 1 70. "
957 975	-1.353	74-633	8-175	25.217	21522423.2
961 325	-1,754	74.712	R1,700	25.25P	21571755.0
967.72+	-1, 355	74.772	A	25.299	21519685.2
955.125	-1.355	74. 871	R .40	75.230	21518315.2
967.325	-1.256	74.051	R	21.370	21516944.2
977.717	-1.758	75 11	81,173	100414 75.450	21514204.8
974 776	-1_750	75,101	81, 140	75.490	71517824
977,175	-1.76/	75. 77	91.574	25.538	71511448.7
979.525	-1.363	75.357	91.7/1	25.577	21510072.2
981.225	-1.342	75.433	R1.976	25.616	215:18695.0
984.325	-1+253	75,514	82.151	25.655	21507316.7
994.774 086 345	-1.364	75.455	MZ+72*	22.693	21574993.7
977+177 991,575	-1.500	75,758	074790 87,58'	5.24717	213 47736 6
993, 775	-1.366	75.040	97.755	25.817	215-1793.0
956.325	-1.367	76.071	82.933	2*.845	2151449.7
998.724	-1.°6P	76.003	83.109	25.893	21499025.5
1001-125	-1.368	76.085	83. 786	25.920	21497640.7
10-3-525	-1.269	76-167	87.467		21495255-0
101 0.025	-1.375	74. 75	23.617	220974 76.030	27474868.7 71493481.4
1011.724	-1-372	76 416	83,994	26-647	21492593.0
		···•••••••••••••••••••••••••••••••••••			and the second





TIME FROM RETROFIRE	PELATIVE FLT. PATH ANGLE	ECLATIVE HEADING ANGLE	(DECASURE)	0500557910 LAT. (DEGREES)	PANIUS IN Farth Center
(SEC)	(DECREES)	(DTGP255)			(FEFT)
1 - 1 2 1 2 5	-1.372	76.200	84.177	25.1 13	21490703.5
1715.515	-1.273	74.597	94.340	76.130	21489313.7
17.925	-1.27?	76.445	94.527	21.175	21487923.5
102.312	-1.274	75.740	R4, 714	26-21	21496541.0
1 727.776	-1. 275	75.077	94,993	26.246	71485139.5
1 72 5 . 12 5	-1.376	74.012	85.730	26 316	21442352.7
1027+525	-1.277	77. 94	85 417	24.35	2148 1954.
1-72.375	-1.277	77 140	85.596	24.345	71479563.
1 24 72/	-1.278	77.757	95.774	24.419	71478155, 7
1134.365	-1.379	77.11	85.897	26.442	21477212.5
1 79.525	-1.379	77.472	96 311	10.487 24 E21	214/21/4.2
1-41.925	-1.297	77.502	86. 10	20+921	21472576
1 44.776	-1,781	77.677	R6 650	26.587	21471174.2
1-49.125	-1.292	7-,743	95.940	26.177	2146 2776 **
1151.525	-1.382	77.849	97.378	26.653	21468375.0
1753.925	-1.383	77.034	4/.2.1H	76.685	21465373.2
1056.225	-1.793	70 1 6	87.569	26-75	21464168.7
1061 125	-1.254	70,103	97.740	76 782	21452765.5
1-63.526	-1.795	78.079	97.03	26.913	21461361.7
1065.91	-1.385	78.344	88.114	26.844	21459977.P
1068.297	-1.395	79.449	94.285	26 . 875	21458575.0
107(.7	-1.386	78.617	95.467	26.037	21457151+2
1.375 53/	-1.380	73, 711	49,970	26.968	21454348.3
1.77.21	-1.289	78.708	80.00	24.008	21457940.7
1000 100	1 209	70 395	BC 10.	27 028	21451532.7
1 82.71	-1.288	79,073	90.371	27. 50	21451124.7
1 . 84. 34	-1, 299	70. 37	85.405	27. 78	21449167. 2
1 187.500	-1.389	76.148	89.734	27.317	214473 7.
1.389.907	-1.389	79.234	80.015	27.146	21445897.5
104 700	-1.700	79.412	9.97	27.253	21444457.0
1597.11	-1.301	70.51	0.46	77, 237	21441665.2
1 00.5	-1,30	70 + 30	9.447	27.265	2144 253.7
1101.873	-1.201	70.671	0.977	77, 777	71478958.5
11 4.272	-1.391	79.745	01.100	27.315	21437446.5
11.6.74	-1.202	70 764	91.371	27 - 27	714346 4.7
1111.5	-1.392	8	91.554	27.207	2143319'.7
1112.7	-1.302	R1.372	91.776	27.474	21431777.0
1116.297	-1.202	6 . 711	01,016	27.451	2:43-371."
1118.572	-1.393	e • 3: ·	97.10	27.677	21423955
1123 472	-1.303	9. 479	92.466	77.57	21426135.5
1125.873	-1, 203	0.) FAN	97.644	77.554	2147477 . 7
1128.377	-1.203	R'.64	97.934	27.581	21423288.5
1130.711	-]-343	R .75	07.17	27.5.5	21421872.7
1132.299	-1.393	4. PI1	23,14	67.6532 27.455	21421924.2
1127 030	-1.304	51. 772	97.568	27.679	21417624
114	-1.394	21,112	07.757	7 7 7	21 41 62 7. 5
1142.7	-1.394	A1.013	93. 236	°7.727	2141470 . 2
1145.1 "	-1.394	31.503,	94,17	27.751	21413372.5
1147.500	-1.325	91, 395	94.394	77,774	21411954.7
1140.0.	-1.305	21.474	44.490	27.797	2141:537.0
1150.310	-1.324	81.567	94.573	27.820	214 9119.
11:4.700	-1.305	e1.650	14.8F7	27.843	2141770107
1159.57	-1, 205	31.547	95,227	27.888	21414864.2
1161.924	-1.294	41 333	95.411	27.91	21473446. 1
1164.267	-1.794	87.75	05.505	27.932	21472736. 7
1166.7	-1.295	92.117	c.781	27.953	214-16-0,5
1169.1.1	-1.704		35,344	27.974	21207771 7
1173.0	-1.795	97 767	97.171	27+995 28_016	21396157.7
1176.25	-1. 764	37_485	04 572	28.037	21 304937. 7
1178.7	-1.304		96.7 7	79.157	21303515. ?
118 . 14	-1.204	42.641	96.934	20.171	21 392545.7
1182.5	-1.204	77.742	07, 78	79, 97	21395677.5
1188.3**	-1.294	-,,,,,,, A040	97.45	28.136	21387844.0
1150.77	-1.393	P . 47	07.435	28.155	21396421. 5
1192.1	-1.207	82,J2E	7, 97,	28.174	21385732.7
1195.5	-1.703	97,278	99. 1	78,107	71383584.7
1255-35	-1-203	07_414	98.104	28.228	21 39 107.7
12: 2.7	-1.203	g , r , p	99.565	2P.246	21379378.5
12/ 5.111	-1.393	82.4 2	98,753	2R. 264	2137791). *
12 7.51	-1.707	83, ACS	99.930	29.281	21376492
12 9.9	-1.297	44.78" R3_997	90,126	28.298	21 373664- 7
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Table B-2b.Reconstructed Reentry Trajectory,
Special Parameters (Continued)

TINE FROM	PELATIVE FLT.	FREATEV" HEADING	THEFTTAL LONG.	GENCENTRIC LAT.	RANTUS TO
RETROFILE	FATH ANGLE	44GL E	(0200025)	(DECREES)	FARTH CENTER
(SEC)	(OFGRETS)	(DECE+ 28)			(+=-1)
1214 755	-1, 392	43.076	00,400	28.331	21372238.0
1217.111	-1.701	94. 71	20.694	28.349	2137 R27.5
1219.500	-1,771	94.165	30.477	78.364	21369413.1
1221.954	-1.391	94.259		74.370	21367096.7
1224.300	-1,351	P4. 353	135.247	78.305	2136556% 7
1226.735	-1.30	BL 247	177.434	28.415	21365152+7
1226.349	-1,390	P4 434	10.810	20.44	21362319 0
1221.01	-1.30	84.771	1004	28.455	21 361-903. 0
1236. 30	-1. 280	94. 275	3 . 7 . 3 44	78,449	21359496.5
1238.75	-1.388	R4, 977	1-1.373	28.493	21358171 7
1241-101	-1.3PP	45.015	111.550	25.497	21356655. *
1243.50	-3-348	85.11	1-1.746	24.51	2135524~0
1245.5	-1,3P7		1.12.133	70 534	2197982967
1257 732	-1.387	95,20K	1.7.31	78,540	7135 006 5
1253,131	-1.3Pf	96 461	177.498	28.561	21349582. 9
1255.510	-1.286	P.F. 5 RA	1-2.584	28.574	21348165.5
1257.900	-1.385	95.691	- 102-974	2R, 585	21346755.5
1260.237	-1.345	0E. 775	113-151	78.597	21345350.5
1267. 77	-1.3**	85 871		28.67.9	71747517 9
1205-171	-1 304	96 (62	103.637	28,631	21341175.5
1265.900	+1.382	86.158	193.814	28.641	71330694 0
1272.200	-1.342	86.254	104.004	78.652	21238253. D
1274.70	-1.242	86.751	1 4.107	28.642	713-6877.5
1276.315	-1.381	85.414	1 4.27	78.66B	21235923.7
<u>1279,47</u> €	<u>.=</u> 1.380	P6.547	174.5AR	P.6R1	21334.47.7
1201.3/2	-1.350	66 T33	1-4-7-7	28.400	21332659.5
1286.475	-1.270	86, 279	115,736	28.708	21379242.2
1229. 75	-1.278	R6. 375	1 . 373	28.717	21 32 8434. 7
1291.47e	-1.378	a7,020	1-4.512	24.72*	?1327'7.2
1293.847	-1. 277	R7.116	1.4"900	28.733	21325637. 0
1296-275	-1, 377	87.212	105.890	28.743	21374214+ 2
1298.675	-1.376		1.5.73	7 P. 74A	71727878.7
1303.474	-1.374	27 5 7	1 6 650	76.775	21310000 5
1305.875	-1.374	87,599	115.547	78.760	71318595 7
1308.261	-1.373	87.694	156.835	24.776	21317211.7
1310.647	-1,372	87.790	1.7.724	2*.782	21315896.7
1313.447	-1.372	87. F#7	1 . 7 . 71 3	2 9. 700	21314415.2
1317.476	-1.371	R7.985	17.475	78.74	71 11 70 47. 5
1326.275	-1-370	99,179	107.784	28-874	21210187-0
1327.675	-1.349	88.275	1.7.971	78.8.9	21378787.7
1324.350	-1.368	RR. 347	1-8.1-4	78.812	71377811.7
1327.750	-1.347	RP. 44 7	1 8,347	78.91 A	21276158.5
1729.791	-1.201		118 202	"R, R71	71 45 64 46, T
1334.09/	-1 345	99 735	1 18 874		21232200.7
1336.959	-1-364	88.451	170,153	78.837	71350474.2
1338. #91	-1.367	49.070	1.9.255	70 835	71 290157.5
1341.750	-1.362	en, 45	1.0.44-	2 P. 83 P	71 7976 86. 7
1347.697	-1,361	90.177	1 2.63	79. R4"	71 736546. 7
1346.55	-1.76	30.238	1.0.342	2P. P43	21 274077. 5
1368 605	-1 247	20 216	115.015	78.844	71 203783. 2
1341.350	_1,350	39 47 7	11 747	78.846	1217121
1353.293	-1.749	10.53	1.35	7 R. 84P	21201-13.
1356.159	-1.257	29.426	11 ++ 427	28.84P	71289347.7
135A. 91	-1.756	>C.7.5	11 .775	7P. 45	21288226.5
1.14: 0.34	-1.355	20, 277	111.776	28,851	21284547.7
1362.071	-1 357	10, 17	111.394	78.54	7129292307
17/7.42	-1.367		111.576	78, 851	71297487 7
137 .595	-1.251	211	111.744	7 A. 85	71281-56 7
137.49	-1.357	· • • • • •	111.012	28.F5/	27991 %. (
1375.376	-1.340	· · · ·	112.147	25.846	21278245.7
1377.335	-1.340	00,455	117,71	78.849	21277129.5
1197.4175	-1.347		117.4979		21 274373 E
1364.004	-1.745	706	11 2 6	79 94	1127777R. 2
1386.934	-1.344	0.442	112. 62	28.84	21271615.0
1384.795	-1. 747	25° E 6 8	117.130	· · · · · · · · · · · · · · · · · · ·	71259975. 5
1391.735	-1.747	-1. 47	112.261	2P. P35	21268864. 7
1304-637	-1.343	e1.134	112.(73	26.971	71247203.2
1306.526	-1. 34.	21.741	112,074	79,828	21266117.2
1555+427	-1,718	11.31	114.7 7	28.874 78 971	21204409." 71263355 0
14^4. 73R	-1.374	51,573	114.435	28,814	71261719.7
14" 6.17"	-1.335	91 651	114.588	28.812	7125-516 5
14 9. 30	-1. 324	21.767	114.BTA	74.9.4	21 258982.5
141 77	-1.333	C1, P45	114.740	2 R. P 57	21257883.7
1433,83P	-1.31	21.04.2	-115,107	7 A. 704	21256251.5

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TIME FROM RETROFIRE (SEC)	ATH ANGLE ATH ANGLE (OFGATES)	FELATIVE HEADING <u>AMGLE</u> {\$FERRES}	1NCETIAL LONG. 	GEOCENTRIC LAT. 	PADIUS TO FARTH CENTER (FEFT)
1415.771	-1.321	92.04	115-351	28.702	?1255153.2
1416.639	-1-370	92.155	115.578	28.785	21253524.5
1477.57	-1.327	02 357	115,757	28.772	21252429.5
1425.371	-1.326	92.478	116.112	28.767	21249707.0
1428. 777	-1-274	92,544	114.243	28.759	21249"62.0
1437.711	-1.373	07.674	116 776	28.753	21246968.2
1475. 11	-1.2	C7_819	116.978	78.738	21244757.7
142 . 977	-1, 19	02,436	117,115	26.778	21242641.5
1430.912	-1.318	da, 12	117.254	79.772	21241557.0
1442.4577	-1.715	02.5 5	117.630	78.7.4	21238952.5
1447.478	-1,213	777 50	117,047	29.694	71237243.5
144.0.445	-1.212	93.477	119. 27	26.446	21236140.0
1452+277	-1.31	C3.516	119.404	78.67	71234553.2
1457. 79	-1.3 7	73.7 2	113,620	2F.65F	71231868.0
1450. 45	+1+?" +	02.780	110.784	2R. 645	21 230 769. 2
1463.077	-1.2.2	03.05°	110 145	28.474	21229189.2
1465.79	-1 -1 -1	04.4	117.310	78.616	21227010.5
1468.546	-1.20	24.176	119.546	7 P. F. 2	21225422.7
1471.590	-1.20P	94.754	110.710	28.59?	21224743.2
1475.30	-1.295	24.642	17. 9	28.569	21222749+0
1478.279	-1,253	94.549	12 . 1 .	29.554	2122 83.0
1482,19	-1.201	24.777	17 .5RC	79.528	21217431.2
1487.854	-1.289	64.05°	121.069	28.5^1	21214799.0
149 . 654	~ / • " P4 ~ * • * P1	05,512	121,121	28.473	2121216045
1490.432	-1.277	06.415	171.094	78,437	712 R446.2
151 2. 299	-1.277	05.570	127.21	2F.414	21216880.0
15 4.232	-1.276	25.45.8	177.762	28.4 1 78.197	71205825.2
1512.252	- 7	05,07	1	7F 74A	21211461.7
1514.417	-1.240	26. 36	127,1/0	20,322	2121 287. 1
1516.545	-1.267	06.110	122.336	78,219	21100137.2
1518.712	-1.255	CA. 275	127 . 177	25.287	2119/95/01
1524.761	-1.261	94.413	1 23. 330	20.264	71195 77.2
1526.22	-1.250	04.40	124.100	78.248	21103909.2
1529.147	-1.257	56 663	126 620	24.232	21192756.2
1532.735	-1.257	16.711	174.601	28.100	21199879.7
1535.854	-1.25	06.P74	124.858	28.174	21198747.5
1535.770	-1.248		125, 24	28.156	21187587.7
1547 377	-1. 741	ç7 . 7 9	176.440	29.113	21194750.7
1545.541	-1.257	77.764	126.510	78. G5	21183634.0
1547.647	-1,734	97.351	125.786	28.277	21182483.0
1555.014	-1.725	97.654	124, 178	25.12	21178525.5
1557.45	-1.271	·7.74-	174.545	27.033	21177416.5
1555.512	-1.217	07.627	126.714	27.073	21174291.2
1561.077	-1.214	د (0 • دی	124 *802	77.954	21175174.7
1564.85	-1.2/8	02.530	127.122	27.925	21173531.5
1565.147	-1.107	ca_, , , ,	127.464	27-895	21171339-5
1571.333	-1,102	09.067	177,427	27. RA4	21170230.0
1574.576	-].185	99.470	127.886	27.833	21168614.0
1576+654	→1,191 -1,174	09.499	128.051	27.813	21167550.5
1581.014	-1.17]	CR 644	124.141	27.771	21145416.7
1564.135	-1.167	99.766	1 2 9 . 4 3 1	27.730	21163834.5
1586.254	-1.159	08.847	123,795	27.718	21162793.7
1591.533	-1.148	04,004	120.126	77.674	21160707.7
1593.677	-1.14	99.11	20.17	27.642	21159181.7
1595.854	-1.136	00.147	127.576	77.610	21158144.7
1507.997	-1.120	26 764	179 945	77.897 27.574	7115712845 71156114.8
161-3-335	-1.115	00.455	137.111	77.54	21154610.5
1605.455	-1.108	99.574	13 . 272	27.518	21153622.7
1607.500	-1.101	99.604	13' 434	27.405	21152634.5
1612.897	-1.EP7	994077	13 .5 13 .P41	27.437	21151049+5
1615.071	-1.1.80	99,94	121,022	77.413	21149247.2
1617.147	-1.(76	0.01	131.164	27.389	21148292.5
1619.798	-1.050	100.004	131.327	27.365	71147333.2
1624.596	-1.054	170.170	131.726	27.3 6	21145006.5
1626.748	-1.047	1 .253	131,880	27.281	21144067.5
1628,871	-1.f47	100.330	132.048	27.257	21143152.7





TIME FROM RETROFIES (SEC)	PILATIVE FLT. PATH ANGLE (DEGREFES)	RELATIVE HEADING ANGLE (DEGREES)	INTERTIAL LONG. IDTOPTION	GEOCENTRIC LAT.	PADTUS TO CARTH CENTER (FEET)
1632.061	-1.623	1.1.424	132.287	27.225	21141796.7
1634.197	-177	1 429	127.446	27.195	21141895.7
1676.317	-1.020	1	117.5	27.171	2113000A.7
10394422	-1	1	117.008	77.100	21127808 2
1643.740	-10 y	1 79	133.156	27.84	21136943.0
1645.874	597	1***.941	133.317	27.158	21136187.2
1649.052	*76	1	133.544	27. 21	21124825-5
1651.216	- 050		133.7-4	24. 395	21133978.0
1655-474		1 1.171	174 14	26.944	21132336.7
1658.652	544	1 1.2 8	134:745	76.916	21131132.0
1660.774			134.379	26.886	21130336+2
1662.912	537	1. 1. 14	134.551	24.854	21129541.5
167 . 34:	- 436	1 1.400	135 11	26.745	21126814.7
1672.466	938	1 1.531	135. ?31	26.739	21126037.5
1677.813	040	171.644	135.67	26.674	21174094.7
1682.066	- 947	1 1 7 7 9	135.077	26.623	71177541.7
1684.204	- 044	1 1.774	1 14. 5	24.597	21121791.5
1687.414	951	. 1 j.pan	124,271	26.558	2112-639.0
1689.541		- 11.865	135.415	26.533	73119872.5
1691.00	+1.726	171.0°R	136.30	20+71	21119040.0
1696.654	-1.11	1.1.0.24	174 397	26.445	21117166
1703.672	-1.2**	1 7-114	1	34,388	21114967.5
17:3+565	-1,774	1 7. 44	117,155	26.366	21314 43.2
1706.627	-1.523	1:2.123	137.557	26,379	21112437.2
17 8.792	-1 720	1 2.7	137.498	74.7 4	21111211.0
1713.597	-1, 431	1.7.4.8	137.975	74.753	21104552.0
1715.246	-1.899	172.539	138.113	26.228	21107140.2
1718.436	-1.051	1.2.779	138.935	26.190	21154998.0
172(-1.956	102.871	138.45/	26.164	211 3541.0
1724.874	-1,033	172.541	179.714	26.114	21130707 0
1728.172	-1.927	1-2.771	138.979	24, 76	71 98637.5
173(-195	-1.939	172.995	139. 36	76. 57	21097285.2
1732+527	-1.079	1-3-7-22	139.162	26.027	21095951.0
1737.672	-1.601	1 3.12	130.475	25.967	71197697.5
1779.795	-1. 77	1 3.156	139.506	25.043	71-91438.7
1741.922.	-1.546	1_3,19?	132+716	25.02	21173212.5
1747.235	+1.851	1 3.26	139.447	25.846	21-48974.5
1749.297.	-1. ***	1 3 774	14	76 641.	2100 C 00 C
1751.273	-1. F47	1 3.707	14	25.813	21 45509.2
1754.220	-1.PF4	1	14. 397	25.790	21383432.*
1761.166	-1 0-9	1-3,227	14 .736	25.720	21070761.5
1764.188	-7. 97	1 3.136	14 .034	75.692	21078131.2
1766.086	-2.221	153.40	14 .975	25.674	21/27/-63-0
1771.020	-7.8°P	1.2.226	141 7	75.656	21 75877.7
1776. 772	-3.545	1 2 1 2	141 435	75.587	21: 799 42. 2
1777.965	-3.783	123.297	141.518_	25.571	21 "68421. 2
178(.958	-4.(42	1.12.571	141.444	75.54A	21 45715.2
1785.177	-4.175	1 3 95.	141 814	75 SJ	71-43897.7
1787.309	-4.215	1 3.672	141.073	25.495	21.5195547
1790.472	-4.296	113.735	142. 24	25.471	21057278.7
1792.595	-4.363	-1-3-619	342+12?	25.454	23 55467.5
1796.918	-4.4F4	173.454	147.757	25-421	71 53697 C
1801.272	-4.566	1:2.397	142.364	25.6 6	71 140347.7
18 2.195	-4. 125	1.3.304	147.433	25.393	21147605.7
1806.474	-4.698	1 3,381	147.51	25.3A1	21-46-77.5
1819.516	-4.975	2 2 2 1	147,455	27.55PP 38.257	21744473.7 21 47961 F
1911.487	- 5.12	1	147.71	75.241	21 4 837 7
1814.51/	-5.521	107+096	147.707	25.327	21 38654. 7
1819,427	-5,859	177.893	147.84*	25,310	21 37237.5
1821. 361	-7.371	1 (Y = 0 (P 1 (7 = 5.57	147_061	75+530 75,700	21124047.5
1823.335	-8.114	1.5*200	143	75 201	21 31657 7
1826.315	-9.217	1. 7.776	347. 73	26,581	21 18954.
1831, 311	-9,673	113.470	147,511	25.274	21 27111.7
1433.320	-11-14	173.449	1-2+1/1 143,238	12+254 35.254	21-74245.7
1835.448	11.585	103.680	143.245	25.251	21026341.7
1835.627	-12.466	1 3,43P	147,200	25.747	71 1 74 R6. 7
1847.884	-13.782 -14 383	1-3.14-	147,772	75.237	21 115534,7
			177.004	/b.232	1 14647.5



,



TIME FROM RETROFIRE (SEC)	PILATIVE FLT. PATH ANGLE	PELATIVE HEADING	INCETIAL LONG. (DEGRETS)	GEDGENTRIC LAT.	RADIUS TO
(000)	10.20481.21	(100.01 . 5)			(+5+()
1845.148	15. 441	1-2.574	143.395	25.228	21011574.0
194 8. 228	-17.260	1	143.478	25.222	21 18752.7
1850.315	-18.200	1 1.704	147.464	25.219	21.1 6833.2
1852.441	-19,547	11.472	142.40	25.214	21 4893.7
1854.579	-21.042	1 1.129	143.514	25.213	210-2956.7
1857.747	-23.277	171.544	142.548	25.214	21000100.7
1859,875	-24.770	100.051	143.57^	25.211	2/ 998217.2
1867. 14	- 26.455	20.421	142.500	25.215	2 996341.0
1864.135	-29.13*	08.856	143.61	25.214	2-994494.7
1967.272	-317	C7.854	143.537	25.2.2	2 971793.C
1869.32	-32.830	97.124	143.654	25.271	20993163.7
1874.51/	-38 - 188	94.945	143.694	25.100	21985769.0
1876.552	-4".289	33.441	143,700	25.19P	2. 994106. 2
1978.648	-47. # 70	02.200	143.723	25.198	2: 982437.
1091.748	-46.(1	00.0 <u>2</u> 4	147.741	25.198	2: 979997.2
1863.796	-49.293	HR.740	143.756	25,108	21078413.1
1885.898	-5'+617	86.582	143.769	25+198	27976821.7
1898.030	-53.063	84.071	143.788	25.199	21974524.2
1891.730	-54.281	82.749	143.700	25,199	2:973.57.5
1997.157	-5.207	32.444	143.817	25.100	21971552.7
1895.334	- 76 - 1 - 2	4 · · · · ·	144.474	25.2	20972054, 5
1998,474		44. 60	141.341		2.967941.0
195-55		94.11.7	143.877	20.2	27.966591.2
1975.744	-74.220		143.85	25.271	2 963253.2
1933.863	-07.772	47.944	144.021		7 948629.2
1939.	-44 010	03 203	144.140	75 2 2	2. 940349.1
1941.105	-47.579	21 051	144 7	26 272	21 94373
1446.14			· · · · · · · · · · · · · · · · · · ·	_ ** •2 ; *	() 44442[[]+
1946.206	-66.496	e . <u>. 7.7.</u>	144. 70	25.202	22943811.0
1949.299	-66.376	76.770	144. 00	• 2 2	043547.5
1953.364	-5.3. 77	77.442	144.1 3	22•2.2	7°941951.
1953.45	-56.021	11.000	144.113		2 941217.7
1955.400	-67.898	78.009	144.127	57+272	20949991.7
1958.514	-68.128	8.476	144.131	27.27.1	21939432.2
1961.001		79+D1/ 04 437	144.140	25.2.2	21,434757.5
1902.347	-40.000	00.04	164 140	26 2 3	2 027/26 7
10.7 051		0 5/0	144 170	52 8 4 7 36 353	2 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
196 (+2)1	-49 072	2 4 2 7 2	144.199	25. 202	31 925797.5
1073 (33	-69.974	69.783	144.202	25.2.3	20 034750.2
1075 001	-70 4 94	38.825	144.211	25.263	20 34107 7
1077 147	-70.201	18 572	144.221	25. 273	2/ 933481. 2
1087 204	-72 645	25.511	144.234	25.2.3	2. 932557. 6
1082 375	-74.203	87.536	144.744	25.2.2	2, 071022, 5
1084 38/	-74.673	37.646	144.253	25,203	2 931310.5
1989.547	-76. 273	94,198	144.276	25.2.3	2 929806.0
1993.711	-77.871	95.715	141. 294	25.2*3	2 978637. 5
1998.996	-91 - 6	07.79	14 . 316	25, 2, 2	2 977277.5
201 255	-9 679	an 1	144.325	25. 212	2. \$ 26646. 2
20.4 . 8/	-81.7 6	19, 927	144.330	25, 7- 5	2 \$ 258 7. 5
2016.137	- 04 - 45	11.699	- 44. 34B	25.21	2: \$ 25764. 5
201 9.275	-70 C 12	91.6	44.356	25.271	20124802.0
211.287	-77.7	39.07	144.360	25.21	20 4 24362.0
2 .13.377	-75.2-	OF. 45	144.378	25.215	201024150.7
2-15.424	-74,1 2	19.4.4	144.397	25.213	21 12 3947. 0
2:19.522		12 cf 3	144.4	25.200	7 02 3769. 5





Table B-2b.Reconstructed Reentry Trajectory,
Special Parameters (Continued)

TIME FROM	OFLATIVE FLT.	PERATIVE HEADING	INCETTAL LING.	GENCENTRIC LAT.	CADTUS TO
RETROFTER	DATH ANGLE	SHOLT	(PEGDECS)	IDEGPESS	FARTH CENTER
(SEC)	105985551	(DEGREES)			(FEFT)
				36 333	~~~~~~
2025-571	-44. 11	12.122	140.429	27.2.17	2. 9237 1.2
2.522.65			140.418	20 • 2 · 2	2. 97. 500%
2075.722		N' . 40e		· · · · ·	2.42.3014.7
2027.771	-41. "	1 1.	144.4**		7 013583.7
2029.867	-36.613	17.517	144.448	2*+2'-3	20.023539
2032-922	-37.617	113.4.6	144.461	25.27.3	21 97 94 14, 2
2135.	-47.78	94.073	144.47	25.713	2-973434.0
2737.163	-32.76P	P6.14]	144.470	7 . 2 3	2-4244R3, 7
2041.165	-35.728	77.267	144.477	75 • Z · 3	7 923315.2
2047+403	-47.012	114.474	144.527	~ ~ ~ ~	7 923145.7
2049.451	-43.84(1.0.0-1	144.532	25.217	Z 92319". Z
2051.490	-54.150	Let 0.	144.54	25.203	21.423. 24. 1
2054.674	-59.771	az. 573	144.552	25.203	20922977.0
2156.65	-57.165	17.4" P	144.567	75.203	2.022020.2
7-56.741	-59.475	07.113	144.57	22.203	21922841.7
2061.873	-40.6 P		144.544	25.27	2 9278.7.5
2063.851	-45.716	82.140	144.59?	25.263	2 92276 . 5
2065.941	-45.652	11.967	144.61	25.273	2 922714.0
2069.003	-28,603	88,007	144.614	25,203	20922641.5
2.71. 201	-33.1.3	PA, CP 3	144.573	25.213	21 922593.5
2073.147	-40. *7?	1-4.676	144.632	25.2.3	21 92 25 50. 0
2076.204	-63.44	157.676	144 . 44"		21 977485.5
2078.292	-52.277	01.1.1	144.554	25.203	<u>2^977443.7</u>
2086.350	-35.352	77,030	144.567	25.273	20 922398.0
2082.471	-27.192	79.560	144.671	25,213	20922355.5
2-85.567	-56.172	A1.750	144.585	25.2.3	24922291.5
2087.617	-F'.P17	05.444	144.407	25.27 3	20977746.5
2799,711	-41.646	~4.765	144.7.17	25.213	25.323206.7
2092.812	-53.792	124.354	144.715	25.2.3	23422124+2
2.04.242		14 .125	144.774	· · · · ·	2092208 6 7
2096.055	-46.418	125. 65	144.713	23.2	20922030
2102.11	-29.779	17.484	144.746		
2102.096	-47.P^3	308.876	144.755	25+213	20921932.0
2154.154	-65.273	-173,939	144.763	25.23	20921884.5
2107.249	-58.637	131.285	144.776	25.252	20921812.7
21-5.296	-44.619	1.5.81.8	144.785	25.2.7	2.1621 764. 7
2111.354	-56.208	137.001	144.794	25,2.17	2-921728.2
2114.448	-49.898	-177.542	144.8.7	22 ?	2 921668. 2
2116.497	-47.206	127.4R7	144.815	25.212	20921625+2
2121.648	-50.879	-161.276	144.837	25.272	20921505.0
2123.671	-27.109	-143+450	144.845	25.2.22	20921464.7
2128.823	-48.532	104.676	144.867	25.202	2° 931 379. r
212	55.767	1	144.974	7E_29.2	3//921334. n
213662	-51, 850	135.065	144.897	25.212	21921214.2
2138.112	-44.453	146.261	144.976	25.201	20921169.7
214r.100	-46.178	-166.186	144.915	25.201	20921125.0
2143.297	-27-268	179.650	154.928	25.201	20921061.2
2145.33	-41.494	12*.787	144.936	25.271	20971021.0
2147.43P	-32.152	111.386	344.945	25.201	20920983.5
2151.541	-44.44	151.088	144.958	25,201	20920935.5
2152.581	-34.617	156.219	144.967	25.201	20923904-2
2154.673	-35.237	151.344	144.975	25.201	20923871.5
2154-673	-35.237	151.344	144.975	25.201	20920871





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APPENDIX C IMU CALIBRATION HISTORY

The following plots contain the history of the preflight calibration values for the accelerometer bias and scale factors and the gyro drift rate. The bias and scale factors are shown as the differences from the flight value, and the gyro drift rate is shown as the actual calibrated value (there is no in-flight adjustment for the gyro drift rate). This information was provided by NASA/Honeywell.

Figures		Page
C - 1	Accelerometer Bias History (Deviation from Flight Constant)	C-2
C-2	Accelerometer Scale Factor History (Deviation from Flight Constant)	C-3
C-3	Gyro Constant Drift Rate History	C-4
C-4	Gyro Input Axis Unbalance Drift History	C-5
C-5	Gyro Spin Axis Unbalance Drift History	C-6



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Figure C-1. Accelerometer Bias History (Deviation from Flight Constant)











Figure C-2. Accelerometer Scale Factor History (Deviation from Flight Constant)



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Figure C-3. Gyro Constant Drift Rate History

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Figure C-4. Gyro Input Axis Unbalance Drift History

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Figure C-5. Gyro Spin Axis Unbalance Drift History





APPENDIX D ERROR SOURCE REGRESSION ANALYSIS

Tables		Page
D-1	Tracker Noise Estimates	D-3
D-2	Error Model A Priori Uncertainties	D-5
D-3	Recovered Errors and Uncertainties	D-6
Figures		Page
D-1	Error Source Recovery History — TSF, DT	D-9
D-2	Error Source Recovery History — A2(4), C2(3)	D-10
D-3	Error Source Recovery History — C4(3), A4(4)	D-11
D-4	Error Source Recovery History — A4(1), PHIZ	D-12
D-5	Error Source Recovery History — XSF, YGIAG	D-13
D-6	Error Source Recovery History — ZGIAU, ZXMSL	D-14
D-7	Error Source Recovery History — ZSF, CO(3)	D-15
D-8	Error Source Recovery History — POX, POZ	D-16
D-9	Error Source Recovery History — POY, XGSAU	D-17
D-10	Error Source Recovery History — DO(3), FO(3)	D-18
D-11	Regression Residual RMS History	D-19
D-12	GE Mod III △P and Regression Fit in Tracker Coordinates	D-20
D-13	GE Mod III △V and Regression Fit in Tracker Coordinates	D-21



 Figures
 Page

 D-14
 MISTRAM I 10K and Regression Fit △V in
Tracker Coordinates
 D-22

 D-15
 MISTRAM I 100K and Regression Fit △V in
Tracker Coordinates
 D-23

 D-16
 MISTRAM II Passive △V and Regression Fit
in Tracker Coordinates
 D-24





APPENDIX D

ERROR SOURCE REGRESSION ANALYSIS

The regression analysis was performed using the IMU telemetered data together with tracking data from the GE Mod III, MISTRAM I 10K and 100K system, and data from the MISTRAM II (Eleuthera) system. The fit domain was that of the following tracking systems:

> MISTRAM I 10K Ř_{SUM}, Þ, Q MISTRAM I 100K Þ, Q GE Mod III R, A, E, Ŕ, Þ, Q MISTRAM II Ř_{SUM}, Þ, Q

This domain was selected since MISTRAM position bias errors have no effect. Weighting of the data was accomplished by visually examining the residuals prior to the fit to determine white noise 1-sigma estimates. Table D-1 indicates the various 1-sigma noise estimates which were used in the regression program.

Tracker		From (sec)	То	1σ	From	То	1σ
	R	120	160	10 ft	160	330	20
	A			0.00005 rad			0.00005
CE Mod III	E			0.00005 rad			0.00005
GE MOU III V	Ŕ			0.25 ft/sec			0.5
	Þ			0.01			0.02
	là			0.01			0.02
	RSUM			0.25			0. 25
	P _{10K}			0.01			0.005
MISTRAM I	QIOK			0.01			0.005
	P _{100K}			0.03			0.01
	Q100K		ł	0.03	•	•	0.01
		140	360	0.15			
MISTRAM II	¢Р			0.02	-	-	-
	٥	•		0.02			l

Table D-1. Tracker Noise Estimates



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Table D-2 lists the total postulated models together with the a priori 1-sigma uncertainties. This model was input into the Recursive Error Modeling Program (REMP) with about half of the terms excluded from the fit. However, the statistical effect of this exclusion is accounted for (Reference 5).

Table D-3 lists the final model selected by REMP along with the error coefficients recovered in the fit. Also in the table are the a priori uncertainties and the a posteriori uncertainties (i. e., the uncertainty associated with the recovered error term). The REMP does a preliminary ordering of the total error model based on the effect of the error function due to the associated 1-sigma a priori uncertainty. The weighted least-square curvefit then proceeds a term at a time using the established sequence. In this manner, the more prominent error sources are used first in the regression solution. The program rejects error functions as the solution proceeds if they are "excessively" correlated with one or a combination of the previously selected functions. The correlation limit (the definition of "excessively") is an input item and has been empirically determined. In this analysis, the following error sources were purposely omitted from the fit, but left in as far as the a posteriori uncertainties are concerned:

BX	PHIX
BY	PHIY
ΒZ	VOX
YSF	VOY
A9(4)	VOZ
A10(4)	YGSAU
A11(4)	ZGSAU

In addition, the following terms were automatically omitted by the program due to correlation:

YGCDR XGIAU ZGCDR XGCDR





Table D-2. Error Model and A Priori Uncertainties

Error	Description	fo a priori uncertainty
вх	X accelerometer bias	5.0 ppm
BY	Y accelerometer bias	5.0 ppm
BZ	Z accelerometer bias	5.0 ppm
*xsf	X accelerometer scale factor	160 ppm
YSF	Y accelerometer scale factor	160 ppm
*zsf	Z accelerometer scale factor	160 ppm
* _{POX}	X initial position bias	50 ft
*роч	Y initial position bias	50 ft
*poz	Z initial position bias	50 ft
XGCDR	X gyro constant drift rate	0.1 deg/hr
YGCDR	Y gyro constant drift rate	0.1 deg/hr
ZGCDR	Z gyro constant drift rate	0.1 deg/hr
vox	X initial velocity bias	0.5 ft/sec
VOY	Y initial velocity bias	0.5 ft/sec
voz	Z initial velocity bias	0.5 ft/sec
*xgsau	X gyro spin axis unbalance	0.2 deg/hr/g
YGSAU	Y gyro spin axis unbalance	0.2 deg/hr/g
ZGSAU	Z gyro spin axis unbalance	0.2 deg/hr/g
XGIAU	X gyro input axis unbalance	0.2 deg/hr/g
*YGIAU	Y gyro input axis unbalance	0.2 deg/hr/g
*ZGIAU	Z gyro input axis unbalance	0.2 deg/hr/g
ZXMSL	Z accelerometer misaligned toward X	35 sec
рніх	Platform misalignment about X	45 🙃
РНІҮ	Platform misalignment about Y	45 sec
*PHIZ	Platform misalignment about Z (IGS azimuth)	100 500
TSF	Timing scale factor	100 ppm
DT	Timing bias	0.01 sec
*A4(1)	MISTRAM I refraction error (central site)	5 n units
C2(3)	Time bias in Mod III	0.01 sec
*C3(3)	GE Mod III range bias	100 ft
*C4(3)	GE Mod III refraction error	5 n units
*DO(3)	GE Mod III azimuth bias	0.0002 rad
*FO(3)	GE Mod III elevation bias	0.0002 rad
A2(4)	Time bias in passive MISTRAM	0.01 sec
A9(4)	MISTRAM II X survey	50 ft
A10(4)	MISTRAM II Y survey	50 ft
A11(4)	MISTRAM II Z survey	10 ft
*G3(4)	MISTRAM II rate bias	0.5 ft/sec
*A4(4)	MISTRAM II refraction error	5 n units

* The asterisks indicate those error coefficients solved for in the regression.



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Table D-3. Recovered Errors and Uncertainties

Name	Coefficient value	A posteriori uncertainty	A priori uncertainty	Number of sigmas*	Units
TSF	-89.9	19.7	100.	0.9	ppm
DT	+0.025	0.0055	0.01	2.5	sec
A2(4)	+0.00088	0.0019	0.01	0.08	sec
C2(3)	-0.00013	0.00036	0.01	0.001	sec
C4(3)	+15.29	3.3	5.0	3.0	n units
A4(4)	+3.15	5.1	5.0	0.6	n units
A4(1)	+1.71	5.2	5.0	0.3	n units
PHIZ	+56.9	1.8	100.	0.57	sec
XSF	+198.	29.8	160.	1.2	ppm
YGIAU	+0.0019	0.29	0.2	0.01	deg/hr/g
ZGIAU	-0.18	0.30	0.2	1.	deg/hr/g
ZXMSL	-37.9	37.4	35.	1.	sec
ZSF	-57.8	157.	160.	0.35	ppm
CO(3)	+74.3	11.6	100.	0.74	ft
рох	+18.6	55.	50.	0.35	ft
POZ	-30.	58.7	50.	0.6	ft
POY	+31.1	39.6	50.	0.6	ft
XGSAU	-1.1	0.44	0.2	5.5	deg/hr/g
DO(3)	+0.000015	0.00001	0.0002	0.07	rad
FO(3)	+0.00005	0.00002	0.0002	0.25	rad
G3(4)	-0.22	0.088	0.5	0.45	ft/sec

 * This column indicates the magnitude of the recovered coefficients in terms of the a priori 1-sigma.




Table D-3 indicates that only one recovered error coefficient (XGSAU) is very large in terms of its a priori uncertainty. It is felt that this error possibly represents a combination of gyro errors that were excluded. The uncertainty of $0.4^{\circ}/hr/g$ is twice the size of the a priori value (0.2), which testifies to the high correlation of this term with omitted terms. * Some compensating effect does occur between XGSAU and ZGIAU.

Figures D-1 through D-10 are plots of the error coefficients as the regression solution proceeds. These plots represent the value of the error coefficients which would be produced by the program if the solution were stopped at the addition of each new error source. These figures also indicate that the solution for ZGIAU shifts abruptly at the inclusion of XGSAU, indicating correlation between these error functions. Figure D-11 is a history of the RMS (root mean square) of the residuals as new error terms are added. Note that the RMS does decrease as XGSAU is added, although the reduction is not impressive. Correlation between PHIZ and XGSAU is evidenced by the level change in PHIZ when XGSAU is included in the fit (see Figure D-4).

Several REMP runs were made using error functions other than XGSAU; however, the resulting fit to the data was decidedly poorer than when XGSAU was used. Because of this, more credibility is given to the final recovered coefficient. To see if a tracker refraction error might be altering the solution somewhat, a regression run was made that used no data beyond 300 seconds, which insured against small elevation angles; the recovered coefficients remained approximately the same (XGSAU became -1.35 °/hr/g). The final solution included tracker refraction errors, and the data were used over the interval 120 to 360 seconds. Data prior to 120 seconds were not used in order that low altitude refraction effects could be avoided. The actual results of the regression may be seen in Figures D-12 through D-16, which are plots of the residuals input to the program with the curve-fit superimposed. The fit to the MISTRAM 10K and 100K data was extremely good, resulting in near zero remaining mean.

The MISTRAM II data were also fit quite well and appears to be reasonably free of systematic trends.

For an explanation of this, see the Appendix of Reference 5.



The GE Mod III curves indicate that although small, systematic trends still remain in all six parameters (Figures D-12 and D-13). Possibly the most dramatic of these is the R residuals that indicate a ramp-type error remaining in the data. There is no explanation for the remaining bias at this time.

Some remarks are in order concerning the validity of the recovered error coefficients from the final regression run. First, it is seen from Table D-3 that the terms

A4(4)	ZXMSL
A4(1)	POX
YGIAU	POZ
ZGIAU	XGSAU

have a posteriori uncertainties larger than the a priori uncertainties, because so many error sources are carried as "nuisance" parameters without being solved for. In particular, this implies that although XGSAU was continually recovered to a level of $\approx -1.2^{\circ}/hr/g$, it could be a combination of some unsolved errors. It can be said regarding XGSAU that it is the one term that does the best job of fitting the data. Second, the RMS remaining after the fit is the smallest yet observed for a Gemini analysis (see Figure D-11), a plot of the RMS history). This remaining level of 1.0 denotes a near perfect fit in terms of the assumed noise on the data versus the final observed RMS. Third, the histories of the coefficients as the solution progresses (Figures D-1 through D-10) indicates that serious compensational effects are not present to any alarming degree in the final reduced model.





Figure D-1. Error Source Recovery History - TSF, DT





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Figure D-2. Error Source Recovery History - A2(4), C2(3)

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Figure D-3. Error Source Recovery History - C4(3), A4(4)







Figure D-4. Error Source Recovery History - A4(1), PHIZ

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XSF RECOVERY

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1					t - F	1		Ϋ.	1	-		Ť	ZC	SIA	U	17	٩E	CON	έĒ	RY	H	١Ŝ	TOF	1Y	T	1		Í				1	1	
	†	1				11			1.	÷.,		1	11			T			Ŧ			÷.			T	1		T				1		
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Figure D-6. Error Source Recovery History --- ZGIAU, ZXMSL

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Figure D-7. Error Source Recovery History - ZSF, CO(3)









Figure D-8. Error Source Recovery History - POX, POZ





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Figure D-9. Error Source Recovery History - POY, XGSAU





Figure D-10. Error Source Recovery History - DO(3), FO(3)





Figure D-11. Regression Residual RMS History



3150-6036-R8-000 Page D-19



Figure D-12. GE Mod III $\triangle P$ and Regression Fit in Tracker Coordinates





Figure D-13. GE Mod III △V and Regression Fit in Tracker Coordinates





Figure D-14. MISTRAM I 10K and Regression Fit $\triangle V$ in Tracker Coordinates







Figure D-15. MISTRAM I 100K and Regression Fit △V in Tracker Coordinates





Figure D-16. MISTRAM II Passive ΔV and Regression Fit in Tracker Coordinates



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3150-6036-R8-000 Page R-1

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