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PROGRAM TECHNICAL REPORT TASK MSC/TRW G-14

GEMINI 7 INERTIAL GUIDANCE SYSTEM EVALUATION AND TRAJECTORY RECONSTRUCTION (U)

NAS 9-4810

15 FEBRUARY 1966

Issued as: Supplemental Report 4

- To: Gemini Program Mission Report Gemini VII MSC-G-R-66-1

 - By: Gemini VII Mission Evaluation Team National Aeronautics and Space Administration Manned Spacecraft Center Houston, Texas



TRW SYSTEMS

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3150-6024-R8-000 Page iii

ABSTRACT

The report contains a detailed evaluation of the Gemini 7 inertial guidance system accuracy during the ascent and reentry phases of the mission. Total system error is found to be approximately equal to its specification, one standard deviation value. An analysis of the external tracking instrumentation accuracy is also included. The results of the error analyses are used to construct a reference Gemini 7 trajectory for the ascent and reentry portions of the mission.



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CONTENTS

Section		Page
1	INTRODUCTION AND SUMMARY	1
2	INERTIAL GUIDANCE SYSTEM PERFORMANCE ANALYSIS	3
3	REENTRY	25
4	TRACKING SYSTEM PERFORMANCE	31
5	TRAJECTORY RECONSTRUCTION	51
APPENDI	X A TRAJECTORY PARAMETER LISTINGS AND PLOTS	A-1
APPEND	X B TRW REGRESSION PROGRAM (REMP) MODIFICATIONS	B-1
REFERE	NCES	R - 1

Total Pages: 123

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3150-6024-R8-000 Page vii -----

ILLUSTRATIONS

Figure		Page
1	GE/Final and 100K MISTRAM ΔV , Thrust Coordinates	4
2	GE/Final and 100K MISTRAM ΔV, Guidance Inertial Coordinates	5
3	GE/Final and 100K MISTRAM ΔP_{s} Guidance Inertial Coordinates	6
4	Navigation Velocity Error	7
5	Thrust Coordinate ΔV with IMU Error Source Fit	12
6	Accelerometer Scale Factor History	13
7	Accelerometer Bias History	14
8	MISTRAM I 100K ΔV in Tracker Coordinates	19
9	MISTRAM I 10K ΔV in Tracker Coordinates and MISTRAM II Passive ΔR Sum Dot	20
10	GE MOD III ΔV in Tracker Coordinates	21
11	Ground Trace of the Spacecraft During Reentry	27
12	IGS and GTI Tracking Data Comparison	28
13	GE/Burroughs and GE/Final ΔV, Thrust Coordinates	36
14	GE/Burroughs and Compensated IGS ΔV , Thrust Coordinates	37
15	GE/Burroughs and Compensated IGS ΔP , Thrust Coordinates	38
16	GE/Final and Compensated IGS ΔV , Thrust Coordinates	39
17	GE/Final and Compensated IGS ΔP , Thrust Coordinates	40
18	MISTRAM I 100K and Compensated IGS ΔV , Thrust Coordinates	41
19	MISTRAM I 100K and Compensated IGS ΔP , Thrust Coordinates	42

UNCLASSIFIED

UNCLASSIFIED

ILLUSTRATIONS (Continued)

Figure		Page
20	MISTRAM I 10K and Compensated IGS ΔV , Thrust Coordinates	43
21	MISTRAM I 10K and Compensated IGS ΔP, Thrust Coordinates	44
22	Passive MISTRAM and Compensated IGS ΔV , Thrust Coordinates	45
23	Passive MISTRAM and Compensated IGS ΔP , Thrust Coordinates	. 46
24	Range BET and Compensated IGS ΔV , Thrust Coordinates	. 47
25	Range BET and Compensated IGS ΔP , Thrust Coordinates	. 48
26	TOPS BET and Compensated IGS ΔV , Thrust Coordinates	. 49
27	TOPS BET and Compensated IGS ΔP , Thrust Coordinates	. 50
A-1	Computed Thrust Velocity in Computer Coordinates (Thrust Tailoff)	• A-3
A-2	Inertial Flight Path Angle (Ascent)	• A-4
A-3	Computed Acceleration, Thrust Coordinates	. A-5
A-4	IGS Sensed Velocity Rev 1 Booster Chase Maneuvers	. A-6

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TABLES

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7

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Table		Page
1	Inertial Guidance Error at SECO	4
2	IGS Navigation Errors at SECO	9
3	IMU Analysis Recovered Error Coefficients	10
4	Preflight Expected Values of IMU Errors	1.5
5	Tracker Sigmas Used in Fit	17
6	Recovered Error Coefficients	18
7	Azimuth Update	23
8	Reentry Initial Conditions	25
9	Comparison of Reconstructed Trajectory With IGS Output	26
10	Gemini 7 Impact Summary	26
A - 1 a	Reconstructed Ascent Trajectory	A - 7
A-lb	Reconstructed Ascent Trajectory Associated Parameters	A - 1 3
A-2a	Reconstructed Reentry Trajectory and Associated Parameters (BET)	A -19
A-2b	Reconstructed Reentry Trajectory and Associated Parameters (7:18 Radar)	A - 35
A-2c	Reconstructed Reentry Trajectory and Associated Parameters (IGS)	A - 53
A-3	PCM Edit Listing for Ascent Flight Phase	A - 61
B - 1	Unmodeled Errors and 1-Sigma Uncertainties	B - 3

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i. INTRODUCTION AND SUMMARY

Gemini Flight No. 7 was launched on 4 December 1965 from Complex 19 at Cape Kennedy, Florida. It was a 14-day manned orbital flight that included orbit adjustment maneuvers. This report, submitted to the NASA Manned Spacecraft Center by TRW Systems in response to Task MSC/TRW G-14 of the Mission Trajectory Control Program, presents the results obtained from analysis of the inertial guidance system (IGS) performance during ascent and reentry flight phases and provides a reconstruction of the spacecraft trajectory during ascent and reentry.

The following is a brief summary of the analysis results:

- There was no evidence of IGS or component malfunctions during the ascent and reentry flight phases.
- The inertial guidance system (IGS) performance during ascent was satisfactory. Best estimates of IGS errors at injection are as follows:

Δx	Ξ	1440 ft	∆×́	Ξ	7.3 ft/sec
∆ у	Ξ	830 ft	Δý	=	10.0 ft/sec
Δz	Ξ	230 ft	Δż	Ξ	0.3 ft/sec

- The dominant inertial measurement unit (IMU) errors of the flight were:
 - (a) Y gyro (pitch) drifts of 0.55 deg/hr constant drift rate and -0.26 deg/hr/g input axis unbalance and
 - (b) an X accelerometer scale factor error of approximately 217 parts per million
- The tracking data was of satisfactory quality. However, analysis indicated the presence of a refraction type error of approximately 12 parts per million in the index of refraction at the MISTRAM 100 K Q site. There is considerable uncertainty in this error magnitude and even in analytical error model, nevertheless the effect is clearly evident in the data. Also a 0.3 ft/sec range sum rate bias in the passive MISTRAM and approximate 0.1 milliradian azimuth bias in the GE Mod III data was found.





- The GE MOD III-Burroughs/inertial guidance update procedure was correctly performed but the aforementioned azimuth bias in MOD III data resulted in a 20-second residual IGS azimuth misalignment during ascent.
- Failure of the onboard, delayed-time-telemetry tape recorder resulted in the loss of IGS data during most of the dynamic portion of reentry, making a detailed IGS evaluation impossible. However, a comparison of IGS data after telemetry blackout with a segment of very low elevation ground tracking data indicates an IGS navigation error of approximately 3 n mi.

Section 2 of this report provides a detailed description of the analysis performed for the ascent portion of flight; this includes a discussion of:

- a) Inertial Measurement Unit (IMU) accelerometer and platform errors
- b) The radio guidance/inertial guidance update procedures
- c) Airborne computer navigation errors

Section 3 provides a description of the IMU error analysis performed for the reentry flight phase, Section 4 describes the external tracking system performance and quality, and Section 5 presents a discussion of the trajectory reconstruction for ascent and reentry. Appendix A contains the Gemini 7 ascent and reentry reconstructed trajectory and support data, including listings and plots of the thrust acceleration profile, and Appendix B contains a discussion of alterations to the TRW regression program (REMP).



3150-6024-R8-000 Page 3

2. INERTIAL GUIDANCE SYSTEM PERFORMANCE ANALYSIS

Comparisons of IGS telemetered quantities and external tracking data were made for the purpose of evaluating the Gemini 7 IGS performance. The IMU evaluation was based in part on thrust (sensed) velocity comparisons (Figure 1) generated by scaling and biasing telemetered accumulated accelerometer count data and comparing the results with external tracking data adjusted for gravity and transformed to guidance coordinates. The residuals from these comparisons were attributed to IMU and tracking system errors.

Comparisons were also made between the telemetered total inertial position and velocity outputs from the airborne computer and external tracking data (Figures 2 and 3). These comparisons, called total inertial comparisons, include IMU and tracking system errors as well as airborne computer navigation errors caused by gravity approximations, truncation errors, etc. The difference between the thrust and inertial comparison sets are called delta-delta comparisons (Figure 4) and they provide a measure of the airborne computer computational error alone.

The inertial and delta-delta comparisons are referenced to the IGS computer coordinate system, which is an inertial, orthogonal, right-handed system referenced to the center of the earth. The x and z axes lie in a plane parallel to the geodetic tangent plane at the launch site at the time of platform release, with the x axis defined by the launch azimuth, positive downrange. The y axis is positive down along the geodetic vertical, and the z axis is directed so as to complete the righthanded x, y, z set.

Position and velocity comparisons were also made in the external tracking measurement coordinates. These were made for the purpose of isolating IMU and tracker error coefficients by performing computer regressions on the differences.

External tracking data used in the evaluation included Quick-Look MISTRAM I 10K and 100K, GE/Mod III/Final, GE/Mod III/Burroughs, Final MISTRAM, Passive MISTRAM II, and BET. An analysis of these data sources is described in Section 4.







Figure 2. Total Inertial Velocity Comparison in Computer Coordinates





Figure 3. Total Inertial Position Comparison in Computer Coordinates





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3150-6024-R8-000 Page 7 3150-6024-R8-000 Page 8

The plots enclosed are referenced to liftoff time (19 hr 30 min 03.702 sec GMT) which occurred 3.512 seconds after IGS "go inertial."

2.1 IGS ERROR

The indicated IGS errors immediately following SECO (337 seconds from liftoff) and equally valid at separation (357 seconds from liftoff) are given in Table 1. These values were obtained by evaluation of the position and velocity comparisons (Figures 2 and 3). The column headed "IMU Error" represents the error contributed by the accelerometer, gyro, and platform alignment sources; the column headed "Navigation Equation Errors" is the contribution due to various approximations within the airborne computer as observed from the delta-delta comparisons^{*}; and the column titled "Total Guidance Errors" is the sum of the two and represents the total IGS error. These total errors result in velocity magnitude and flight path angle errors at separation of the following amounts:

> |V| = 9 ft/secY = -0.014 deg

Observation	Unit	IMU Error	Navigation Equation Errors	Total Guidance Errors
x	ft/sec	5.6 ± 0.5	1.7 ± 0.2	7.3 ± 0.5
Ý	ft/sec	9.9 ± 3.0	1.0 ± 0.1	10.9 ± 3.0
ż	ft/sec	0.2 ± 1.0	0.1 ± 0.1	0.3 ± 1.0
x	ft	800 ± 50	640 ± 10	1440 ± 51
Y	ft	820 ± 50	10 ± 3	830 ± 50
Z	ft	220 ± 10	10 ± 3	230 ± 10

Table 1. Inertial Guidance Error at SECO

Note: The ± numbers are 1-sigma estimates.

*Level changes at 107 seconds in the x and z curves are due to updating the initial earth rate conditions by the onboard computer as a result of the RGS/IGS update routine.





Table 2 is a comparison of the navigation errors observed on this flight with those predicted by preflight simulation.**

	F	Position (ft)			Velocity (ft/sec)		
Trajectory	x	Y	Z	ż	Ŷ	ż	
Actual	640	10	10	1.7	1.0	0.1	
Simulation	175	60	-18	1.9	0.9	-0.15	

Table 2. IGS Navigation Errors at SECO

2.2 IMU ANALYSIS

2.2.1 IMU Error

Analyses to recover IMU error source coefficients were performed by using the procedures and data processing programs as documented in Reference 1 except that the Recursive Error Modelling Program (REMP) was used for regression analysis. The IMU error source coefficients recovered in the analysis are presented in Table 3. These were ultimately derived from a hand fit to the MISTRAM and GE/Final thrust velocity residuals (Figure 1) and later substantiated by a computer regression analysis (see Section 2.2.2).

The most significant indications of the thrust velocity comparison plots are x and y velocity differences which build up to approximately 2.5 and 2 ft/sec at BECO and 6 and 10 ft/sec respectively at SECO. In addition, small z velocity errors are indicated until 310 seconds after which a negative slope of approximately 0.044 ft/sec² is indicated by MISTRAM data.

The dominant error sources which contributed to the x axis residuals were an x accelerometer scale factor error of approximately 217 parts per million (ppm) and an IGS time scale factor error of -32.2 ppm.

**The preflight values were determined from simulation results obtained by telephone from IBM. Since no exact simulation of the Gemini 7 trajectory was available, values were obtained by interpolating from a series of simulations for similar trajectories with various launch azimuths.





The time error was evidenced by 0.8 ft/sec and 2 ft/sec jumps in the x velocity residuals at BECO and SECO respectively. The accelerometer and time scale factor errors alone did not provide a satisfactory fit to the data however.

Error Source	Recovered Coefficient	Units
X Accelerometer Scale Factor	217	ppm
Y Accelerometer Output Axis Sqd Nonlinearity	100	ppm/cross g
Y Gyro Constant Drift Rate	0.55	deg/hr
Y Gyro Input Axis Unbalance	-0.26	deg/hr/g
Platform Misalignment about Y Accelerometer Axis	20	arc sec
Platform Misalignment about Z Accelerometer Axis	20	arc sec
IGS Time Scale Factor	-32.2	ppm
X Accelerometer Bias	19	ppm g
Y Accelerometer Bias	45	ppm g
Z Accelerometer Bias	-33	ppm g

Table 3. IMU Analysis Recovered Error Coefficients

Pitch type error sources were used to fit the y velocity residuals because they provided the necessary coupling in the x axis to null out the residual x axis velocity error. The pitch error sources which combined with the time accelerometer scale factor error sources to provide the best fit to both the x and y velocity residuals were: y gyro drifts of 0.55 degree per hour constant rate and -0.26 degree per hour per g input axis unbalance, and a pitch misalignment (PHIY) of 20 arc seconds.

The small z velocity residuals indicate negligible IMU error propagation in the z axis; however, a MISTRAM or GE/Mod III error is suggested by the systematic difference between the MISTRAM and Mod III residuals. By comparison of the difference between the two with propagations of possible MISTRAM and GE error sources, it was concluded that the observed tracker residuals are attributable to a -0.005 degree azimuth bias in the GE Mod III data. Since IGS z velocity updating was





accomplished with the Mod III data, the IGS experienced an equivalent residual azimuth misalignment (PHIZ) of 20 seconds after updating.

The z velocity slope of the MISTRAM residuals which exist even after SECO time suggests the presence of a MISTRAM error. Analyses revealed that a Q channel refraction error of approximately 6 n units would account for the velocity slope which occurred beyond SECO (see Section 5). A small residual velocity error still existed in the data after compensating for the refraction error. This was best fit by a z accelerometer output axis squared nonlinearity of approximately 100 ppm/cross g.

The fit associated with the recovered coefficients is presented in Figure 5, which also shows the preflight expected IMU errors presented in Table 4, propagated with the observed timing errors. Comparisons of the errors indicate that the actual pitch drift and resulting y velocity error approximates the preflight values. Conversely, the x accelerometer scale factor error and resulting x axis error was larger than the preflight values and the expected z axis drift was not evident during flight. However, the recovered scale factor error appears to be consistent with the accelerometer scale factor history. This is evident in Figure 6, which shows the variation of accelerometer scale factors between calibrations. The y and z accelerometer scale factors were somewhat constant for a three-month period just prior to launch and were most likely near their desired value during flight since their errors were not evidenced by the flight test data. The x accelerometer on the other hand demonstrated considerable scale factor variations throughout its calibration history.

Accelerometer biases were recovered during orbit phases of flight by determining the slope of IGS thrust velocities during an interval after insertion when no thrusting was being applied (Figure A-4 of Appendix A). The recovered biases are also presented in Table 3. Their small magnitudes are consistent with the accelerometer bias histories indicated in Figure 7.



Figure 5. Thrust Velocity Comparison in Computer Coordinates







Figure 7. Gemini 7 Accelerometer Bias History





Error Source	Magnitude	Units
X Accelerometer Bias	-38	ppmg
Y Accelerometer Bias	100	ppmg
Z Accelerometer Bias	11.2	ppmg
X Accelerometer Scale Factor	40	ppm
Y Accelerometer Scale Factor	0	ppm
Z Accelerometer Scale Factor	10	ppm
X Gyro Constant Drift Rate	0.08	deg/hr
Y Gyro Constant Drift Rate	-0.07	deg/hr
Z Gyro Constant Drift Rate	0.02	deg/hr
X Gyro Input Axis Unbalance	-0.1	deg/hr/g
Y Gyro Input Axis Unbalance	0.22	deg/hr/g
Z Gyro Input Axis Unbalance	-0.11	deg/hr/g
X Gyro Spin Axis Unbalance	0.26	deg/hr/g
Y Gyro Spin Axis Unbalance	0	deg/hr/g
Z Gyro Spin Axis Unbalance	0.07	deg/hr/g

Table 4. Preflight Expected Values of IMU Errors*

*Obtained from Honeywell.

2.2.2 Regression Analysis

A regression analysis was performed on the Gemini 7 IGS and tracker data. The following error model was chosen as a result of the hand fit. The regression program (REMP) assigned the coefficient values and the covariance matrix for these terms.

- XSF = X accelerometer scale factor error
- TSF = Timing scale factor
- POX = X position bias
- POY = Y position bias
- POZ = Z position bias
- PHIY = Platform misalignment about Y
- YGIAU = Y gyro input axis unbalance
- XGIAU = X gyro input axis unbalance
- YGCDR = Y gyro constant drift rate





- A2(1) = MISTRAM I timing bias
- G2(4) = MISTRAM II timing bias
- C2(3) = GE Mod III timing bias
- G3(4) = MISTRAM II rate bias

Several other error sources were carried in the regression program as unmodeled effects; i.e., their effect is examined in the statistics of the recovered terms but no coefficients are solved for (see Appendix B for explanation of this technique).

The regression domain chosen was the following:

P, Q, RSUM	10K MISTRAM
Þ, Q	100K MISTRAM
Ř, P, Q	GE Final (Mod III)
RSUM	Passive MISTRAM

Table 5 lists the assumed noise estimates for these parameters over various time spans in the fit.

The velocity domain was selected for two main reasons: 1) it is completely insensitive to tracker position bias (DC only), and 2) the IGS errors are less correlated in this domain, which usually affords a more reliable inversion of the normal matrix (i.e., less numerical errors in inversion). The coefficients which were recovered fit the ΔV curves (in IGS coordinates) quite well and are all of believable magnitudes.

The assumptions made in conjunction with the regression run are as follows:

- a) The data noise was white (Gaussian).
- b) The selected error model is sufficient to model all errors.
- c) The tracker rate domain is the most desirable for regression purposes.

The MISTRAM I and II and GE Mod III rate residuals were fit quite well. The final recovered error coefficients are listed in Table 6 with their associated a posteriori 1-sigma uncertainties.



Parameter	Sigma	From	To	Sigma	From	To	Sigma	From	To
P10K	0.01	50	160	0.0025	160	280	0.01	280	360
й _{10К}	0.01	50	160	0.0025	160	300	0.01	300	360
^R SUM	0.1	50	360						
P100K	0.02	50	160	0.005	160	360			
й _{100К}	0.025	50	160	0.001	160	330	0.025	330	360
R Mod III	0.15	50	360						
PMOD III	0.25	50	320	0.5	320	360			
Qmod III	0.25	50	320	0.5	320	360			
RSUM _{PASSIVE} MISTRAM	0.1	180	360						

Table 5. Tracker Sigmas Used in Fit

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Note: Sigmas are all in ft/sec and the From/To times are in seconds from launch.

3150-6024-R8-000 Page 17

	1 Sigma
XSF 189	100
рніч 26	32
POX 27	11
РОУ -68	112
POZ 27	64
TSF -56	23
YGIAU -0.18	0.72
XGIAU -0.05	0.59
YGCDR 0.35	0.84
A2(1) 0.007	0.007
G2(4) 0.007	0.0066
C2(3) 0.007	0.0082
G3(4) 0.27	1.7
B5(2) -12.4	30

Table 6. Recovered Error Coefficients

The terms YGCDR, YGIAU, XGIAU, POY, G3(4), and B5(2) were not well recovered since the ratios of a posteriori to a priori recovered error coefficient uncertainties were large. The main cause for this is that so many "unmodeled errors" were carried in the a posteriori statistics. This means that these errors very likely represent some combination of the total error model; however, such a combination is impossible to determine using the data available. The term B5(Z) is a refraction error in the MISTRAM 100K Q leg. This term was originally left out of the fit but the residuals indicated that it was definitely present.

Examination of the histories of recovered error coefficients in the fit as the error model is expanded reveals that the fit is very stable; little cancellation exists and all variations are well within the estimated.

Figures 8 through 10 are the tracker rate residuals used in the fit with the fit itself superimposed on the residuals. It is obvious that some error remains in the data, especially in Mod III and the passive MISTRAM





Page 19









Page 21

3150-6024-R8-000 Page 22

range sum rate data. It was decided that a sufficiently good estimate of IGS error was obtained and that further investigation would not benefit this analysis effort appreciably.

Three timing errors A2(1), C2(3), G2(4) were carried, representing timing biases in the MISTRAM I, GE Mod III and Passive MISTRAM, respectively. It is obvious that the tracking systems have little or no relative timing error between themselves; thus, the ≈ 0.0070 second recovered coefficient for all three trackers should be considered as a bias in the IGS time word of the same amount.

2.3 AZIMUTH UPDATE

An azimuth alignment correction is calculated at three separate times by the onboard computer. On the first pass through the navigation equations after platform release, the roll gimbal angle reading is compared with the desired value and the difference is used as a correction to the intended flight azimuth. This correction is called $\Delta \eta_x$, where a positive value implies that the platform is rotated clockwise from the desired azimuth.

Additional azimuth corrections are made during flight at 100 and 140 seconds after liftoff. These are calculated by comparing the crossrange (z direction) velocity as measured by GE/Burroughs with that derived from the airborne system and attributing the residual to a platform misalignment.

The calculated updates are not telemetered; however, they are obtained quite accurately from the data analysis. Table 7 summarizes the updates determined by the following methods:

- a) Calculated from the telemetry data and simulation of the inflight calculations.
- b) Calculated from the jumps in the inertial velocity comparisons or the delta-delta curve.
- c) Derived by IBM during their postflight simulation.

The value indicated at 100 seconds includes that at 0 seconds. The value for 0 seconds in the delta-delta and TRW simulation column was determined from an observable jump in the IGS z velocity after Platform Go-Inertial. This jump corresponds to the IGS first correction.



Time (Sec from liftoff)	Flight Calculation Simulation	Delta -Delta	IBM Postflight Simulation	Units
0	-0.00006	-0.00017	-0.00017	radians
100	-0.00834	-0.00857	-0.00849	radians
140	0.00003	0.00019	0.00012	radians
Total	-0.00831	-0.00838	-0.00837	radians
(100 and 140)	-0. 4763	-0.4766	-0.4766	degrees

Table 7. Azimuth Update

The total azimuth correction of -0. 4763 has been included in all plots contained in this report.

The history of initial alignment error is:

GT-2	$\eta_x = -0.29 \text{ degrees}$
GT-3	$\eta_x = -0.52 \text{ degrees}$
GT-4	$\eta_x = -0.12 \text{ degrees}$
GT-5	$\eta_x = -0.27$ degrees
GT-7	$\eta_x = -0.48$ degrees

Mean value = -0.34 degrees l-sigma spec value = 0.25*

*Honeywell

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3150-6024-R8-000 Page 25

3. REENTRY

3.1 INITIAL CONDITIONS

The state vectors at retrofire, as calculated by the TRW postflight trajectory reconstruction (ESPOD) and as computed real time by the RTCC and used by the IGS, are given in Table 8.

	IGS (RTCC)	Postflight (ESPOD)	IGS-Postflight
x	18, 485, 400 ft	18, 487, 851 ft	-2,451 ft
у	11, 702, 400 ft	11,699,406 ft	2,994 ft
z	-49,500 ft	-51,845 ft	2,345 ft
ż	-11,874.9 ft/sec	-11,870.4 ft/sec	-4.5 ft/sec
ý	18,780.6 ft/sec	18,783.1 ft/sec	-2.5 ft/sec
ż	12,282.3 ft/sec	12,282.5 ft/sec	-0.2 ft/sec

Table 8. Reentry Initial Conditions*

^{*}t = 18 December 1965, 13h 28m 07s

The coordinate system of the above vectors is that used by the RTCC: earth centered inertial, X through Greenwich at 0^{h} day of launch. This initial condition difference is somewhat greater than has been found on previous flights where the resultant differences have been less than 2,000 feet and 2 ft/sec. However, it was also noted that the quality of the "fit" to the pre-retro tracking station data was poorer than usual. This problem is being investigated as part of the orbit phase trajectory reconstruction.

3.2 POST-RETRO FREE FLIGHT

The best trajectory was fit to the post-retro fire tracking data (HAW and WHS), and the trajectory compared to the IGS output at two points under 400,000 feet. The result is shown in Table 9.

Based upon the accuracy of the telemetry data, there is no significant position difference between the IGS and postflight reconstruction trajectories just prior to atmospheric reentry and telemetry blackout.



	S	pacecraft Position	
Time From Retro- Fire, Altitude	Geocentric Latitude (Deg)	Longitude (Deg)	Radius (Ft)
1307 sec, 383 K ft			
Reconstruction	28.874	257.899	21, 292, 216
IGS	28.874	257.901	21,293,093
1360 sec, 352 K ft			
Reconstruction	28.894	261.881	21,261,090
IGS	28.893	261.901	21,261,071

Table 9. Comparison of Reconstructed Trajectory With IGS Output

3.3 ATMOSPHERIC REENTRY

Because of the loss of the onboard tape recorder data, there is no telemetry available on the portion of reentry between 1400 and 1800 seconds after retrofire, or from approximately 350,000 to 120,000 feet altitude. Ground radar tracking during most of this interval has provided reasonable position data but very poor velocity data. There is, however, approximately 100 seconds of overlapping Grand Turk radar tracking and telemetry data after blackout. The spacecraft covers an altitude range from 120,000 feet to just after drogue deploy at about 60,000 feet. Figure 11 shows the ground trace of the spacecraft as measured by the IGS and as given by the GTI tracking data. The target and shipestimated-pickup points are also shown. An impact summary is given in Table 10. The resultant IGS error at drogue deploy is 3 n mi.

Source	Longitude (Deg)	Geocentric Latitude (Deg)
Target Point	-70.0	25.234
IGS (drogue deployment)	-70.10	25.280
GTI Radar (drogue deployment)	-70.145	25.254
Ship (pickup)	-70.146	25.216

Table	10.	Gemini	7	Impact	Summary
-------	-----	--------	---	--------	---------

Figure 12 is a position comparison between IGS and GTI tracking data in guidance coordinates. The spacecraft is almost due north of the











GTI site at this time, but at an extremely low elevation angle. All the data is below 3° ; after 1840 seconds, the spacecraft is below 1° ; and after 1875 seconds the spacecraft is indicated as being below the horizon. Because of the low elevation, very large errors can be expected in the elevation measurement, which is mostly the x direction in the IGS coordinate set at this time. (The spacecraft has flown through a central angle of 113° since retorfire.) However, the range and azimuth measurement should be reasonable, resulting in valid z and y measurements, respectively. The smooth z curve reflects the good range measurement. The angular data after 1890 seconds is considered invalid.

As a rough measure of what this trend represents in terms of IGS accuracy, it was assumed that all the difference was due to IGS platform misalignment, that the spacecraft velocity could be considered a constant over the interval, and that the slope of the difference was IGS-sensed velocity error. The following errors result:

ΔV_x	=	80 to 100 ft/sec	<u>v</u> =	13,000 ft/sec
Δv_y	=	90 ft/sec	v _y =	18,000 ft/sec
ΔV_z	=	80 ft/sec	<u>v</u> =	400 ft/sec

Equivalent IGS Platform Misalignment is:

Pitch up: 0.3° to 0.4° Roll positive: 0.4°

The ratio of x to y error is only approximately correct for a pitch error; however, the magnitude of the error is consistent with expected accuracies. The data is too poor to speculate further about the sources. No attempt was made to explain the initial position errors indicated on these curves at 1800 seconds because of uncertainty in initializing the IGS data.

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3150-6024-R8-000 Page 31

4. TRACKING SYSTEM PERFORMANCE

Tracking data available for analysis of the Gemini 7 IGS performance included the following:

- a) GE Mod III/Burroughs
- b) GE Mod III/Syracuse/Final
- c) MISTRAM I Quick Look 10K and 100K
- d) Passive MISTRAM
- e) Range BET

Each of the above sets was used for position and velocity comparisons, as described in Section 2. The GE Mod III/Burroughs data were used for quick look analyses; however, detailed analyses were subsequently accomplished with the remaining sources. A TRW program (TOPS), which is used to produce powered flight best estimates of trajectory (BETs), was also used to aid the tracking data analysis.

For convenience, tracking system data were compared with inertial guidance data which has been corrected for guidance system errors derived from the hand fit results of Section 2.2.

Three main tracking system errors were extracted from the ensemble IMU/Tracker analysis scheme. These were:

- a) An apparent refraction error in the Q_{100K} MISTRAM I system of ≈ 12 n units.
- b) An azimuth bias of $\approx 10^{-4}$ radians in the GE Mod III data.
- c) A range sum rate (R) bias of ≈ 0.3 ft/sec in the passive MISTRAM data.

These errors were extracted by using the regression program (see Section 2.2) as well as by manually adjusting the observed residuals. It should be noted, however, that the uncertainities of these errors are large. The regression program included unmodeled effects for both the IMU and the tracking system, which resulted in relatively large a posteriori uncertainties.



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4.1 GE MOD III

4.1.1 GE Mod III/Burroughs

The Burroughs raw data received consisted of raw counts recorded on punched paper tape at a rate of two data points per second. The data were transferred to magnetic tape at TRW and processed in the data reduction programs.

Figure 13 shows GE/Burroughs and GE/Final IGS coordinate velocity comparisons superimposed. Significant differences exist between them in the x and y directions. The x-difference is attributable to a 0.01-second timing error in the Burroughs, and the y-difference is most likely due to an incorrect refraction correction applied to the Burroughs data. This refraction correction is based upon ground refractometer measurements and is updated and refined by airborne measurements in the GE/Final data reduction.

4.1.2 GE Mod II/Syracuse/Final

The GE/Final data were processed by GE/Syracuse from the ten per second Flight Data Recorder output. The data were available raw and unsmoothed in natural coordinates and as smoothed Cartesian x, y, z data. The final GE natural coordinate data were used in the computer regression analyses discussed in Section 3.

In general, the quality of the GE/Final data was quite good. No major errors were apparent, although the moderately large (approximately 10⁻⁴ radian) azimuth bias mentioned in Section 3.2 serves to explain part of the z-coordinate difference between GE and MISTRAM comparisons (Figure 1). This azimuth error was verified by the TRW TOPS BET analysis (Section 4.4), which also showed less than 0.05-milliradian bias in the elevation measurements, and was further verified by the GE Mod III data analysis presented by General Electric in Reference 2.

Plots of the residuals between the GE/Final data and the corrected IGS trajectory are presented in Figures 16 and 17.



4.2 MISTRAM DATA

The quick look data received consisted of scaled and corrected but unsmoothed position data measurements. These are: range sum measurement, R; range difference measurements from 10,000 foot baselines, P_{10K} and Q_{10K} ; and range difference measurements from 100,000 foot baselines, P_{100K} and Q_{100K} . Also range sum, P and Q, measurements from MISTRAM II (Passive mode) were obtained. The data were processed and differentiated in TRW programs to give essentially three sets of tracking data.

4.2.1 MISTRAM I

MISTRAM I/IGS compensated thrust coordinate comparisons are presented in Figures 18 through 21. (Also see Figure 1 for uncompensated IGS MISTRAM velocity comparisons.) These differences show a generally good agreement with GE/Final data in the x coordinate. The z coordinate plots, however, indicate an approximate 0.5 ft/sec difference with those of GE/Final, and while part of this is due to the aforementioned GE azimuth bias (Section 4.1), it was determined in the TOPS analysis (Section 4.5) that the MISTRAM 100K Q channel exhibited an error arising from an outlying site unaccounted refraction difference (see also the regression results of Section 2.2). The effect of this error is to "droop" the z coordinate comparisons after about 300 seconds (compare with the TOPS results of Figure 26). This error was not apparent in the 10K measurements.

The TOPS BET results also showed an approximate 2 n-units refraction error of the same type in the MISTRAM 100K P channel. The effect of this error is most pronounced in the vertical (y) direction, and was of such a sign as to manifest itself also as a "droop" beginning at about 300 seconds. However, the Q refraction error also propagates into the y channel and on this flight was of opposite sign to the P error, thereby resulting in some cancellation. The net effect of these two errors was to cause the y channel IGS/MISTRAM velocity differences to exhibit a negative slope after SECO, a phenomenon which is clearly apparent from Figure 7 and 18. The total magnitude of this combined refraction



error in the vertical channel is estimated at about -2 ft/sec at SECO. No other significant MISTRAM I errors were detected on this flight.

4.2.2 MISTRAM II (Passive Mode)

MISTRAM II/Compensated IGS comparisons are shown in Figures 22 and 23. The regression results (Section 2.2) showed an approximate 0.27 ft/sec range sum rate bias, which is confirmed by the TOPS BET. However, although in general MISTRAM II performed well on this flight compared to previous flights; its measurements could not be considered accurate enough to be used without benefit of measurements from other systems. For example, the P channel exhibited a large (approximately -6 foot) time varying bias, the source of which is unknown at present. Its character seemed to reflect both refraction and survey errors; however, a detailed analysis was not performed since it was not needed for the IMU analysis on this flight. The MISTRAM II Q channel also exhibited a refraction error of the same type as that found for MISTRAM I. The matnitude of this error was in the range of 5 to 10 n-units.

4.3 RANGE BET

Figures 24 and 25 show comparisons between compensated IGS and the AFETR Best Estimate of Trajectory (BET). This BET combined the measurements from MISTRAM I, 10K and 100K, MISTRAM II, GLOTRAC, GE Mod III, and C-band FPQ-6 radars Numbers 19.18 (Merritt Island), 3.18 (GBI), 7.18 (Grand Turk Island). The program is a conventional least squares adjustment in which a constant bias error model for each observation is specified. The problems of this model are exemplified by the comparisons of Figures 18 and 24, in which the BET shows remarkable agreement with the MISTRAM results, particularly in the x and z coordinates. This arises primarily because the MISTRAM data was heavily weighted in the adjustment, and because the program did not account for a refraction error. Furthermore, the estimate of MISTRAM 100K P bias was in gross error (by about 1 foot), thereby causing the BET vertical velocity estimates to be in error by about 10 ft/sec at SECO. The reason for the erroneous P bias estimate is not clear, but possibly arises from incorrect weighting of the other measurements used in the adjustment.

3150-6024-R8-000

Page 35

4.4 TOPS BET

Figures 26 and 27 show comparisons between compensated IGS data and the TRW TOPS (Trajectory Optimization System) BET program. The input to TOPS included MISTRAM I (R_{SUM}, P₁₀, Q₁₀, P₁₀₀, Q₁₀₀), MISTRAM II (R_{SUM}, P, Q), and GE Mod III (R, A, E, R, P, Q) data described previously. The IMU/TOPS comparisons show good agreement, and the differences noted are within estimated 1-sigma limits. Since the TOPS BET was derived without the use of IMU measurements, these results serve to verify the conclusions reached in Section 2.2 of this report.





Figure 13. Thrust Velocity Comparison in Computer Coordinates





with IMU Errors Compensated





Figure 15. GE/Burroughs Thrust Position Comparison with IMU Errors Compensated





with IMU Errors Compensated







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Figure 22. MISTRAM II Passive Thrust Velocity Comparison with IMU Errors Compensated











Figure 25. Range BET Thrust Position Comparison with IMU Errors Compensated

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3150-6024-R8-000

Page 50



Figure 27. TOPS BET Thrust Position Comparison with IMU Errors Compensated



5. TRAJECTORY RECONSTRUCTION

This section provides a description of the trajectory reconstruction for the ascent and reentry flight phases presented in Tables A-1 and A-2 in Appendix A. The data are provided in an ECIG coordinate system with the origin at the center of the earth. The z axis is the North Polar, and the x-y plane is the equatorial plane with the x-z plane containing the Greenwich Meridian at Go-Inertial time. Trajectory parameters such as velocity magnitude, altitude, flight path angle, heading, latitude, and longitude are also presented.

The ascent reconstruction consists of corrected guidance data. Corrections applied to the ascent data were the IMU error source magnitudes presented in Table 3 in Section 3.

The reentry trajectory reconstruction was obtained by making use of the TOPS BET program. The BET was derived from four ETR tracking radars, the coverage of which was as follows:

Radar	Data Spans (In sec from retrofire)
0:18 (Patrick AFB)	1545-1740
19:18 (Merritt Island)	1537-1707
3:18 (GBI)	1548-1751
7:18 (GTI)	1710-1943
TOPS BET	1551 -1745

The TOPS program requires overlapping coverage of at least two radars therefore the BET presented terminates at 1751 seconds.

Listings of the BET, uncorrected Grand Turk (7:18) and reconstructed IGS reentry trajectories and their associated trajectory parameters are presented in Appendix A. The IGS reentry trajectory is uncorrected since no conclusive IMU error analysis for the reentry flight phase was possible.

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3150-6024-R8-000 Page A-1

APPENDIX A

TRAJECTORY PARAMETER LISTINGS AND PLOTS

PLOTS

Figure		Page
A - 1	Computed Thrust Velocity in Computer Coordinates (Thrust Tailoff)	A - 3
A-2	Inertial Flight Path Angle (Ascent)	A-4
A - 3	Computed Thrust Acceleration in Computer Coordinates	A-5
A - 4	Revision 1 Booster Chase Maneuver IGS Sensed Velocity Increments	A-6

LISTINGS

Table		Page
A-1a	Reconstructed Ascent Trajectory	A-7
A-1b	Reconstructed Ascent Trajectory Associated Parameters	A-13
A-2a	Reconstructed Reentry Trajectory and Associated Parameters (BET)	A-19
A-2b	Reconstructed Reentry Trajectory and Associated Parameters (7:18 Radar)	A - 35
A-2c	Reconstructed Reentry Trajectory and Associated Parameters (IGS)	A-53
A-3	PCM Edit Listing for the Ascent Flight Phase	A-61

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Figure A-2. Inertial Flight Path Angle

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Table A-1a. Reconstructed Ascent Trajectory

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GEMINI TRAJECTORY IN ECIG

TIME IN SECONDS FROM LIFTOFF

TIME	×	۶	7	X-D0T	Y-D0T	Z-D0T
1.370	3026412	-18152080	9927856	1325.237	210-146	5.703
3.707	3029512	-18151609	9927880	1327.770	192.533	14-892
6-044	3032618	-18151181	9327926	1330.591	173.774	24-622
8.381	3035731	-18150798	965766	1333.278	154.001	34.845
10.718	3038850	-18150462	9928089	1336.491	133.403	45.496
13.053	3041975	-18150176	9928209	1339.815	111.560	56.700
15.828	3045790	-18149904	9928385	1344.233	84.305	70.619
18.165	3048845	-18149734	9928564	1347.882	60.805	82.972
20.510	3052011	-18149621	9928775	1352.452	35.727	96.451
22.991	3055373	-18149566	9929032	1357.499	8.092	111.583
25.437	3058700	-18149581	9929325	1363.979	-20.173	127.575
27.304	3061253	-18149639	9929575	1371.052	-41.854	140.279
29.747	3064618	-18149776	040266	1384.101	-70.886	158.669
32.194	3068025	-18149986	9930351	1401.410	-100.080	177.520
34.638	3071475	-18150266	9930809	1423.100	-129.477	197.662
37.085	3074988	-18150619	9931319	1448.321	-159.179	218.850
39.528	3078562	-18151044	0881666	1478.177	-189.091	240.829
41.973	3082217	-18151544	9932497	1512.467	-219.461	264.129
44.416	3085958	-18152117	9933171	1550.682	-250.046	287.395
46.861	3089800	-18152767	99339 0 3	1592.688	-281.016	312.252
49.310	3093755	-18153492	99347 0 9	1638.542	-311.695	338.589
51.778	3097861	-18154301	9935570	1688.687	-343.480	366.104
54.224	3102057	-18155179	9936499	1743.919	-374.476	393.659
56.093	3105359	-18155900	9937254	1790.092	-397.358	414.905
58.538	3109815	-18156908	9938304	1855.147	-426.992	443.471
60.986	3114441	-18157989	9939624	1924.044	-456.197	472.325
63.449	3119269	-18159148	9940626	1997.769	-484.250	503.777
65.929	3124319	-18160381	9941913	2077.030	-510.171	534.680
68.394	3129543	-18161668	9943271	2161.657	-533.603	567.833
70.886	313504N	-18163024	9944731	2250.929	-554.165	604.453
73.376	3140762	-18164428	9946285	2345.872	-573.275	642.585
75.277	3145295	-18165532	9947533	2422.870	-587.438	670.273
77.746	3151407	-18167004	9949230	2529.563	-604.327	704.362
8 0. 243	3157866	-18168531	9951033	2644.483	-619.704	739.148

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2112.358 2188.819 525.060 564.535 783.860 971.804 Z-D0T 253.515 428.828 475.760 616.915 669-810 906.580 249 • 646 2270.144 841.947 878.365 915.848 957.302 989.4**0**2 117.450 207.603 289.067 336.217 382.653 725.812 797.040 2284.397 2257.454 171.024 803.901 030.981 162.122 843.921 073.721 -715.703 -775.746 -774.435 -769.063 -745.876 -734.389 -724.028 -705-564 -684.698 -646.394 -615.186 -597.610 -552.784 -693.214 -737.239 -749.456 -759.832 -767.716 -775.627 -695.862 -672.927 -631.654 -578.144 -516.968 -459.059 -637.567 -658.951 -710.768 -726.794 -773.007 -676.775 -759.041 -660.101 -562.11] Y-D0T TIME IN SECONDS FROM LIFTOFF 4418.206 4775.014 4989.108 5212.350 5445.823 7234.437 9605.816 3008.086 3141.215 3279.139 3424.436 3867.140 4042.319 4227.332 4617.400 5684.440 5930.189 6126.651 6388.968 6659.747 6941.470 7539.547 859.059 8191.657 8543.405 8907.930 9296.119 9782.776 2880.974 3541.407 3699.234 2761.251 9804.681 9893.391 X-00T 0012829 0030325 9963468 9978999 0001950 0004893 0008805 0016984 0025720 0045115 0054670 0065863 9954809 9958959 9961153 9967805 9970436 9976044 9982069 9984492 9987770 9294626 0021281 0035070 0040034 0050453 0057067 0060312 9952885 9956847 1716799 9991161 9998261 9965321 2 -18198509 -18205248 -18216660 -18179883 -18183598 -18185505 -18187448 -18189380 -18191315 -18192793 -18196628 -18200336 -18202130 -18206965 -18208654 -18210317 -18211948 -18213553-18223236 -18171658 8173312 -18174993 -18203501 -18215117 -18218145 -18219604 -18220688 -18221277 -18222039 -18170072 -18176711 -18178489-18181711 -18194721 7 3237225 3247650 3258429 3269696 3290836 3303556 3316882 3330619 3344898 3356383 3371769 3387746 3404387 3421744 3458727 3543008 571215 3186228 208998 3217899 3227356 3278647 3439820 3478364 3499067 3520417 3560967 3585173 3609324 3171393 3164496 3194084 3202367 3178681 × 21.259 57.036 92.520 01.855 09.366 11.860 .13.767 16.264 18.758 23.728 26.187 33.000 35-447 37.897 55.609 90.072 96.896 06.872 28.092 30.551 40 - 344 42.800 45.247 47.722 50.169 54.552 59.488 82.696 85.142 87.617 94.991 99.355 04.351 52.651 TIME

Reconstructed Ascent Trajectory - Continued GEMINI TRAJECTURY IN ECIG Table A-1a.
Continued
Trajectory —
Ascent
Reconstructed
Table A-1a.

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GEMINI TRAJECTORY IN ECIG

TIME IN SECONDS FROM LIFTOFF

2-001	2244.793 2232.400 2232.400 2220.949 22199.417 2199.417 2199.417 2199.417 2139.500 2139.500 2108.729 2108.729 2108.729	2062.968 2047.814 2015.789 2016.789 2001.047 1985.464 1937.563 1937.563 1921.057 1921.057 1921.653 1935.1575 1887.710 1887.710 1887.710 1853.615 1853.6157 1860.575 1764.4627 1764.4627 1764.4627 1764.4627 1764.4627 1764.4627 1764.4627 1764.4627 1764.4627 1764.4627 1764.4627 1764.4627 1764.4627 1764.4627 1764.4627 1764.4627 1764.4777 1764.4627 1764.4777 1764.4777 1764.4777 1764.4777 1764.4777 1764.4777 1764.4777 1764.4777 1764.4777 1764.4777 1764.4777 1764.4777 1764.4777 1764.4777 1764.4777 1764.4777 1764.47777 1764.47777 1764.47777 1764.477777 1764.4777777 1764.47777777777777777777777777777777777
Y-D0T	-400.505 -341.814 -286.391 -286.391 -236.059 -176.719 -111.403 -42.531 27.240 98.090 169.653 242.810 316.768 391.467	467.241 544.494 622.396 622.396 622.396 653.593 863.593 945.778 10.29.778 10.29.778 10.29.778 12.010 12.01 1
X-00T	9984.752 10078.165 10167.774 10167.774 10167.774 10250.806 10348.483 10348.483 1054.9.538 1054.9.538 1055.751 10552.751 10552.751 10652.751 10652.751 1080.262 11191.043	11303.291 11649.725 11649.725 11649.725 11669.892 12011.711 12136.041 12261.918 12261.918 122651.6445 122651.6445 122651.6445 122651.6445 122651.6445 122651.6445 122651.645 12289.845 12280.087 13680.087 13691.696
Z	10071392 10076873 10082028 10082028 10082028 10097331 10107844 10113054 10118215 10118215 10128426 10128426 10133471	10138482 10143456 10143456 10153296 10153296 10172526 10172526 10172538 10181907 10186533 10195682 10209688 102096653 1022138653 10222105 10222105 10222105 102222055252
۶	-18224291 -18225200 -18225927 -18225927 -18226476 -18225927 -18227332 -182273380 -18227380 -18227380 -1822557 -182255800 -182256557 -182255800	-18223985 -18223985 -18223461 -1821349 -1821349 -182137946 -182137946 -182137946 -182137946 -18205980 -18195980 -18195735 -18182539 -1818650 -1818650 -18165874 -18165874
×	3633734 3658293 3658293 3658293 3703167 3778731 3778731 3778731 3873284 3873284 3882984 3882984 3882984 39395665 39395665	5963818 3991309 4019099 4019099 41047148 41047148 4104586 4104189 4104189 41047148 4104788 413132 4221685 43375216 43375736 453132267 453132267 453132267 453132267 45313266 4531266
T [ME	161.944 161.944 164.393 166.708 168.808 178.650 176.074 176.074 178.495 183.343 185.765 188.185 185.185	193.024 195.443 195.443 202.712 202.712 207.551 207.551 207.551 207.551 207.551 207.551 217.232 222.245 218 222.252 218 222.252 218 222.252 218 222.252 218 222.252 218 222 222.252 218 222 222 222 222 222 222 222 222 22

			TIME IN SECON	IDS FROM LIFTOFF		
TIME	×	۶	7	X-00T	Y-D0T	Z-D0T
243.148	4595494	-18156755	10233475	14048.234	2394.234	1714.124
245.593	4630041	-18150993	10237643	14207.560	2408.767	1694.498
248.041	4665022	-18144966	10241767	14369.581	2515.435	1674.705
250.487	4700375	-18138679	10245840	14534.191	2624.347	1654.665
252.936	4736163	-18132119	10249865	14702.352	2735.499	1633.859
255.381	4772324	-18125292	10253835	14873.498	2848.217	1612.916
257.829	4808951	-18118178	10257758	15048.762	2963.593	1591.522
260.276	4845994	-18110783	10261626	15225.752	3 380.997	1569.887
262.732	4.883597	-18103071	1n265453	15408.007	32n1.209	1547.591
265.178	4921516	-18035091	1n269212	15593.332	3323.310	1525.111
267.628	4959953	-18386797	10272923	15782.691	3447.862	1502.148
270.074	4998798	-18078207	10276567	15976.034	3575.010	1479.064
272.521	5038121	-18969304	10280156	16173.446	3704.599	1455.289
274.968	5n77947	-1806-0076	10283688	16375.159	3837.235	1430.999
277.416	5118290	-18050516	10287161	16582.177	3972.891	1406.215
279.089	5146150	-18043791	10289499	16725.966	4067.175	1389.031
281.545	5187493	-18-33629	10292879	16941.465	4208.912	1362.767
283.992	5229221	-18023152	10296181	17161.452	4353.760	1336.228
286.442	5271546	-18012303	10299421	17357.312	4562 . 960	1308.499
288.844	5313570	-18001310	10302530	17614.331	4652 . 680	1280.731
291.161	5354647	-17993357	10305467	17838.273	4870.777	1253.3333
294.207	5409441	-17975431	10309229	18142.339	5000.920	1216.617
296.525	5451759	-17963662	10312015	18380.768	5157.038	1188.211
298.842	5494637	-17951527	10314735	18625.906	5316.967	1159.552
301.166	5538220	-17938978	10317396	18378.958	5481.686	1129.949
3 n 3.486	5582325	-17926063	10319983	19138.650	5651.337	1099.273
305.805	5627004	-17912760	10322494	19405.945	5826.094	1967.421
308.123	5672311	-17899n45	1r324932	19681.148	6006 . 998	1034.823
310.440	5718228	-17884915	10327293	19965.260	6193.430	1001-006
312.766	5765011	-17870285	10329578	20259.786	6386.239	966.316
315.816	5827409	-17859411	10332453	20662.112	6649.002	918.916
318.135	5875697	-17834749	19334542	20979.965	5857 . 441	881.547
320.453	5924717	-17818602	10336541	21310.752	7573.481	842.739
322.780	5974706	-17801881	10338455	21654.386	7298.648	8n2 . 374

Table A-la. Reconstructed Ascent Trajectory - Continued

GEMINI TRAJECTORY IN ECIG

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Continued
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Trajectory
Ascent
Reconstructed
Table A-fa.

GEMINI TRAJECTORY IN ECIG

TIME IN SECONDS FROM LIFTOFF

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	×	>	7	X-00T	Y-00T	Z-DOT
	25384	-17784669	10340270	22011.580	7532.151	760.777
~	6866	-17766921	10341985	22384.400	7773.852	718.288
	29186	-17748618	10343600	22773.812	8023.793	675.101
~	32613	-17729661	10345118	23183.703	8284.137	630.845
	36854	-17710143	10346528	23612.637	8555.509	585.108
-	98829	-17687511	1 r 347978	24116.111	8872.037	532.376
-	99 9 50	-17687099	10348003	24125.980	8881•605	530.193
-	568 <u>0</u> 7	-17662365	10349411	24157.609	8978.927	487.700
	15629	-17644161	10350367	24144.361	9032-050	457.937
-	67155	-17624820	10351311	24129.743	9Å87.686	426.381
12	18198	-17605531	10352180	24111.645	9141.719	395.211
	92987	-17577038	10353336	24084.042	9220.274	349.299
-	44215	-17557360	1 n354n45	24064.596	9273.991	317.668
~	95472	-17537541	10354689	24344.643	9327.703	286.267
1.7	71339	-17507967	10355518	24914.513	9406 . 698	239.254
_	17099	-17489990	10355947	23995.979	9454.212	211.09n
	32677	-17464044	10356479	23969.537	9522.906	170.672
<u> </u>	32234	-17444295	10356791	23949.294	9574.044	139.742
<u>.</u> .	97613	-17418051	10357117	23921.999	9642.249	99.279
1	47047	-17398963	10357291	23901.554	9693.811	68.761
	12439	-17371434	10357423	23876.414	9762.695	27.868
-	51826	-17351178	10357449	23855.266	9814.404	-2.765
	26831	-17324327	1n357386	23827.275	9881.84 0	-43°090
<u> </u>	19718	-17302321	10357254	23804.327	9936.663	-76.026
(* F	10720	-1728J965	10357057	23791.985	9989 .69 6	-107.651
5	95780	-17253528	10356707	23753.176	13956.963	-148.444
4	4817	-172327 n 3	1 7356368	23731.135	10107.876	-179.194
0	19621	-17204993	10355824	23772.179	10175.022	-219.573
u۳۱ –	18646	-17183885	10355337	23679.970	17225.878	-250.439
n i	3448	-17155791	10354596	23650.211	10293.000	-290.979

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Table A-1b. Reconstructed Ascent Trajectory Associated Parameters

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	GEM	INI 7 RECONSTRU	CTED ASCENT TRI	AJEC TORY			
TIME FROM LIFTOFF (SECONDS)	INERTIAL VEL. MAGNITUDE {FT/SEC}	RELATIVE VEL. Pagnitude (FT/SEC)	INERTIAL FLT. Path angle (degrees)	INERTIAL HEAUING ANGLE (DEGREES)	ALTITUDE (FEET)	GENDETIC LAT. (DEGREES)	GENDETIC LONG. 1 DEGREESI
1.370	1341.8	12.4	. 528	90.002	-2.0	28.507	-80.555
3.707	1341.8	32.6	1.392	90.072	50.5	28.507	-80.555
6.044	1342.1	54.1	2.310	90.045	151.5	28.507	-80.555
8.381	1342.6	76.7	3.275	90.070	304.0	28.507	-80.555
10.718	1343.9	100.4	4.281	260.09	510.5	28.507	-80.555
13.053	1345.7	125.3	5.342	90.129	773.5	28.507	-80.555
15.828	1348.8	156.5	6.660	90.171	1164.5	28.507	-80.555
18.165	1351.9	183.5	1.798	90°144	1561.0	28.507	-80.555
20.510	1356.4	212.5	9.011	90.208	2025.0	28.507	-80.555
22.991	1362.2	244.6	10.344	90.214	2591.7	28.507	-80.555
25.437	1370.2	277.9	11.700	90.205	3230.0	28.507	-80.555
27.304	1379.0	304.0	12.732	90.189	3773.0	28.507	-80.555
29.747	1395.1	340.1	14.104	90.125	4559.5	28-507	-80.555
32.194	1416.3	7.775	15.437	90.064	5436.5	28.507	-80.555
34.638	1442.7	417.3	16.737	89.975	6404.5	28.507	-80.555
37.085	1473.6	459.1	17.995	89.869	7469.5	28.507	-80.554
39.528	1509.8	503.2	19.190	89.757	8631.7	28.507	-80.554
41.973	1551.2	550.5	20.332	89.627	9896.5	28.507	-80.553
44.416	1597.0	600.2	21.389	89.520	11266.5	28.507	-80.552
46.861	1647.4	653.2	22-392	89.386	12746.0	28.507	-80.551
49.310	1702.2	109.1	23.316	89.218	14338.5	28.507	-80.549
51.778	1762.0	769.3	24.194	89.055	16061.2	28.507	- 80.547
54.224	1826.9	832.3	24.948	88.905	17886.5	26.506	- 80.545
56.093	1890.3	882.7	25.436	B8.792	19361.7	28.509	-80.543
58.538	1954.9	952.3	25.996	R8 • 6 4 2	21397.0	28.508	- 80. 540
60.986	2033.3	1025.0	26.477	88.501	23555.5	28.508	-80.537
63•449	2116.8	1102.2	26.884	88.300	25851.5	28.509	-80.533
65.929	2204.9	1182.4	27.162	88.117	28286.2	28.509	-80.528

Continued
ociated Parameters
Trajectory Ass
econstructed Ascent
Table A-1b. R

GEMINI 7 RECONSTRUCTED ASCENT TRAJECTORY

TIME FROM LIFTOFF (Seconds)	INERTIAL VFL. Magnitude (FT/SEC)	RELATIVE VEL. Magnitude {FT/SEC}	INERTIAL FLT. Path Angle (degrees)	INERTIAL Heading Angle (degrees)	ALTITUDE (FEET)	GEODETIC LAT. (DEGREFS)	GENDETIC LONG. (DEGREES)
68.394	1,98,22	1266.8	27.34H	87.879	3042H-7	28.510	-80.523
70.886	2396.0	1355.5	27.459	87.556	33521.2	28.510	-80.518
73.376	2499.3	1449.4	27.507	я7 . 226	36135.0	28.511	-80.511
15.277	2581.9	1524.3	27.488	87.034	38566.0	28.511	-80.506
77.746	2694.8	1626.2	27.378	86 . 849	41568.2	28.512	-80.498
80.243	2815.3	1735.3	27.206	86.675	44723.0	28.513	-80.490
82.696	2937.3	1847.3	27.057	86.604	47940.2	28.514	-80.441
85.142	3063.1	1964.9	26.970	R6.564	51273.5	28.515	-80.471
87.617	3196.5	2090.0	26.833	86.426	54780.5	28.516	-80.460
90.072	3334.9	2219.7	26.646	A6.332	5,388.5	28.518	-80.448
92.520	3478.4	2355.4	26.475	R6.253	62116.7	28.519	-80.435
166°76	3629.6	2499.1	26.291	86.127	66022.0	29.520	-80.421
96.896	3750.6	2614.1	26.113	86.034	69125.7	28.522	-80.409
99.355	3913.0	2768.B	25.859	85.930	73255.2	28.523	-80.393
101.855	4085.1	2933.1	25.572	85.831	71594.7	28.525	-80.376
104.351	4264.0	3104.3	25.261	85.730	82068.2	29.527	-80.357
106.872	4452.2	3284.7	24.919	85.633	86 129.7	28.529	-80.337
109.366	4645.9	3470.9	24.564	85.533	91479.7	28.531	-80.315
111.860	4847.4	3665.0	24.192	85.442	96367.7	28.533	- 80.292
113.767	5006.6	3818.8	23.902	95 . 376	100196.5	28.535	-80.274
116.264	5222.3	4027.3	23.500	85.288	105332.7	28.538	-80.248
118.758	5446.2	4244.0	23.065	95.210	110594.0	28.541	-80.221
121.259	5679.7	4470.4	22-615	85.148	115995.2	28.544	-80.192
123.728	5919.0	4703.4	22.217	85.102	121455.5	28.547	-80.161
126.187	6166.2	4945.0	21.848	85.059	127031.2	28.550	-80.129
128.092	6364.0	5138.9	21.580	R5.028	131449.2	28.553	-80.103
130.551	6628.5	5398.3	21.255	84.998	137284.2	28.556	-80.067
133.000	6901 . 5	5666.8	20.952	84 . 984	143252.5	28.560	-80.030

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able A-1b. Reconstructed Ascent Trajectory Associated Parameters	Continued
Cable A-1b. Reconstructed Ascent Trajectory Associated Parameters	
Table A-1b. Reconstructed Ascent Trajectory	Associated Parameters
Table A-1b. Reconstructed Ascent	Trajectory
Table A-1b. Reconstructed	Ascent '
Table A-1b.	Reconstructed
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	6EM	VINI 7 RECONSTRU	CTED ASCENT IR	AJECTORY			
TIME FROM LIFTOFF (SECONDS)	INERTIAL VEL. MAGNITUDE (FT/SEC)	RELATIVE VEL. Magnitude (ft/sec)	INERTIAL FLT. Path angle (degrees)	INERTIAL Heautng angle (degrees)	ALTITURE {FEET}	GEODETIC LAT. (DEGREES)	GEODETIC LUNG. (DEGREES)
777 JEI	7195 0	5 947.0	20-660	84.961	0.875941	28.564	- 79. 990
108 121	8 187L	0.0554	20.382	84.942	155677.2	28.56R	- 79.949
772 071	7790.2	6543.5	20.113	R4.926	162147.2	28.572	- 79. 905
	8113.2	6863-0	19.855	84.914	168825.0	28.576	- 79. 859
145.747	8449.7	7196-1	19.609	84.903	175671.0	28.581	-79.810
147 722	8805.7	7548.8	19.368	84.892	182797.0	28.586	- 79. 759
150 160	0174-0	7914-9	19.140	84.8R2	190055.7	28.591	- 79 - 705
152 451	05,68,7	8-015 4	18.917	84.871	197644.0	28-596	-79.648
154-557	CAR2.1	8617-1	18.752	84.864	203614.2	28.601	-79.602
	10061	8795.3	18.663	84.860	206997.7	28.603	-79.576
157 026	F 1001	RRO9.1	18.465	84.882	211569.2	28.606	-79.540
150.488	10158-0	886.4	18.134	84.923	219364.5	28.612	- 79.478
161-944	10741-8	8966.8	17.804	84.965	227098.7	28.618	-79.415
FPF. 441	1.978.01	9049.9	17.481	85.007	234735.2	28.623	-79.351
166.708	10411-4	9130.3	17.181	85.048	241892.5	28.629	-79.291
168.8C.8	10489-2	9205.5	16.915	85.083	248330.0	28.634	-79.235
171.730	10581-0	9744.4	16.606	85.126	255694.5	28.639	-79.170
173.450	10674-8	9385-0	16.269	85.166	262991.2	28.645	-79.105
176-074	10770.4	9477-5	15.919	85.207	270191.5	28.651	-79-038
178.495	10869-4	9572.5	15.571	85.247	277304.5	28.656	-78.971
180.027	10968.4	9669-5	15.227	85.285	284345.7	28.662	-78.903
183.343	5 0 2 0 1 1	9768.7	14.887	85.325	291281.7	28.668	-78.834
185.745	11174.5	9869-9	14.547	85.362	298130.5	28.674	-78.764
188_185	11280.6	9973. 3	14.212	85 . 398	304883.5	28.679	-78.694
190.604	0.1389-0	10079-1	13.882	85.435	311544.2	28.685	-78.622
192 076	4.00411	10186.9	13.554	85.472	318117.2	28.691	-78.550
105-443	11617-1	10297.2	13.228	85.506	324598.7	29.697	-78.477
197.865	11726.7	10409.3	12.908	85.547	330994.1	28.702	- 78.403

Table A-1b. Reconstructed Ascent Trajectory Associated Farameters -- Continued

GEMINI 7 RECONSTRUCTED ASCENT TRAJECTORY

TIME ROM LIFTOFF (SECONDS)	INERTIAL VEL. Magnitude (ft/sec)	RELATIVE VEL. Magnitude (FT/SEC)	INERTIAL FLT. Patm angle (degrees)	INERTIAL HEADING ANGLE (DEGREES)	ALTITUDE (FEET)	GENDETIC LAT. (DEGREES)	GEODETIC LONG. I DEGREES)
200. 285	11843.7	10524.0	12-589	85.578	337293.5	28-708	-78.378
202.712	11963.3	10641.4	12.272	85.614	343517.0	28.714	-78.251
205.132	12084.8	10760.7	11.962	85.650	349630-7	28.720	-78-175
207.551	12208.6	10882.5	11.656	85.687	355649.2	28.726	-78.097
209.971	12335.2	11007.0	11.351	85.723	361577.2	26.732	-78.018
212.393	12463.8	11133.7	11.051	85. 9	367416.2	28.738	-77-938
214.813	12595.1	11263.1	10.753	85.	373156.5	28.744	-77-857
217.232	12728.7	11394.9	10.460	95. b	378800.0	28.750	-77.775
219.651	12865.2	11529.6	10.169	85.874	384350.2	28.756	-77.692
222.078	13004.4	11667.1	9.882	85.913	389820.0	28.762	-77-608
224.498	13146.2	11607.3	9.600	85.952	395179.7	28.767	-77-522
226.918	13290.8	11950.3	9.320	85.992	400443.0	28.773	-77-436
229.338	13438.2	12096.2	9*0*6	86.033	405610-0	28.779	-17.349
231.761	13588.8	12245.4	8.777	86.075	410697.7	28.785	-77.260
234.186	13742.6	12397.8	8.510	86.118	415673.5	28.791	-77.170
236.610	13899.7	12553.5	8.249	86.162	420563.5	28.797	- 77.079
239.035	14059.5	12712.0	166-7	86.207	425356.5	28.804	-76.987
240.657	14171.0	12822.7	7.816	86.237	428587.0	28.808	-76.923
243.148	14338.5	12989.0	7.562	86.292	433266.5	28.814	-76.827
245.593	14509.3	13158.6	7.311	A6.330	437837.0	28.820	-76.731
248.041	14683.6	13331.8	7.063	86.377	442314.0	28.826	-76.633
250.487	14861.3	13508.5	6.818	86.424	446686.7	25.832	-76.533
252.936	15043.3	13689.4	6.574	86.472	450961.2	28.638	-76.433
255.381	15229.1	13874.2	6.336	86.521	455127.7	28-844	-76.331
257.829	15419.1	14063-3	660.9	86.571	459105.7	28.850	-76.227
260.276	15613.1	14256.4	5.866	86.621	463160.2	28.856	-76.122
262.732	15812.6	14455.0	5.635	86.672	467031.5	28.862	- 76.015
265.178	16015.9	14657.6	5.409	86.723	470784.0	28.868	-75.907

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Table A-1b. Reconstructed Ascent Trajectory Associated Farameters - Continued

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	CEM	HINE 7 RECONSTRU	CTED ASCENT TRI	AJEC TURY			
TIME From Liftoff	INERTIAL VEL. MAGNITUDE	RELATIVE VEL. MAGNITUDE	INERTIAL FLT. PATH ANGLE	INERTIAL HEADING ANGLE	ALTITUDE (FEET)	GFONETIC LAT. IDEGREES)	GEODETIC LONG. (DEGREES)
(SECONDS)	(FT/SEC)	(FT/SEC)	(DEGREES)	(DEGREES)			
267.628	16224.2	14865.1	5.187	86.776	474437.0	28.874	-75.798
270-074	16437.4	15077.5	4.969	86.829	477978.0	28.880	- 75. 696
272.521	16655.6	15295.0	4.753	86.883	481413.2	28.886	-75-574
274.968	16879-1	15517.8	4.540	86.938	484742.7	28.892	-75.459
277.416	17105.9	15747.0	4.330	86.993	487965.2	26.898	-75.343
279.089	17268-9	15 906.6	4.189	87.032	490105.0	28.902	- 75 - 262
281.545	17509-1	16146.2	3.982	R7.090	493153.7	28.905	-75.143
283.992	17755-0	16391.6	3.779	87.148	496079.5	28.914	-75.022
286.442	18009-1	16644.1	3.575	87.207	498895.0	28.419	- 74. 899
288.844	18262.6	16896.2	3.380	R7.266	501542.0	28.925	-74.776
291-161	18515-0	17150.1	3.193	87.324	503990.0	28.930	-74.656
294.207	19857-7	17492.3	2°953	87.401	507047.7	28.937	- 74. 496
296.525	19126.9	17761.1	2.776	87.461	509252.0	28.943	-74.371
298.842	19404-1	18037.9	2.603	87.521	511352.0	28.948	-74.245
301.166	15690-6	18324.1	2.432	87.582	513352.7	28.953	-74.116
303.486	19985.3	18618.5	2.262	87.645	515242.7	28.958	-73.986
305.805	20299-1	18922.1	2.093	87.709	517021.5	28+963	-73.853
308-123	20602 8	19235.6	1.925	87.772	518688.2	28.968	-73.718
310-440	20927-1	19559.6	1.758	87.638	520238.5	28.973	-73.592
312-766	21263.8	19896.1	1.595	87.904	521679.0	28.978	- 73 . 442
315.016	21724.3	20356.4	1.384	87 . 994	523388.5	28.985	- 73 . 255
318.135	22089.1	20721.0	1.224	88.062	524549.0	28.989	-73.109
320.453	22468.4	21100.1	1.066	88.132	525585.2	28.994	-72.962
322.780	22864.6	21496.2	6 06 °	68.203	526499.0	28-998	-72.811
325.102	23276.3	21907.8	. 755	88.276	527280.5	29.003	-72.657
327.421	23705.9	22337.3	. 606	84.349	527931.2	29.007	-72.500
329.738	24154.6	22785.9	. 464	9A.425	528452.5	29.011	-72.341
332.064	24626.5	23257.8	.329	88.502	528848.2	29.015	-72.178

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	GEM	ILNI 7 RECONSTRUC	CTED ASCENT TRI	AJEC TURY			
TIME FROM LIFTOFF (SECONDS)	INERTIAL VEL. Magnitude (FT/SEC)	RELATIVE VEL. Magnitude (FT/SEC)	INERTIAL FLT. Path angle (degrees)	INERTIAL HEADING ANGLE (DEGREES)	ALTITUDE (FEET)	GEODETIC LAT. (DFGREES)	GEDDETIC LONG. (DEGREES)
334.382	25120.7	23752.0	•196	88-581	529116-0	29-014	- 72 - M2
336.979	25700.9	24332.1	. 055	98.671	529261.2	54.023	-71-821
337.025	25713.6	24344 B	4 9 0 •	88.672	529262.2	29.024	- 71.918
339.794	25776.2	24407.4	• 032	88.776	529311.7	29.028	- 71 - 612
341.816	25781.8	24413.0	.033	A8.85 2	529344.7	29.031	-71.461
343.950	25786.2	24417.4	• 035	88.933	5293R0.0	29.034	- 71 - 302
346.066	25788.8	24420.0	. 037	89.014	524417.0	29.036	- 71 - 144
349.170	25790.3	24421.5	.039	89.132	529473.7	29.040	- 70-913
351.298	25791.0	24422.2	.041	89.213	529514.5	29.042	- 70. 755
353.429	25791.3	24422.5	- C+0-	89.293	529556.7	29-044	- 70. 596
356.586	25791.5	24422.7	• 046	89.414	529622.0	29.046	- 70.360
358.492	25791.3	24422.5	. 047	89.487	529663.2	29.047	-70.218
361.227	25791.7	24422.9	.049	89. 590	529724.2	29.049	-70.014
363.295	25791.7	24422. A	.052	89.670	529772.2	040.62	-69.860
366.026	25791.5	24422.7	. 054	R9.774	529838.2	29.051	-69.657
368.094	25791.8	24423.0	• 056	89.852	529889.7	29.051	-69.503
370.831	25794.4	24425.6	.058	89.957	529960.0	29.052	-69.299
372.900	25794.5	24425.6	. 059	90.036	530014.2	29,052	-69 - 144
375.627	25794.4	24425.5	• 062	90.140	530088.5	29.051	-68.941
377.848	25794.3	24425.5	• 064	90.224	530150.5	29.051	-68.775
166°61E	25794.3	24425.4	.066	90.306	530212.5	29.050	-68.616
382.729	25794.1	24425.2	. 068	90.410	530294.2	29.049	-68-412
384.794	25793.9	24425.0	.070	90.489	530357.0	29.048	-68.258
387.526	25794.0	24425.1	e10.	90.593	530443.2	29.046	-68.054
389.596	25794.0	24425.1	.074	90.672	530510.0	29.044	-67.900
392.334	25793.8	24424.9	.077	717.06	530600.7	29.042	-67.696

Table A-1b. Reconstructed Ascent Trajectory Associated Parameters - Continued



	TIVE	×	
	1551.660	4100255.500-16245833.250	0.
	1552.00	4125153.406-18241438.75	` ت
(1553.600	4150073.875-16237054.25	Э,
C	1554.600	4174556.812-18232652.256	0
:(1555. ເບິທ	4155871.000-182235.250	<u>.</u>
	1556.000	4224703.375-18223727.75	S.
	1557.600	4245544 675-18215237.00(Ó
J	1558.000	4274353.750-18214687.250	0
	1555.000	4255163.562-18210158.00	3
	1560.000	4323526.187-18205565.500	3
D	1561.000	4348680.375-162UL975.75	\mathbf{C}
	1562-000	4573446.312-16156355.75	3
EI	1563.000	4358154.259-18151652.50(\circ
N	1564.000	4422345.625-18187021.50	0
17	1565.000	4447534.537-18182352.75	0
	1566.644	4472168.562-18177c11.00	0
	1567.000	4456813.437-18172850.u0	C
4	1568.1.	4521411.6e7-18108112.250	Э
	1505.(4540,01.125-1816340.25(Э
	1576.01	457.577516156547.25	1
	1571.1 1	4599112.537-16153731.50	~ 7
	1572.iu	4615029.753-18146881.25	-
	1573.נונ	4044151.25,-18144039.75	0
	1574.404	4-1666 9.667-1813514C.5L	Ċ
	1575.600	4695066.437-18134260.00	2
	1576.60	4717478-527-18129322-50	Ċ

9653535.125

5836354.603 5646780.125

9843188.125 5835o04.125 5835579.125 5832338.50U 5828690.250 5625437.543 5821383.750 9817710.750 5814024.250 5813318.500 \$8.160012 • 750 5802869.75u 9795115.625 \$791552.375 5767c17c375 5784036.375

967851U.625 5675012.125 5E71547.5UÜ

5668034.753 5664546.250 5861003.000 5 557487.253

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-3417.718 -3358.619 Z-D01 -3385.530 -3473.559 -3636.679 -3682.184 -3738.700 -3725.952 -3468.256 -3402.687 -3516.740 -3528.455 -3545.135 -3544.677 -3530.668 -3589.689 -3611.957 -3643.517 -3675.617 -3688.552 -3722.703 -3757.106 -3805.016 -3778.217 -3592.667 -3623.200 -3646.337 -3672.511 -3488-441 -3623.252 100-Y 4481.579 4530.978 4553-018 4591-007 4388.543 4893.180 4437.976 4470-549 4612-809 4646.017 4646.596 4696.292 4686.453 4772.493 4764.165 4790.294 4840.235 4942.039 4922.750 4587.016 5023.399 383.644 4324.301 4562.890 4714.132 4782.708 4824.766 4861.266 4900.042 5009-804 X-DCT 24951.552 24511.335 24887.552 24856.125 24793.026 24739.664 24730.585 24712.176 24676.959 24653.614 24601.809 24581.282 24570.445 24537.568 24394.136 24354.801 24921.710 24816.728 24761.294 24672.482 24593.548 24529.200 24512.539 24453.264 24341.743 24296.067 24295.325 24792.701 24858.u41 24443.727

Table A-2a. Reconstructed Reentry Trajectory and Associated Parameters (BET)

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3150-6024-R8-000 Page A-19

-3811.744

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5035.812 5055.815

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24265.767 24249.487 24222.267

> 578C236.75U 5776420**.**500

9795346.875

4741272.612-18124381.250 4166247.437-18119423.250 4/90565.187-18114445.000 4614852.750-18105436.250 4835182.1 Cu-16104421.500 4863435 \$500-18055385,750 4 cê 7001 • 687-18054348 • 000

577.000 578.000 575.000 58L.CC 581.500 1582.Cüu 1583.100

Table A-2a.	Reconstructed Reentry Tra	ijectory and Ase	sociated Param	eters (BET) -	- Continued
1584.664	4311861.753-186236.750	67726U1.0cu	24191.722	597ċ•ú8¢	-3826.043
1585.000	4536uc2.937-18084189.250	976£771.375	24177.461	5087.054	-J044.218
1586.600	4960221.062-18075087.000	9764931.375	24139.341	5105.261	-3846.326
1587.000	45 64536-457-16073562-500	5751C82.625	24100.889	5131.331	-3864.101
1568.CLC	5u06431.437-16066823.500	5757218.25U	24u80.698	5151.296	-3871.040
1585.000	5032566.754-16063671.250	9753340.625	24055.284	5160.560	-3877.577
1550.000	5056559.125-18058906.250	9745456 . 0u0	24042.477	5176.538	-3879.940
1551.LOG	5660586.937-16453321.040	6745575.753	24035.110	5187.470	-3890.740
1552.666	5104586.187-18348117.750	9741673.125	23588.793	5231.355	-3500.332
1553.じじひ	5126553.437-16442687.000	3737853.37579	23943.900	5254.800	-3524.665
1594.600	5152517.500-16037643.250	5733925.750	23957.463	5230.311	-3825.974
1555.666	5176352.875-16622313.500	5725858 . 25U	23875.090	5295.845	-3552.253
1556.CUC	5248231.625-18827C5C.CuC	5725554.125	23618.531	5328.515	-3964.750
1557.000	524665.250-18021724.500	5722012 • 5ul	23807.333	5341.902	-3446.340
1558.000	5247661.062-18016370.750	5716061-000	23761.866	5336.041	-3964.814
1559.000	5<71554.212-16J11C23.5UU	5714082.750	23804.038	5390.664	-3937.936
1600.000	5295363.875-18005631.500	9710142.375	23732.966	5398.070	-3967.626

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	5843.310 -4064.476	5873.554 -4031.447	5895.316 -4049.319	5931)•586 -4058•006	5854.077 -4058.994	5954.178 -4042.687	5912.881 -4058.755	5989.344 -4078.215	5948.714 -4101.743	59()9.544 -4104.887	5967.755 -4109.950	59:11.853 -4090.808	5951.266 -4074.592	5998.243 -4075.974	5945.167 -4091.198	5999.416 -4133.064	5895.326 -4098.531
iociated Paramet	22145.582	22116-744	22052 • 644	21989.555	21938.259	21893.572	21833.620	21762.210	21690.315	21630.261	21575.947	ž1525.115	21462.191	21419.931	21245.137	21273.437	21222.685
actor y and Ass	9573516.125	5565462.250	9565426.750	9561372.125	9557305.750	5553234.375	9545175.000	4545105.75U	5541026.125	453c942.125	9532827.025	5526742.125	9524678.375	9520553.125	9516465.750	9512356.125	9508268-000
Reconstitucied meaning and	6076215.875-17813665.250	6. 5 8 3 4 5 . 8 7 5 - 1 7 6 0 7 7 6 6 • 7 5 0	6120427.562-17801501.750	£142452.812-17796626.750	6164414.937-17790134.750	6166323.687-17784171.500	6206164.167-17778232.250	6225975.667-17772354.750	6251658.525-1776c470.000	4273363.375-17760407.030	6254553.625-17754430.750	6316547.437-17746571.500	6338041.687-177427C3.500	6459477-875-17736729-250	E386838.625-17736825.560	402144-937-17724868.75U	6423404.562-177185c9.5JU
Table to -ta	1 434-000	1635,000	1636.000	1637.004	1638.600	1635-400	1640.000	1641-000	1642_000	1643-050		1645-000	1646-30.0	1647.600	164H - 114 C	1645-000	1650.000

3150-6024-R8-000 Page A-22

Table A-2a.	Reconstructed Reentry	Trajectory and A	ssociated Farar	neters (BET)	- Continued
		GEMINI GUICANCE Nasa • Manned Sp	ANALYSIS PROGR	۲ ۲	C1/C8/66
		ECI (GUICANCE TI	(G CCURDINATES Ime ease)		
TIME	×	7	x-201	Y-D0T	Z-001
le51.Cú	6444573.062-17712829.5	0 9504132.375	21142.740	5929.876	-4129.435
1652.030	6465710.500-17707119.2	50 951 LIU7.125	2u990.476	6574.462	-4428.904
1653.LUU	e466718.537-17700910.2	50 9455832.375	21027.520	5873.552	-4027.847
1654.000	65U7658.125-17694878.2	0 9491724.750	21906.282	5759.919	-4043.215
1055.662	6528046.125-17689121-0	JU 9467728.500	26453.543	5838 . 945	-4078-096
1650.00%	c545495.750-17683162.0	00 5483612.125	2u816.U38	6067.690	-4132.698
1657.540	6570278.c67-17677180.C	0 9475484.375	24763.585	5809.366	-4077.254
1658.600	¢590577.125-17671116.5	JC 5475331.750	20664.530	6102.850	-4174.876
1c55.000	6611c60.000-170c5277.7	5U 9471369-U00	20615.852	6083.049	-4092.063
1660.000	6632218.375-17659157.0	JC 5467154.750	20570.476	5744.683	-4027.177
1661.000	<pre>% # # # # # # # # # # # # # # # # # # #</pre>	ju 9463U27.625	2U457.115	6157.232	-4181.197
1662.000	6673200-002-17647358-U	.n 9459001-250	20408.339	5890.664	-4101.753
1663.üL(i	e653561.562-17641255.2	5 G 9454825.75 0	23333.890	6120.78C	-4101.936
1664.000	6713942.562-17635572.2	SU 945C834.875	20312.407	5754.603	-4054.701
1665.600	6734106.612-1762558.0	00 9446652.250	20175.384	6171.642	-4128.128
1666.000	6754269.500-17623423.2	5G \$442546.250	20116.489	6075.245	-4151.893
1667.000	6774378.675-17617550.7	5 U 943E512.750	20032.130	6102.717	-4174.733
1668.440	6754353.125-17611369.0	00 9434307.625	20034.718	5656.116	-3542.394
1669.000	6814237.687-17605555.7	5U 943U3U3.625	19986.714	5583.105	-3835.216
1670.000	¢83421€.375-17595738.7	00 9426242.250	19760.979	6342.889	-4248.451
1671.000	6453962.625-17553534.2	50 9422006-000	15697.331	6216.975	-4229.963
1672.000	6873730.312-175878U3.U	JU 9416U87.250	19711.849	5758.747	-3557.741
1673.010	6495334.312-17561280.2	020.9413920.750	19500.450	6340.253	-4397.817
1674.000	691248U.187-17575657.0	00 9405763.750	15037.210	5368.726	-3785.478
1675.000	6932257.540-17565379.5	o 9405537.675	15430.156	6119.022	-4177.790
1676.000	6551801.875-17563821.5	20 9401707.000	19386.091	6022.604	-3537.851
1677.000	0.971455-875-17557656.0	JC 9347536.875	15293.712	5840.542	-4082.813
1678.000	699u243.250-17551205.2	50 93933U8.375	19161.030	6176.713	-4159.323
1675-000	7469454.812-17545556-5	062-0162862 00	15129.385	5830.148	-4064.845
1686.000	7626536.000-17539651.7	50 9385259.125	16998.546	6271 . 054	-4186.358
1681.000	747412.562-17534178.0	10 5381384.125	18959.158	5863.342	-4070.457
1682.000	70cc469.187-17527tc4.5	00 5377173.125	18820.208	5951.435	-4288.185
1683.000	7085322.437-17521730.0	JU 5373246.875	18797.597	5965.824	-4012.960

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3150-6024-R8-000 , Page A-23

Table A-2a.	Reconstructed Reentry Tra	ijectory and Asi	sociated Param	ieters (BET) —	- Continued
1684.CC	7104064-625-17515631-040	9365207.000	18623.957	6413.208	-4260.955
1685.641	7122810.000-17519066.500	5365257.125	16573.912	6290.424	-4170.172
1686.000	7141446.537-17534324.250	9361432.000	18674.994	5526.514	-3684.530
1687.000	7155924.312-17497536.000	9357450.500	16384.356	c474.857	-4684.953
1688.Cuu	7178380.5uu-17452245.250	9353468.375	16363.909	6020.954	-40c8.714
1689-00)	7196746.537-17486414.500	9349557.625	185.9.091	5605.131	-394().593
1650- Ŭ UŬ	7214855.560-17474592.750	9345300.375	18062.445	6834.805	-4175.812
1651-010	723335.187-17474615.55	5341779.125	16372.955	4816.675	-3511.280
1052-000	7251252.125-17408353.5%	5337718.CUO	18149.780	5662.995	-3671.625
1653.010	7265328.475-17402546.5° U	515.5853.375	17862.552	6208.694	-4111.262
1654.00	7287358.312-17457120.75	933 1255 250	17657.435	5965.660	-4179.069
1655.001.	1245146.544-17454542.230	9326233 .375	17358.466	6121.542	-3613.535
1656.6.6.	7322958.414-17445258.254	5322519-375	17706.813	6230.319	-3766.732
1c57.50.	724-45	531831,5•75J	17657.974	5683.394	-3855.459
1656.01	1027892.502-17452086.250	9-14425.d75	17525.482	5957.981	-3411.134
Le\$5	7375621.1.55-17427166.515	9311168-250	17632.627	5448.610	-3266.648
17. U.L	7395236•475-174419524559	372.1c51.52	17211.933	6126.577	-4474.565

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		ECI (GUIDANCE TI	G CCURDINATES Me 2ase)		
7 [ME	> ×	7	X-DCT	Y-DCT	7-DUT
1761.000	7413426.512-17415358.50	. 93J32C1.625	17414.357	5459.545	-3472.572
1762.044	7427086.090-17410475.25	1 9259763.375	17103.216	0326.772	-4003.206
1703-600	7444535.012-17404151.25	1 9245708.375	16942.602	ć645•646	-4082.329
1704-000	7401052.500-17397452.75	J 9291567.000	16875.495	6978.711	-3795.455
1765.365	7472573.251-17351533.25	· 5265535.375	17125.422	5755.518	-3294.208
1706.01.	7456441.5441.2545) 9285266.500	17150.216	4614.516	-316(.535
1707-61.	751=134-312-172E1511+Lv	5201472.25U	lcúya.5cl	5749. ú 58	-3635.641
1768.646	67.21.1625717.629-71737567	32277721.375	16734.655	5849.102	-3349.555
1705.000	7546422.537-17365228.75	5 < 7 4 4 5 6 . 8 7 5	16933.358	4534.123	-2745.854
1710-000	7563147. le /-17364657.50	5271085.125	16575.024	5901.221	-4054.681
1711.0%	7573440.50 1-0 30 1-0 735 5352.	. 9207152.75U	loc33.541	4593.293	-2979.837
1712-00-	7252774 . 627-17352637 . 25)	le 153. Juñ	6383.35 9	-3763.755
1713.600	7611787.675417346294.25	1 9255821.575	158-00.850	6851.360	-4352.053
1714-555	<u>1521775.531-1754-151.0).</u>	J 52:5887.375	16475.909	5946.086	-3703.969
1/15.001	7c43c27.81c-17334411.25	1 5222441.250	16244.398	4712.520	-3291.434
1/1c•C()	7655831.754-17346556.25	0.524852500	15708.031	6282 . 037	-3556.162
	1610103-431-17323566-01	- 524564.D.¢25	111.82vc1	5196.381	-3374.263
1/18-645	1051454.622-17217638.250	: 9242,56.5CJ	15340.251	4583.164	-3426.312
1/19•041	1111140.312-17316150.53	9238382.c25	150,99,621	7389.414	-4248.630
	11/2255.000-17305477.750	5<54251•5CU	15219.036	6346.181	-4005.332
1/21-010	727534 .25 17292129 .75	9230247.750	12423.892	6125.315	-3833.826
1722.60	1793194.629-17294236.25	 5226560.250 	15845.337	4200.934	-3166.548
1723.4.	1166456.734-17268756.34	- 9223241.75U	15.08.564	5854.325	-3427.240
1724.	7122762.615-17262236.25	9224J61.750	15261.384	5122.339	-3327.417
1725.61	775e5é6.375-17277678.25.	. 5216247.25N	14805.067	0.031.790	-3773.816
172¢•i'i -	7013047.375-17271558.19	5212523-564	14770.c15	5926.052	-3661.327
1727.000	7528265.812-17205517.504	4205J28.75J	14927.288	5208.024	-3384.352
1726.04	7312547.675-17202113.00	521,424.125	14611.226	5592.984	-2517.3JZ
1/25-64	12 - 12 14 - 6 1 3 - 1 7 2 3 2 7 1 2 - 2 5	- 92c1434 . 500	14273.081	6467.958	-4223.864
1736.6	1871757.075-17248245.15	5197c52.625	14082.165	4678.673	-3346-249
1/31.00	7265561.(000-17263531.50	9134379.25v	14535.512	4479.713	-345.334
1/32.11	1951 715.1s7-17228477.25	5191959125	14352.734	5074.311	-3416.051
1/35.51	7515111.5c2-17233188.751	5167c75.50	14264。149	4831.071	-3.81.317

Table A-2a. Reconstructed Reentry Trajectory and Associated Parameters (BET) - Continued

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Table A-2a.	Reconstructed Reentry Tra	ajectory and As	sociated Paran	leters (BET)	Continued
1734-662	7555138-250-1722850 0-75 0	0134.994.550	14102.701	4555.891	-2882.447
1735.040	7943122.437-17222576.500	5181124.125	12¢82•368	6531.665	-4426.279
1730.640	7356465.687-17215256.259	317c6z3.625	10404-034	6826.381	-4284.402
1757.04	797-278-937-172053c0-010	5172776.750	135u2.554	ců76.415	-3427.662
1738.CCU	7583545.566-17264516.259	91c5289.250	12632.323	5049.075	-3527.587
1735.640	7557472.167-17155177.530	51r6134 .5 u0	13869.596	4516.272	-2632.672
1740-000	8311027.687-17155634.750	9103681.75U	14288.622	2502.921	-2132.123
1741.000	8025279.125-17151536.25V	91-0,423.750	13402.745	4579.219	-2565.004
1742.00	Er 36622.550-17166809.25J	(sl57896.Cd2	12227-640	47:13.535	-2896.037
1743.600	8452335.812-17182473.500	£155069+25J	13542.11.	4562.530	-3024.773
1744.000	8)65572.675-17178343.250	515228U.E75	13167.522	4646.674	-3096.705
1745.000	E47E647.812-17173725.500	6145136.750	12922.915	5391.873	-3129.590



Table A-2a. Reconstructed Reentry Trajectory and Associated Parameters (BET) -- Continued

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	-19	-7 BET TAACKEK R	EENT NY				
TIME FRCM LIFICFF (SECCAGS)	INEKIJAL VEL. Magnitule (FI/SEC)	KELATIVE VEL. Magnijude 1FT/SEC)	INERTIAL FLI. Path Angle (degregs)	INERTIAL Péacing angle (degrées)	ALTITUCE (Féét)	GEUDETIC LAT.	GEDUETIC LONG. (DEGREES)
1189434.261	25534.1	24144.5	142-1-	1 4 1 4 2	26443 2		
1185435.231	6.15545	2-2-11-4			24000042		C18.58+
1185436.261	25531.6	8 1 1 1 1 1				170.07	242.68-
1185437.251	255ue.1	24154-7		27-27	C• 7 7 0 + + 7	110-07	-83.668
1189438.201	2-2-1962	2-15140			0.001442	20102	- 69-59-
1185439.281	25482.6	24133.2	-1-072	200000		374472	-83.522
1185440.281	25472.5	26123.5		20°00	2.121642	996.12	644.63-
1185441.531	25447.5	24166.1	- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	100000 100000	1-166242	21.910	-83.376
1169442-241	75467		CT707	162.04	241503.5	57.968	-83.303
1 18944 2 541					241424.0	27.958	-83.230
1185644 361			222-1-	96.41c	240886.4	27.548	-83.157
19244444		<	-1.206	524-85	244363.5	£7.938	-83.084
10707666077	1-01-02	24061.2	19101-	50 ** 96	239627.5	21.927	-83.012
		24052.00	-1.156	58.56	235280	21.917	-82.939
10707644077	0.000 1.1.1.1	24121.1	-1.231	56.547	238710.7	27.407	-82.866
10700110770011	2.57622	24024.4	-1.160	JB. Ú53	236159.2	27.847	-82.794
1974446911	<pre></pre>	24410.4	-1.173	96.638	2376411-0	27.847	-82.721
	<pre>c> 1 t • c</pre>	23965.E	-1.255	98.¢36	2371.07.5	27.876	-82.649
1424214641		23974.5	-1.156	J8.727	230548.0	27.640	-82.576
102+22+201	246,123	2.9927.6	-1.171	94.73¢	2360.14.0	27.855	-82.504
	2 2 2 4 2 • C	23547.5	-1.11c	58.753	235480.	27.845	-62.432
	3.67262	2-12652	-1.165	96 . dž4	234462.2	27.834	-82.359
100.430.61	5 61 7 6 7	23527.7	-1.166	94.84.	234426.5	27.824	-82.287
197.0242011	22424 • 0	23940.6	-1.075	38.88 ¢	233516.7	27.813	-82.215
192.124.011		23861.2	-1.155	768°84	233371.5	27.833	-82.143
TR7*8646911	222U6.4	23658.5	-1.145	165-86	232865.5	27.792	-82.071
102050542571	25166.S	23821.1	-1.202	99.01¢	232321.2	27.741	-81.999
	5-163-5	<2416.L	-1.055	240.52	231794.7	27.776	-81.927
152.134581	25145°C	237öž.ť	-1.202	59.076	231204.7	27.75	-81.855

CONFIDENTIAL

	61-	-7 BET TRACKEP N	EENTRY				
TIME FRCP LIFTLFF (SECCNCS)	INERTIAL VEL. Magnitule (FT/SEC)	RELATIVE VEL. Magnitueé (FT/SEC)	INERTIAL FLT. Path angle (degrees)	INERTIAL HÉAUING ANGLE (DEGREES)	ALTITUVE (FEET)	GEUDETIC LAT. (LEGREES)	GEUDETIC LONG. (DEGREES)
						076 60	
1185467.381	251LC.C	23752.5	-1.261	211.65	230149.0		
1105423		23748.7	-1.156	99.169	230221.2	21-130	-910172
		C 11750	-1-151	99.212	229711.0	27.727	-81.641
1 187464 • 7 5 1			-1-135	99.261	229195.7	27.716	-81.565
152.5346911				50, 00	228699.0	27.705	-81.498
1185466.201	2.10102			1.45.00	228190.7	27.694	-81.427
1185467.261	1-31362			00 400	227689-0	27-683	-81.355
1185468.261	25004.1	1.00062			227104.5	11.672	-81-284
1185469.221	24571.3	23624.1.	55571 1		2 909966	27.661	-81-13-
185470.281	24542 2	23545.0	-1.123	104.44	1.040022		
1196471-561	24527.5	235eû.7	-1.114	99 * 496	226232.5	1.000	741-10-
1105477.751	24406-3	23559.1	-1.066	99.535	225716.2	27.638	T/0*18-
11066333 561	24497.6	23550.4	-1.063	99.558	225238.7	27.627	-81°000
100 70710011	24 004 5	25547.4	-1.036	59 .6Ú 3	224773.5	27.616	-80.930
107057557571				99-612	224299.7	27.634	-80.859
T32.6/94811				50.673	223664.7	27.593	-80.788
1185476.221	24 6 Z 3 4 Z		008 -	96.5.00	223396.5	27.582	-80.718
1185477.241	24010.4			727 00	222816-5	27.570	-80.647
1185475.281	C. E1742	23420-1		77. 75 F	222351.5	27.559	-80.577
1185475.261	24727.3	23380.5		77. 7AC	22184V.G	27.548	-80.507
1185480.261	24716.4	4.76362	371.1-	200 451 20 451	221340.5	27.536	-80.437
11854El. 2cl	24674.3	23321.5			0000000	27.525	-80.367
1189482.261	24722.5	23375.2	-1901	99°100	2 202 202 2	27.613	-80-297
1185483.žël	24660.4	23313.4	<n1.1-< td=""><td>0.00</td><td>2.075022</td><td></td><td>727 Da.</td></n1.1-<>	0.00	2.075022		727 Da.
1185464.201	24572.5	23226.6	-1.625	016*66	2.112212	2007 20	- 400 - 1 5 T
1185485.261	24503.9	23217.2	-1.113	296.66	5-024612	144017	
1185486.281	24550.5	23202.2	-1.056	516°65	2.267815		
1185467.281	24451.7	23144.6	-1.652	426°66	21845/.2	104-17	070 04-
1165488.211	24434.5	23CEE • 4	-1.120	1.00.084	21/554.1		
1185449.261	8+43442	23077.6	450*1-	E66°55	n•214/17	****	

Reconstructed Reentry Trajectory and Associated Parameters (BET) - Continued Table A-2a.



Table A-2a. Reconstructed Reentry Trajectory and Associated Farameters (BET) -- Continued

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G1-7 BET TRACKER REENTRY

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TIPE FRCP LIFICEF	INEKTIAL VEL. Macritule	RELATIVE VEL. Pagnituge	INERTIAL FLT. Path angle	INERTIAL Feacing Angle	ALTITUCE (FEET)	GEGDETIC LAT.	GEODETIC LONG.
(SECCRES)	(FT/SEC)	(FT/SEC)	(CEGRFES)	(DEGREES)			
185490.281	24392.4	23445.5	-1.062	100.050	217635.0	27.432	-79.810
185451.581	24367.4	23020.3	-1.064	100.024	210564.5	27-421	-79.741
185452.221	24284.3	22536.2	-1.110	1 10.281	216116.7	27.405	- 79.672
185453.ZHI	24200.5	2291 7	-1.666	100.138	215660.7	27.357	-79-604
185454.2El	24264.5	22917.4	-1.021	100.116	215159.7	27.386	- 79.535
185455.261	24214 . 9	22664.0	-1.035	100.165	214705.7	27.374	-79.466
185456.261	24171.6	22824.9	-1.056	100.239	214225.7	27.362	-79.398
185457.Zel	24117.E	22771.1	-1.636	140.255	2137#6.0	27.351	-79.330
185458.261	24036.0	22751.5	-1.041	100.181	213340.7	27.339	-79.262
185455.261	ィチックた。モ	22711.5	-1.046	1 10.275	212871.0	27.327	-79.193
185.002681	24026.7	22679.6	-1.062	100.282	212423.C	27.316	-79.126
189561.261	23585.6	22638.0	-1-072	100.304	211960.2	27.304	-79.058
189502.20l	23425.6	22582.2	-1.092	100.415	211536.5	27.292	-78.990
185563.281	23512.3	22565.2	-1.65	100.326	211676.5	27.281	-78.923
185564.221	23648.3	22501.5	-1.026	100.416	210633.2	27.269	-78.855
165505.261	23767.1	22441.05	-1.021	100.500	210164.7	27.257	-78.788
185500.261	23766.5	22413.5	-1.062	100.421	209746.5	27.245	-78.721
189507.261	23717.2	22370.5	-1.057	100.498	2u9305.7	27.234	-78.654
189508.281	23672.4	22325.5	965	100.506	206880.5	27.222	-78.587
165555.201	2 - 5 2 3 E 2	22262.5	-1.617	100.555	208440.0	27.210	-78.521
189510.241	23565.8	22226.9	-1-6:03	1.00.539	208015.2	27.198	-78.454
189511.281	23541.5	22193.9	-1.066	100.633	207591.2	27.187	-76.388
189512.241	23511.3	22164.3	960	100.585	297174.7	27.175	-78.322
185513.281	23457.9	22116.6	EP 5	1.0.585	206737.7	27.103	-78.255
185.14.281	2413.2	22066.6	-1.025	100.697	206316.2	27.151	-78.189
185.515.201	23371.7	22024.7	-1.046	100.628	245920.7	27.139	-78.124
185516.221	5.45ELS	219Ec.E	-1.071	100.555	205466.7	27.128	-78.058
189517.201	23266.5	21914.5	915*-	140.800	205062.5	27.116	-77.993

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INEXTIAL VEL- MacNITULE (FT/SEC)	RELATIVE VLL. Mauniile [fi/sec]	INERTIAL FLI. Path Angle (Cegrees)	INERTIAL Fëading angle (Uegrees)	ALT ITUDE (FÊET)	GEODETIC LAT. (DEGREES)	GEDDETIC LONG. (DEGREES)
SAVAF 6	2144-8	246	100-723	244618.7	27-104	-11.927
	21836.6	-1.019	100.772	204221-2	27.042	-77.862
2.45155	21787.1	-1.068	100.786	2013616.5	27.080	797 . 77-
2 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5 -	21714.5		100.915	C-34399.1	27.069	-77.732
2 4040-1	21645.4	-1.068	1.00 . 794	202929.0	27.057	-77.667
27581.4	21634 6	5 64	100-914	202495.7	27.045	-77.603
2,2936.8	21590.2	-1.159	100.902	202114.2	27.033	-77.538
22862.2	21510.1	-1.05	5FD.101	201727.0	27.021	+14"11-
22603.3	21457.5	-,996	101.128	201201.0	27.009	-77.410
2.776.2	21414.2	-1.11	101.105	200737.0	26.997	-77.346
27c91.3	21345.5	- 925	101.178	200392.6	26.985	-77.283
22641.7	21295.4	-1 - 04	101-118	200056.0	26.975	-77.219
2614.3	21267.5	-1.077	101-097	194608.0	26.961	-77.156
22532.1	21186.2	581	101.233	199241.0	26.949	-77.093
27486.3	21140.7	-1-142	101.256	194627.2	26-937	-77.030
2404 4	21056.5	861	101.381	198487.0	26.926	-76.967
22343.5	20358.3	975	101.445	157993.0	26.914	-76.905
22437.4	21093.2	-2.750	101.364	197752.2	26.902	-76.843
22200.9	2nu54.9	711	101.356	197054.7	26.889	-76.780
22115.6	20770.8	473	101.568	196595.7	26.878	-76.718
22074-1	23729.1	685	101.585	190430.5	26.866	-76.657
72072.7	20727.2	-1-249	101.459	196036.2	26.854	-76.595
21948.2	20602.5	- • 664	101.651	195617.2	26.841	-76.534
21947.6	2.3602.6	-1-380	101.583	195116.7	26.829	-76.473
21867.6	20534.7	-1.230	101.452	154880.5	26.818	-76.412
21733.5	2.385.2	- 393	101.765	194366.7	26.800	-76.351
21765.6	20423.5	-1.51/	101.635	193933.7	26.194	-76.290
21633.9	20285.4	824	101.824	143734.5	26.782	-76-230
	MARAI MARAI (FIVAL (FIVAL (FIVAL (FIVAL (FIVAL 2332 2332 2332 2332 2325 2334 2225 2225	INEXTIAL VEL. RELATIVE VEL. MAGNATULE F1/SEC) F1/SEC) F1/SEC) F1/SEC) F1/SEC F1/SEC) F1/SEC F1	INENTIAL VEL. RELATIVE VEL. INENTIAL FLI. FI/SEC FI/SEC FI/SEC FI/SEC FI/SEC FI/SEC FI/SEC FI/SEC	INENTIAL VLL. RELATIVE VLL. INENTIAL FLT. INENTIAL FLT. INENTIAL VLL. FT/SEC FT/SEC FT/SEC CEGREES LUGEARES ANGLE FT/SEC FT/SEC FT/SEC CEGREES LUGEARES ANGLE FT/SEC FT/SEC FT/SEC LUGEARES LUGEARES LUGEARES 23235.8 21065.8 21056.6	INERTIAL VEL RELATIVE VEL INERTIAL RELATIVE VEL INERTIAL RELATIVE VEL INERTIAL RETUDE FT/SEC FT/SEC FT/SEC CEGREES CEGREES CEGREES LUO-722 SU4CLE-72 FT/SEC TLUBE-8 965 LUO-722 SU4CLE-72 CU4CLE-72 Z3165-6 Z1187-1 1019 LUO-722 SU4CLE-5 Z3165-6 Z1185-7 1019 LUO-722 ZU4CLE-5 Z3165-6 Z1634-6 LUO-723 ZU4CLE-5 ZU3295-6 Z2691-7 Z1634-6 LUO-914 ZU2295-7 ZU2395-7 Z2641-7 Z1445-2 LUC-72 ZU4CLE-5 ZU2395-6 Z2641-7 Z1644-6 LUO-1178 ZU295-7 ZU295-7 Z2641-7 Z1445-2 LUO-1178 ZU0056-6	Interflat. VEL. REATIVE. VEL. Interflat. V

Table A-2a. Reconstructed Reentry Trajectory and Associated Parameters (BET) -- Continued

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Table A-2a. Reconstructed Reentry Trajectory and Associated Parameters (BET) - Continued

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GI-7 BET JAACKER REENTRY

TIME FROM LIFIUFF (SECCACS)	INEKTIAL VEL. Magnitude (F1/SEC)	RELATIVE VËL. Magnitule (ft/sël)	INERTIAL FLT. Path Angle [Uegreës]	INEKTIAL Feading Angle (Degrees)	ALTITULE (feet)	GEUDETIC LAT. (DEGREES)	GLODETIC LONG. (DEGREES)
1189546.281	21621.7	20262.6	÷66.1-	1.1.566	143202.7	26.765	-76.170
1185547.231	21447.7	20153.5	1.430	101.956	193076.2	26.757	-76.110
1189548.241	E1448.3	20152.H	5,5.1-	101.633	192504.2	26.745	-76.051
1 185549. zal	21421.2	20076.6	-1.327	191.841	192076.2	26.734	-75.991
1185550.241	21353.2	20066.8	-1.426	1J1.900	151802.7	26.722	-75.932
1189551.281	21167.d	19843.3	JE7	101.961	191172.5	26.710	-75.873
1189552. 2ċl	21103.3	19757.5	.223	101.835	190997.5	26.698	-75.814
1189553.241	21184 • 4	19840.1	-2.132	101.872	190.714.7	26.686	-75.756
1185554.241	21(83.6	19740.0	-1.833	1-12-027	19-0043.7	26.674	-75.697
ll89555. čil	21913.7	19505.6	356	102.006	189932.0	26.662	-75.639
1189556.281	20471.6	19625.8	-2.389	102.340	189271.0	26.650	-75.581
1185557.241	29706.8	19362.5	. 757	102.172	188897.7	26.638	-75.523
1185558.241	5-264-5	19451.2	-1.561	102.168	188111.2	26.626	-75.466
1185559.281	2uc78.5	1,3564	-1.055	101.747	183182.5	26.614	- 75.409
1189560.2dl	£0567.7	15224.6	847	192.379	187577.2	26.602	-75.352
1189561.201	2-1557-2	6.61201	-1.745	102.154	186621.0	26.591	-75.295
1189562.241	2u4u7.0	19464.0	848	102.421	186538.7	26.579	-75.238
1185563.241	20440.1	19056.3	-2.053	102.162	186129.5	26.567	-75.182
1189504.261	20256.3	18415.3	303 · I	102.462	186125.2	26.555	-75.126
1185565.441	20199.2	18855.1	-1.551	102-923	185386.0	26.543	-75.070
1189566.221	žU125.7	18781.5	-1-205	102.248	184858.0	26.532	-75.015
1185567.251	20152.8	14810.C	-2+669	1.12.256	184290.5	26.520	- 74.959
1189568.241	L . 84022	18705.2	-2.250	102.269	184244.5	26.509	-74.904
135.5565811	15821.0	13475.5	• 253	1u2.120	184053.0	26.497	-74.850
1189570.281	19914.7	18565.3	-2.714	101.869	183239.2	26.486	-74.795
1189571.2cl	1~54C~1	18406.2	-1.565	102.467	185055.7	26.474	-74.741
1189572.251	19567.5	18225.7	- 40.5	102.775	182653.2	26.463	-74.687
1189573.žel	15758.6	18413.8	-3.876	141.700	181329.5	26.452	-74.632



	61-	7 BET TRACKER R	ENTRY				
TIME FROM LIFTOFF (Seconcs)	INEKTIAL VEL. Magnitude (ft/Sec)	KELATIVE VEL. Maŭnitude (fi/sec)	INERTIAL FLT. Path Anglé (degrees)	INERTIAL Heading Angle {uegrees)	ALTITUDE (FEET)	GEODETIC LAT. (DEGREES)	GEODETIC LONG. (DEGREES)
			055 6	000 001	7.00181	26.440	-74.579
1189574.251	1.01621		162.2	102-0105	18118.0	26.429	-74-526
1189575.241	19304.0				1 00 000 1	24.418	-74.472
1189576.281	19352.6	18005-8	- 2 - 5 - 1	600 COL	1000500	26.406	-74-420
1185577.281	15264.4	L 7962 .			100100 3	26 30F	-74.367
1189578.261	19221.3	17371.4	-1-424	186.101	7.001001		
1189579.261	19147.0	17758.5	-2-004	101.000	180010.0	105+07	
1189580.281	18546-5	17603.4	171	102.719	178831.5	26.373	202.41-
1100501.051	12010-2	17575.3	-1.628	102.505	177502.0	26.362	-74.210
1100K63 341	19761	17411-6	.657	101.547	178158.5	26.351	-74.159
11070563 241		17474 - C	-3.054	103.842	178499.2	26-339	-74.108
1107000.CCL	0 0 0 0 0 T	2 05671	242	102.145	177298.7	26.329	-74.057
102000000000000000000000000000000000000		17436.3	-2.941	102.345	177854.0	26.318	- 74.006
11852829*251	10101		-4.005	1.12-125	176871.0	26.307	-73.956
122 • 02C5PTT	1001 CO1	17205.7	-4.485	100.887	175652.2	26.297	-73.905
102010011	1001			101-326	175628.2	26.286	-73.855
122888.581		J J J J J T I	2.660	102.702	175830.7	26.276	-73.805
132•5865811			-1-000	102.353	176647.0	26.264	-73.756
102-0464011		0 1 1 0 0 1 1 0 0 1	-1-044	101-430	174552.5	26.254	- 73. 706
197°1464911	17765 A	14264	3-611	101.745	174790.2	26.245	-73.657
107-72/271			-2.521	103.512	175441.2	26.234	-73.609
102-52255			2.912	102.387	174336.7	26.223	-73.560
102********	0 95555		55.5-	101-957	174034.5	26.213	-73.512
122.522551 T				102.027	172849.7	26.203	-73.465
147.9868BL1				172.450	171836.5	26-192	-73.417
1189597.2 81	17520.5	0.14101	607-7-		0 007121	24.192	-73.370
1185554.261	17158.4	15857.6	1.658	103.52		904 • D3	
1189559.251	17350.1	16002.1	-3.345	101-684	1.1212-0	217.02	
1189604.241	17650-7	15746.2	.166	102.773	1110111	701.02	
1189601.281	16555.4	15614.6	.620	CDE.EDI	110022.1	761.07	

Table A-2a. Reconstructed Reentry Trajectory and Associated Parameters (BET) --- Continued

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Table A-2a. Reconstructed Reentry Trajectory and Associated Parameters (BET) - Continued

	-19	7 BET THACKER R	EENTRY				
TIME FROM LIFIGFF (Seccnes)	INENTIAL VEL - Magniture (FT/SEC)	KELATIVE VEL. Magnijude (FT/SEC)	INERTIAL FLT. Path angle (degrees)	I NERTIAL Heauing Anglé (degrees)	ALTITUGE (FEET)	GECDETIC LAT. (DEGREES)	GEUDETIC LONG. (DEGREES)
1189602.261	17335.4	16004.2	-7.525	101-938	169995.6	26.141	-73.184
1189603.241	16970.2	15631.2	102.4-	102.925	168211.7	26.131	
1159604.281	17032.7	15696.7	-3.514	1.02.763	166825.0	26.121	-73.093
1189605.661	16696.3	15360.5	3.416	103.940	167237.2	26.110	-73.048
1189¢C¢.281	1c5b1.7	15244.3	-3.415	103.580	166608.7	26.100	- 73.003
1189607.261	16438.8	15095.1	590	102.974	166389.2	26.091	-72.958
1185608.281	16430.2	15065 . 2	-3.851	142.881	105584.0	26.080	-72.914
1189¢05.2±1	lo33ö.u	14995.4	-3.431	112.737	1c4415.C	26.070	-72.870
1189616.261	lole7.1	14624.5	706	143.040	103763.0	26.061	-72.826
1189611.261	16635.6	14052.7	-2.428	102.912	1c2875.5	26.651	-72.783
1189612.281	1 e 229.2	14858.7	-6.431	103.672	161219.0	26.041	-72.740
1189613.261	15779.5	14443.4	.624	104.101	160405.7	26.430	-72.697
1189614.201	15576.1	14236.2	1.657	103.548	160651.7	26.020	-72.655
1189615.261	U.sous.U	1+261.5	954	143.648	160475.2	26.010	-72.613
1189616.281	15372.E	14026.7	.235	102.546	160674.2	26.001	-72-572
1189617.201	15256.0	L3947.2	129	192.070	160046.0	25.992	-72.531
1189618.281	15754.1	14471.8	-7.676	104.414	159041.2	25.982	-72.489
1189619.261	15645.2	14321.2	-8.750	103.493	156160.5	25.972	-72-448
1189620.281	15198.4	13854.7	-5.00£	102.031	154744.2	25.962	-72.407
1189621.281	15103.9	15777.9	-2.458	145.568	154853.2	25.952	-72.368
1189622.241	14816.8	13466.2	1.723	102.107	153900.5	25.543	-72.328
1189c23.281	14662.0	13346.6	9.672	104.250	155316.7	25.534	-72.289
1189624.241	14474.6	43142.5	-280	103.378	155453.7	25.925	-72.250
1189625:241	14334.6	12985 .4	195	102-867	155856.2	25.916	-72.212
1189626.241	14421.3	13080.4	.253	103.592	156207.5	25.907	-72-174
1189627.281	14522.1	12961.9	352	103.724	157204.2	25.897	-72.136
1185628.281	14348.1	13002.4	-3.152	102.453	156668.5	25.888	-72.098



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Table.	A-2b. Reconstructed	Reentry	r Trajectory an	d Associated Pa	trameters (7:	18 Radar)
		GE Na	MINI GUICANCE Sa • Mannec Sp	ANALYSIS PRUGR Acecraft cente	A M R	01/10/66
			ECI (GUICANCE TI	G CCGRDINATES Me base)		
TIME	×	>	7	X-D0T	Y-D0T	2-001
711-666	£254132+25 C-17 8610	0€ 1 • 03•	9266236.675	15570.862	2629.238	-4045.121
712.666	6311213.uu0-178584	44.500	5262578.875	17141.559	2331.898	-3053.877
713.000	6328094.187-176537	-E9.75C	5255465.625	16517.355	5604.880	-3830.688
714.600	6344116.437-178486	000-11	5255465.675	16694.507	5227.332	-3614.112
715.000	6360cc6.875-176432	25.346	5251765.75C	15645.093	3701-231	-3886.600
716.CUU	6377023.060-178398	05.75U	9248335-546	16604.913	5466.207	-3604.514
717-066	6393UL1.5U0-178345	55.000	92444e4.<5u	15410.116	4967.872	-4066.531
718.000	640 5066.250-178300	45.25U	9240837.125	17433.083	2025.040	-2530.235
719.000	6425690.875-178264	78-000	5237668.250	15831.038	4635.181	-3731.163
720.000	6441056.562-178215	54-500	5233758.375	14802.729	4085.149	-4146.317
721-000	6456643.25U-178165	81.500	5229956.500	15930.364	5221.491	-3623.633
722-600	6473047.062-178127	12.750	9226754.000	16091.720	2964.84J	-3151.042
723-000	6466554+687-178080	66.750	5223109.625	15047.003	4817.238	-3743.460
724.000	£503592.537-17804C	41.500	9219612.375	15.072.0743	4549.247	-3761.125
725.000	6518964.250-177552	17.750	5215790.000	15192.696	4985.419	-3695.328
726.000	6533979-937-177943	24.000	9212040.250	14299.905	4427 . 81U	-3953.870
727.600	6545756.500-177895	81.500	5208794.125	15789.593	3251.476	-3015-569
728.000	6564348-750-177853	59.250	9205632.000	14804.592	3640.555	-3454.540
725.600	6575601.000-177813	28.000	9201659-000	15016.327	2819.703	-3166.610
730-000	6594382.750-177767	18.750	9198115.000	13663.394	4165.233	-3538.483
731-000	6609019-312-177720	55.250	9194519.675	13897.064	4106.735	-3767.658
132-000	6623680.937-177672	90-750	9196569.750	14476.175	4589.113	-3571.808
733-660	6638154.062-177633	55.750	5167574.125	15064.974	3962.778	-3152.582
734.000	6652562.625-177589	64.750	9164107.125	15199.354	3219.832	-2901.747
735-600	6667051.625-177547	46.750	918C768.G00	13694.773	4273.363	-3634.368
736-600	6681477.375-177510	45.250	5177550.675	15111.296	1984.757	-2551.009
737-000	6695594.125-177466	74.000	9174136.375	14195.778	4567.122	-3396.844
738.000	670 9445. 500-177421	96.750	9170664.375	14279.510	4738.315	-3343.684
135-000	6723242.625-177377	37.500	9167217.625	13886.953	4610.464	-3440.285
740-000	6137176.625-177331	71.500	91¢3853•750	13415.388	4282.357	-3476.829
141.600	6150052.562-177268	18.000	5166450.250	13528.644	4423.822	-3406.835
142-000	6164245.000-177246	60.ŬUO	9157154.750	13136.025	2697.908	-3099.161
143.000	6777690.562-177207	71.500	5153936.125	13928.605	4561.916	-3189.524

3886.0U0 3604.514 4066.531

3150-6024-R8-000 Page A-35

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-3340.456	-3311.256	-3219.511	-3146.163	-3098.912	-3235.061	-3118.256	-3063.740	-3094.285	-3057.309	-3004.774	-3019.343	-3354.928	-2901.962	-2871.342	-2847.454	3010 206	CN7•0107-
4104.586	4236.450	4166.152	4246.600	4511.102	3598.074	4137.918	3867.442	3948.571	4018.291	3958.485	3976.186	4942.672	3913.365	3659.064	3523.382		1044405
13040.264	13031.167	13073.495	13191.040	13339.369	11945.829	12688-097	12377.045	12206.512	12219.815	12151.980	11860.242	11386.033	11929.788	11437-845	610-92011		11382-023
5150610.375	9147349.125	9144078.375	9146674-250	5137683.000	9134521-250	9131427-875	9126285.675	9125245.250	9122205-125	9119206-750	9116173.675	5112193.125	000-2210116	9107249-500	090 8189010		9101385.250
47CC 951-562-17716515-500	600 107 250-17712157-250	22-3127-062-12708006-250	6211211805 187-1770 3873.750	6222225 125 125 125 125 125 125 125 125 1	2555669,187-1765669,750	4845467_875-17691501-750	KARE RE2.312-17687514-750	4802277_437-17683578-500	4005510 250m17675677.250	69017767 187-17676701 000	C3CHCB 037-17671637.750	C3230C00711110110210120 40417475540176676485500	LOTE 2000 250 250 250 250	6973300000000000000000000000000000000000	00000000000000000000000000000000000000		69E7725.062-17651843.000
000 772																755.000	766.000

Reconstructed Reentry Trajectory and Associated Parameters (7:18 Radar) - Continued Table A-2b. A-30

3150-6024-R8-000 Page A-36

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ır) — Continued	01/10/66		Z-D0T	-2738.320	-2650.270	-2657.079	-250,023- 1001,001-	-2578.553	-2544.546	-3219.020	-2456.603	-2882.509	-2402.055	-2376.993	-2425.424	-2622.942	-2383.397	-2216.733	-2251.964	-2233.250	-2880.942	-2127.292	-2064.183	-2019.547	-1953.256	-1565.752	-1926.606	-1907.252	-1799.776	-1896.137	-2057.614	-3094.068	-1832.306	-1643.114	-2939.464
rs (7:18 Rada	¥.		Y-D0T	3616.221	3078.490	3455.477	CT1 • 1115	3416.471	3511.290	5313.989	3197.573	4406.149	3404.826	3106.671	3218.006	3966.993	3380.009	3035.309	3037.978	3066.251	5039.106	2988.208	2690.599	2660.459	2363.311	2644.980	2608.464	2635.501	2286.670	2791.541	3217.048	6169.742	2801.737	2189.711	5720.139
ated Parameter	NALYSIS PROGRA	; CCORDINATES 16 Base)	X-00T	11339.513	10799.416	11065.107	11692.4UZ	10650.747	10724.228	9672.256	10214.187	9556.065	10485.687	9624.756	560°E445	5286.866	5492.061	5590.620	5069.582	5042-083	E573.590	8992•885	E495.600	6338.450	1001.213	8212.405	6224•336	8195.689	7875.510	8600.491	7943.756	7097.045	8442 • 627	7381.272	5741.835
tory and Associ	HINI GULCANCE / 54 • MANNEC SP/	ECICANCE TIN	7	5656610.675	5695343.750	5652636.250	C1C+2000C05	9664895.625	9082325.625	5675645.625	5076995.375	907435C.625	5071793-000	5065415.500	5066978.125	5064236.250	5661664.125	5659401.000	9C57197.625	9054813.875	9652258.375	9045E58.625	5047783.875	5045440°315	904 34 14• 250	9041228-500	5035278.500	9037373.125	50354C8-000	5U32140.625	5031214.000	5025180.750	9627152 . 500	9025183.675	9023303.125
Reentry Traject	GE NAS		٢	-17648194•500	-17643121.000	-17635724 . 5u0	-17633682.250	-17625755-000	-17626334.750	-17622680.250	-17618574.000	-17615250.250	-17611680.750	-17608587.500	-17605157.750	-17601025-250	-17557270.500	-17594163.000	-17591338.750	17567642.750	-1/283865./50 17500037 500	004 ·/ / 2086/1-	000-964//6/1-	UC2+21651611.	NGJ • N7711 GJ T.	006-545/26/1.	04/ 81/ 404/ 1.	1/262/78.000	17558573.250	17556347.750	17553675.250	17550528.000	17547348.750	17544275.500	17541435.500
Reconstructed			×	-000*8505559	7009666.250-	7020529.312-	7042463.812-	7053182.812-	7063755.250-	7073854.937-	7083568.750-	7093836.875-	71u3765.687-	7113560.875-	7123420.187-	7132406.187-	1141411.937	7151066.312-	7160063.437-	-000-1505011	-00C+3/0//1/	-790•052391/	-000-2106611	7011615 06000	-200°210117/	-164-EUD0221	-20C+2222222	-671•6770671	-1242413.150-	12155555-312- 2000 - 2002	7256597.750-	7266067.125-	1273555.125-	1280857•000-	1251898.312-
Table A-2b.			TIME	761.000	762-000	763•000 764-000	765-000	766.000	767.COG	768.000	769.600	170-000	771-600	1/2-000	173-000	14.000		1/6.000		770 000										200 002	189.000	199 - 067	000-15/	172.000	173-561

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-1680-151	-2201.480	-1821.915	-1577.544	-1791.307	-1452.014	-2511.139	-1460.363	-1400.756	-1313.766	-1573.872	-1335,932	-1248.381	-1606.304	-1546.657	-1137.248	-1230.723
2457.336	3855.115	2875.968	2267.745	2930.274	1962.278	4893.831	2207.334	2052.396	1827-593	2563.419	2009.907	1841.804	2774.478	2707.347	1680.124	1964.178
7896.803	6501.102	6691.896	6504.957	6359.295	6163.479	5605.582	6751.737	6580.329	5524.080	5438.629	5311.051	5657.395	4733.688	5874.715	5879.272	5668.638
5C21406.625	9015666.000	5017724.750	5015716-125	5013943.250	5012385.375	5010439.250	50C8653.75U	5007266-875	9005577.675	9003586-125	9002296.750	5001076.250	8595645.500	855F138-125	8956501.375	8995322+000
7294632•937-17538512•500	7301191-437-17535557.000	7367665-000-17532776-000	7313550.687-17529423.500	7320574.437-17526593.500	7226576.500-17524318.000	7337884.875-17520948.750	7326664.250-17517585.750	7244843.562-17515588.250	735/04/5-312-17513161-250	7264246 275-17510551.250	7241927.500-17507671.000	7267205.375-17565564.500	7272577 812-17503561 500	1212211-012-1-210-1122121 22-22-15 212-12210225-250	001 - CICODCIT_21C+CIIICI 001 - CICODCIT_21C+CIIICI 200 - CICODCIT_21C+CIIICI	1367568.562-17456219.000
754-000	795,000	766 000		700 000											808-000	810-000 810-000

Table A-2b. Reconstructed Reentry Trajectory and Associated Parameters (7:18 Radar) -- Continued

CONFIDENTIAL

3150-6024-R8-000 Page A-38

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Table A-2b.	Reconstructed Reentry Tra.	jectory and Asso	ciated Paramet	ers (7:18 Ra	.dar) — Continued
	02	EMINI GUICANCE Asa • Manned Sp	ANALYSIS PROGRA	۲ ۲	01/10/66
		ECI (GUIDANCE TI	G COORDINATES Me Base)		
TIME	×	7	X-00T	Y-00T	Z-00T
611.000	7392113•375-17454255.750	8994123•500	4810-519	1474.730	-1020.074
812.000	7357860.250-17491239.500	8592492.500	4865.122	1552.587	-1034.138
813-660	7402432.750-17485772.250	8591505.675	4761.449	1494.152	-995.627
814.000	7407003-062-17487600-500	8990251.675	5141.062	1908.725	-1155.194
815.006	7411531.625-17485154.000	8586913•675	4802.546	1861.326	-1119.360
816.600	7416084.187-17482580.250	8567672.750	4479.395	1678.504	-1016.162
817.000	7420242.250-17481152.750	8566625.500	3849.147	3097.712	-1550.540
818.000	7424665.812-17476505.750	8565382.750	3961.061	1126.404	-765.360
815.000	7428718-042-17476813-000	6984231.125	4380.422	1420.482	-874.491
820.000	7432636.750-17474532.750	8983024.750	3246.652	1086.921	-693.895
621 - 00Ü	7436191.062-17472610.000	8581742.375	3067.426	1123.164	-693.176
822.000	7440317.437-17470425.750	8580834•625	3290.054	1787.285	-951.581
823-000	7444061.687-17468779.250	E975926.875	4011.136	1988.063	-1057.921
824-600	7447665.500-17466410.750	8578734.875	4106.871	2523.936	-1271.158
825.000	7451202.937-17464000.250	6577525.000	2507.752	1794.039	-893.492
826.000	7454366.125-17461430.250	E576295.E75	2995.437	1033.858	-598.252
827.000	7457886.500-17459636.000	8575365.750	2643.372	2420.765	-1139.175
828 . じじじ	7461146.187-17457457.500	E974318.625	2335 . 749	3840.153	-1751.423
825.600	7464056.500-17455560.750	8973381.125	3342.736	1135.411	-616.565
830.000	7467213.687-17454044.500	6972617.125	2990.221	973.972	-533.064
831.000	7470462.375-17452054.500	6571676.250	3996.851	1305.943	-717.124
832.600	7473571.562-17450456.750	ES7CE74.875	3294.854	1102.206	-580.657
833.000	7476614.625-17448375.750	E9699U5.25Ü	2825.306	819.635	-427.950
834.000	7475867.187-17447215.000	8565322.675	3004.543	1048.866	-510.422
835.600	74 27 58.750-17445417.750	8568479.675	619-020	4666.305	-1924.547
836.000	74640C8.25u-17440723.500	8566495.875	4809.397	-1385.824	408.145
837.000	7486425.062-17443346.500	E567463 . E75	3306.951	-497.391	128.742
838.000	7491412.687-17441668.500	8566689.750	2009.989	6639.251	-2813.115
000.568	7492745.812-17438002.000	8565159.875	5463.789	-2346.523	840.481
840.000	7456181.500-17438860.500	E565454.E75	4736.840	-3549.997	1397.714
841.600	7458853.875-17436601.000	8564458.125	1471.428	6566.046	-2921.046
842.000	7455826.625-17432524.750	6562945 . 625	2395.147	1272.068	-539.581
843.000	7503219.062-17431857.000	8562443.625	1876.179	621.623	-229.718

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CONFIDENTIAL

3150-6024-R8-000 Page A-39

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r) — Continued	-127.334	-255,322	-43.668	-205.616	-325.436	-404.350	-2302.374	20.357	-271.242	-1146.702	-901.650	-148.086	-192.376	-104.322	-402.922	-263,232		-2464-400
s (7:18 Rada	489.163	667.645	310.085	528.630	883.577	960.158	5322.622	116.547	822.189	2995.024	2182.686	571.975	666.031	551.249	970.264	025 010		6244 • 589
iated Parameter	1409-518	2196.900	1653.883	2076.594	2211.942	2634.996	1521.038	1701.402	1864.083	609.206	2134-803	1345.300	1453.345	1190-619	739-187		LU40.679	-1057.470
tory and Associ	8562122•375	8560829-250	8540525.875	6558587.250	8558915.250	6556502 . 250	8958003.875	8957954.125	6557292.250	8556781-125	P556286_000	8955411-875	8955148-125	8554850 000	PC54689_750		200.0004152	8953480.625
Reconstructed Reentry Trajec	7505520-187-17431165-250	7507477.687-17428062.000	7505622-937-176225-000	7511438-187-17423630-250	7613376-375-17423319-000	7516034-750-17422350-750	7517660.500-17421027.250	7521256.437-17420997.500	7521990-500-17415158-500	7624573_562-17417508_000	7626301 687-17616554.250	7537587_875-17614430.250	7520156 - 000-17613668-250	7630336 060 17613852 750	001 270771172000000000000000000000000000	00000000000000000000000000000000000000	75363C1.250-17411247.500	7538025.000-17405187.500
Table A-2b.	JUJ 998	000 370	000°770	000-048	848 COU	845-000	850-000 850-000	851 .000	552 DOU							000-858	855.000	860.000

		N A C	ENINI GUICANC	E ANALYSIS PR	UGRAM Nter	01/10/66
			E I GL I DANCE	CIG CCORDINAT TIME BASE)	ES	
1 M E	×	۶	7	D0-X	T Y-DOT	2-007
.000	7626666 2560-1761	05315.500	CC3 222 ECS	5 81.2 5 20	1261 130	
-000	7540304-126-126	0.2598.000	8051247 625	07C * 100C	611-1C71 676	
	7761-647 6306736	000.000.000	C20+1+21240 C20-142		243-843	161.008-
	1721-100-22002221 1721-100-22002221	000-56100	6722078•127 8651051-500	-001.290 3769 660	282•905c	-2134.959
-000	7546558-875-1740	ua239.250	8551356.750	2612-732	- 2458,840	1157.763
• 000	7550165.937-1740	05335.750	8552274.50U	-1213.811	6284.215	-2527.286
- 000	7548024.437-1735	57764.500	8945238.500	775.806	1603.215	-581.448
- 000	7545072.062-1739	96770.250	E548956.E75	1365.200	159.333	43°026
- 600	1550078.750-1735	92165.750	E547022.250	2884.079	-4938.476	2315.269
-000	7551764.125-1739	93049.750	8547531.500	-151-891	5404.937	-2277.705
.000	7553348.250-1735	51055.750	E546770.625	1920.828	-1056.504	608.425
000.	7557026-375-1735	94161.000	6546175.250	1829.041	144-010	14.021
000-	7557450.562-1735	91265.500	8547061.375	918.946	3454•229	-1407.873
	3611-181*5841661	86103-000	8944935•375	1011-297	1722.685	-654.825
000-	96/T-7TC+6/3666/	87769.250	8545808.125	4605.414	-1634.725	649.388
	1501221•687-1735	85555.000	8545111.125	975.133	1834.270	-651.822
000-	(361863•687-1738	82034-250	8543504°125	1214.614	-4871.470	2452.939
000-	1433862+562-1742 7555253 2562-1742	27575.250	8566673.750	-2757701.719	-1010089.836	352162.617
	06/1_670*107506/ 06/1_670*107506/	07C 14* 200		261.0621	536.563	-93.268
	7545740 (1520) 7545740 (1520)	81634•25U Bubba End	062.9114.250	856.815	1588.181	-590.624
000	7570664.187-1738	PD 2 4 3 - 2 5 0	000°2366758	01604641 2670 482	841-144	201 •08- 155
000	7572301-000-1738	80686-000	8543681 F75	2152.609	-1562,853	934 108
.000	7572031.500-1737	76422-000	8541556.500	-411-407	4575-316	-1884.741
000-	7574641.187-1737	75236.250	8941525.750	2936.561	-2386.535	1108-641
.000	7576568.937-1737	77559.000	8542692.000	452.028	2233.776	-830.731
• 000	7576080.250-1737	73634.250	E54C884.E75	105.646	3089.658	-1153.136
• 600	7577558•667-1737	72881.250	8541004.250	7435.217	-14439.009	6516.255
• 600	7579157.125-1737	71164.250	E940345.E75	6102-052	-9974.014	4598.382
-000	7581137.375-1737	70755.250	8540314.750	1116.454	438.562	12.410
.600	7562765.437-1737	71267.000	6540686.125	1158.127	355.211	-25.687
	7583772.250-1737	70029-500	8540285.250	-5585.250	16385.601	-6589.375
000	7584220.125-1736	57154.750	6539192.125	2170.511	-1995.819	1048.285

Reconstructed Reentry Trajectory and Associated Parameters (7:18 Radar) - Continued Table A-2b.

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-2b.	Keconstructed Reentry 114Je				
	009 97937261-000 3007332	8640530-375	-393.256	5879.991	-2528.933
				2631 526	-1399.757
	7586437.062-17363392.250	6231184.623	N70*061-		
	7627046 276-17362427.250	FC37454.750	-707.284	8105.334	-3487.502
			200 C77L	-14266,195	6417-975
	7585302.187-17362276.19	E531381.623			
	7601000 187-1726665 000	£538£77.375	9.014	3512.883	-1340.221
		022012-250	2076-932	-1367.166	772.234
	062+0+2605/T-/RT++70266/	n-1+7776660	11111111111111111111111111111111111111		-504.70B
	7593568-187-17361227-750	8937612.250	すかり・レーン	106+6701	
	JECENTE 107-1736667-250	#536488.675	-1332.396	656ܕ258	-2700.554
		000 2777235	3356.766	-4781.133	2294.156
	001 • 0661 CE11 - 00C • 1 75 35 61				-403-N82
	7557921.312-17358330.750	8536799.25U	C11•160	0 4 0 • 0 0 0 T	
	7501 40 ENAL17257818 750	AC 36 744 .000	1151.698	384.988	26.092
			070 7001	-1056.297	579-255
	7555826.375-17356020.750	010 * F + T U F A			
	7401741 425-17356686 750	8936777.675	1316.801	749.935	cc1•76-
			702 207	-1377-369	828.908
	J602774.93711/12035000	C 7 T + 1 D C 3 C 4 D			
	74112034 562-17354671-000	8526216.000	1277-079	2403-842	- 400 - 400
	2014 - CONTRACT - 2017 - 2010 - 2014	000000000000000000000000000000000000000	CEE UYE I	539.059	-47.314
	7605466.93/-1/333823-200	0.1 * 5 7 6 7 6 6 6 0			701 73
	7606757.437-17353260.250	8535870.000	1370.342	017•010	LOT *0C_

3150-6024-R8-000 Page A-42

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Table A-2b.	Reconstructed Reentry Tra	jectory and Asso GEMINI GUICANCE	ciated Faramet	ers (7:18 Rad AM	ar) — Continued 01/10/66
		NASA • MANNED SI	PACECRAFT CENTE	X	
		EC IDANCE TI	IG COURDINATES [me base]		
TIME	×	7	X-D0T	Y-D0T	Z-00T
611.600	760£168.812-17352675.000	005-995799-500	1909.158	758.635	-171-532
512-600	7605803.250-17352011.00	J E535662.500	1329.934	521.243	-38.666
000.619	7611135.937-17351458.00	0535625.750	1294.665	530.623	-75-527
714•0CO	7612765.187-17350826.00	0 8535502.500	1811.652	729.631	-185.788
	(c14023.875-17350237.75	0 8535437.375	1341.801	551.636	-55.454
000 A 10	1612258-437-17345686.50	0 8935366.750	1152.376	511.153	-45.343
	ctc>c0.550.525-17345140.250	0 8535348.E75	826.579	1570.375	-526.555
	/e1/306-500-17347771-750	000-6464659 (1352.981	528.444	-95.242
	1018/39+500-17347724-250	0 8535140.125	1412.136	173.858	116.909
	1620147.437-17347406.250	6535157.375	1739.771	210.639	23.645
000-126	/622050.000-17346754.750	0 6535062.375	1354.779	605.673	-66.600
000 000	1622292.931-17346257.500	9535045.875	1166.155	552.712	-30.094
	/c 240 55.000-1/345871.500	0535111.250	1345.734	576.327	-50.991
	10.6055.517-17344909.000	8934807.750	4566.441	1617.209	-815.573
	1628235+812-11344238+000	8534684.375	1033.808	448.671	50.008
	1054118-315-1/343815-500	8934732.675	743.125	372.699	143.360
	00.53654511-616-5216201	8535462.125	822.209	419.003	85.152
	151-34-000-1/343168-750 7433737 243 134 134 135 155	£534990.125	1314.778	558.737	-29.627
	1032131+002-111342376+250	8534793.250	2811.283	700.301	-150.651
	1000484747777777777777777777777777777777	8534496.625	715.502	364.765	93.571
	7635666 431-1/3410(3.750 763666 212 350666 250	E534651.875	1244.990	565.359	91.627
033.000	16326666917-11340680°250	E534627.000	904.149	417.866	53.113
	NG7*77604617_778*8841681	E534814.750	-4175.956	-1147.561	1285.665
	103/066443/-1/340265.750 3440465 433 43655555 555	£535180.375	3476.415	1245.237	-569.582
	1040052.43/-17338572.250	8534566.675	1680.582	683.454	-111.370
	1042U85.15U-1738375.50U	8534552.375	940.972	542.592	83.170
	1044118-08/-1/337564-750	6534396.375	2218.135	860.562	-188.425
	1644653.1E/-1/337262.500	8534575•625	612.460	377.489	37.820
	1043951.437-17337214.000	6534529.125	-92.823	474.275	139.012
100-146	100°63/67-1133/660000	E535274.250	1362.816	400.991	152.172
	DDG • 8450557 T_DC7 • 1 DOLLO1	8535441.125	1016.338	96.188	361.861
	000-++629FF1T-C16+0C00401	8935606.000	1243.060	46.702	-1060.449

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Table A-2b. Rec	constructed R	eentry Traje	ctory and As	ssociated Fa	rameters	(7:18 Radar) — Continued
	61	-7 RE-ENTRY RA	DAR 7.18				
TIME FRUM LIFTOFF (SECCADS)	INERTIAL VEL+ Magnituge (F1/SEC)	RELATIVE VEL. Magnitude (fi/sec)	INERTIAL FLT. PATH ANGLE (DEGREES)	INERTIAL Heading angle (degrees)	ALTITUDE (FEET)	GEODETIC LAT. (DEGREES)	GEODETIC LONG. (DEGREES)
100 1000000	1 - CAE 7 1	14086.7	2.255	107-217	171463.5	26.224	-73-559
10245427877	1.566.9	16239.2	5.926	104.202	172402.5	26.213	-73.511
1105504.781	17856-7	16510.4	-4.714	101.493	171967.5	26.203	-73.463
110567,581 110567,581	17863-2	16512.9	-3.172	101.446	170633.2	26.193	-73.416
1100509.081	16540-1	15205.7	405	104.953	169437.7	26.183	-73.367
11072706555 11005555.381	17849.2	16499.0	-3.804	101.114	169959.0	26.172	-73.322
1 1 0 0 4 1 0 - 2 4 0 4 0 4 0 4 0 4 0 4 0 4 0 4 0 4 0 4	16694.0	15358.5	-4.511	103.497	168655.2	26.162	-73.275
102 1070011	2007 CECCI	16405-2	8.025	103.266	168109.5	26.151	-73.229
102410211	16968.3	15625-0	-3.035	102.658	168763.2	26.141	-73.162
1100403 341	14124-3	14794.3	-4.386	104.424	167604.0	26.131	-73.137
1020020011	17151.4	15804.1	-3.746	101.749	166445.0	26.121	-73.092
110000505050505050505050505050505050505	C-E9991	15328.7	3.636	103.986	166814.7	26.110	-73.046
1100404 301	5-25-1	14896-4	-3.755	102.982	166047.2	26.100	-73.001
1106407 301	14187.3	14848-8	-2.963	103.506	165852.7	26.090	-72.957
1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		15066.5	-3.937	102.562	164722.2	26.080	-72.914
1100400.281	15483.1	14153.0	-3.827	104.599	163591.0	26.070	-72.870
1189610-281	16400.5	15060.4	2.953	103.282	163394.2	26.060	-72.825
1185611-281	15632.1	14296.4	.110	104.276	162413.5	26.050	-12.183
1185612-281	15603.5	14273.5	3.404	104.765	162269.2	26.040	
1185613-281	14817.2	13451.9	-3.703	105.346	161427.0	050.05	160-71-
1100414-381	14572.5	13642.7	-2.867	104.817	160500.5	26.021	-72.655
1185415-281	15600-6	14259.5	-3.222	103.153	159528.5	26.011	-72.613
1 1 8 9 6 1 6 - 2 8 1	15893.3	14548.0	.111	102.788	159312.0	26.001	716*71-
1186617.281	15805.3	14464 .8	2.975	103.264	158620.2	25.992	160.21-
1165618-281	14795.2	13465.3	-3.257	104.206	15817 <u>0</u> •5	25.982	684*7/-
1185619.281	15453.1	14136.0	7.468	104.382	158197.7	22.972	
1189620-201	15294.4	13950.5	-3.053	102-783	157500.7	504.07	
1185621-281	15412-2	14066.4	146.6-	102-30B	n•/10061	604 +07	100.21-
Table A-2b. Reconstructed Reentry Trajectory and Associated Parameters (7:18 Radar) - Continued

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	61	I-7 RE-ENTRY RA	CAR 7.18				
TIME FROM LIFTOFF (Seccncs)	INERTIAL VEL. Magnitude (FT/Sec)	RELATIVE VEL. Magnitude (FT/SEC)	INERTIAL FLT. Path angle (Cegrees)	INERTIAL Heauing angle (degrees)	ALTITUCE (FEET)	GEODETIC LAT. (DEGREES)	GEODETIC LONG. (DEGREES)
189622.281	15031.3	13689 - 7	-3-612	102.956	155750-5	25-944	-72.329
189623.281	14505.2	13168.5	-3.268	103.831	154885.7	25.935	-72.289
189624.281	14635.1	13295.3	-3.405	1103.311	154059.5	25.926	-72.250
185625.261	12763.7	12439.2	2.502	105.745	153466.2	25.917	-72-212
.189626.281	14999.8	13652.8	-2.837	102.269	153108.7	25.907	-72.174
189627.281	14073.2	12736.2	-2.848	103.878	152336.2	25.898	-72-136
189628.281	14096.9	12758.2	-3.216	103.538	151563.2	25.889	-72.098
189629.281	14093.9	12753.3	-2.720	103.354	150808.2	25.880	-72.061
.189630.281	14210.4	12867.1	-2.651	102.927	150132.5	25.872	-72+024
189431.281	14418.5	13071.8	-3.167	102.246	149434.5	25.863	-71.988
189632.261	12888.5	11558.7	-2.351	104.994	148755.2	25.854	-71.952
189633.281	13705.2	12363.9	-2.886	103.212	148090.5	25.846	-71.915
.189634.281	13324-2	11985.1	-2.289	103.658	147406.2	25.837	-71.881
189635.281	13197.1	11658.7	-2.671	103.673	146836.0	25.828	-71.845
.185636.281	13221.9	11881.8	-2*995	103.401	146243.5	25.820	-71.811
.185637.281	13128.9	11786.3	-2.756	103.359	145628.2	25.812	-71.776
.189638.261	12868.2	11529.2	-3.301	103.475	144849.5	25.804	-71.742
189639.281	12858.0	11528.3	-8.252	102.876	144142.7	25.795	-71.708
.189640.281	1288¢.3	11544.3	-2.664	103.164	143124.7	25.787	-71.676
189641.281	12347.4	11609.0	-2.446	103.748	142595.5	25.779	-71.643
.185642.281	12168-4	10771.7	-2+202	104.038	141804.7	25.772	-71.610
.185643.281	12295.5	10955 . 5	-2.528	103.490	140952.2	25.764	-71.579
.189644.281	12213.7	10872.5	-2+056	103.370	140450-0	25.756	-71.547
.185645.281	11538.1	10203.4	641	104.439	138315.2	25.749	-71.516
.185646.281	11892.7	10552.2	-1.701	103.510	137905.0	25.741	-71.486
.189647.281	12554.6	11206.5	-1.695	102.321	137509.2	25.734	-71.454
.189648.281	11226.2	5891°3	.245	104.428	137418.2	25.726	-71.425
.189649.281	11478.7	10137.9	-2.025	103.431	137105.5	25.719	-71.395

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Table A-2b. Rec	constructed R	eentry Traje -7 RE-ENIRY RA	ctory and As 0AR 7.18	ssociated Pa	rameters	(7 : 18 Radar	·) — Continued
TIME FROM LIFTOFF (Seccncs)	INERTIAL VEL. Magnitude (ft/sec)	RELATIVE VEL- Magnitude (FT/SEC)	INERTIAL FLT. Path angle (degrees)	INERTIAL Heading angle (degrees)	ALT ITUDE (FEET)	GEODETIC LAT. (DEGREES)	GEDDETIC LUNG. (DEGREES)
1189656.281	11567.8	10224.7	-2.177	103.052	136671.5	25.712	-71.366
1185651.281 1189453 261	11495.8 10981.3	10164.8 9641.4	-13.005	102.012	134588°2	25.698	-71.310
1185653.281	10910.6	9583.9	-9.015	102.747	134048.2	25.691	-71.282
1189454-261	11283.3	9938.3	-1.754	102.792	133302.2	25.684	-71.254
1189655•281	10389.3	905U.7	-2.043	103.690	132990.0	25.677	-71.228
1189656+281	16267.0	8929.7	-3.01E	103.708	132398.5	25.671	-71.200
1189657-281	10433-7	9100.3	-7.158	102.756	130802.7	25 • 664	-71.175
1185658.261	10353.9	9013.4	-3.457	103.084	129621-2	25.658	-/1.149
1189659•261 1185460 201	10300.8 5826.8	2-8678 7-848	-1.235	103.508	129042.2	25.645	-71.099
194000011 1940612	5805.5	8465.7	-2.591	103.356	128164.2	25.639	-71.074
1185662-281	10353.7	4-2406	-14.122	101.416	126663.2	25.633	-71.050
1189663-281	5712.2	8369.5	-2.006	103.066	125543.2	25.628	-71.026
1189664 • 281	9147.4	7.909.7	-1.442	103.771	125309.5	25.622	-71.002
1189665•281	8982.6	7644.5	-1.504	103.686	124168.7	25.616	-70.980
1185666.281	8257.5	6926.1	-1.286	104.558	123875.5	25.610	-70-957
1189667.281	8648.5	7505.7	-1-523	103.501	123076.2	25.605	-70.934
1189668•281	8840.6	7500-4	-1.167	103.398	C-868221	25.502 25.502	109114-
1189669-281	8611.66 0.06	7160 0	576°T-	103.633	120062.2	25.589	-70.871
11276/U.\$21	0.0100	7803.1	-1.12	102.596	120748.0	25.583	-70.850
11896772.5A1	E814.0	7474.2	-5.384	102.406	120104.2	25.578	-70.831
1189673.281	5899.8	8673.1	-23.989	99.627	119189.7	25.573	-70,811
1185674.281	9082.1	7.734.7	-1.285	102.283	118249.7	25.568	-70.790
1185675.281	1872.6	6533.4	.172	103.444	117380.0	25 . 563	-70.771
1189676.281	8621.4	7448.4	-27.964	100.088	116621.2	25.559	-70.752
1185677.281	£439.2	7094.1	210	1U2.630	115700.0	22.24	-10.134

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Table A-2b. Reconstructed Reentry Trajectory and Associated Parameters (7:18 Radar) - Continued

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GT-7 RE-ENTRY RADAR 7.18

TIME FRCM LIFTGFF	INERTIAL VEL- Magnitude	RELATIVE VEL. Magnitude	INERTIAL FLT. Path Angle	INERTIAL Heading angle	ALTITUDE (FFFT)	GEODETIC LAT.	GEODETIC LONG.
(SECCACS)	(FT/SEC)	(FT/SEC)	(DEGREES)	(DEGREES)			1 DEGREES
1185678.281	1872.3	\$\$\$2°6	-13.981	101.584	115094-0	25.550	-70.717
1189679.281	7508.1	6173.7	-6.528	102-477	113968.2	25.545	-70.698
1189686.281	7067.2	5728.4	-2.466	103.112	112392.5	25.541	-70.682
1189681.261	7227.4	5896.7	-7.925	102.176	111560.2	25-537	-70.665
1189682.281	6629.3	5293.1	-+952	103.567	111187.0	25.533	-70.649
1189683.281	7853.5	6636.2	-24-043	100.130	109636.2	25.529	-70.632
1189684.281	7252.0	5907.4	855	102.464	108410.7	25.525	-70-617
1189685.281	7033.9	5690.8	150	102.688	108316.7	25.521	-70.601
1189686.281	5965.0	4629.4	-1.478	103.391	107185.0	25.517	-70-587
1189667.281	6215.1	4889.4	-8.385	102.322	106341.7	25.513	-70-572
1189688.281	5833.7	5-2644	-3.795	102.858	105144.2	25.510	-70-557
1189689.281	6079.2	4738.4	807	102.744	105104.2	25.506	-70-544
1189690.281	5717.1	4420.0	-13.534	101-872	104385.7	25.503	-70.531
1189691.281	6650.9	5314.6	-7.361	101.427	103386.7	25.500	-70-518
1189692.281	6219.5	4877.2	1.655	102.480	101900-0	25.497	-70.505
1189693.281	6124.2	4779.5	-1.584	102.084	101816.5	25.493	-70.492
1189694.261	5133.9	3796.2	• 31 4	102.853	101508.2	25.490	-70.479
1189655.281	5210.5	3870.6	243	102.567	59934.2	25.487	-70-467
1189656-281	5088.7	3745.0	.067	102.544	99898.2	25.484	-70.457
1189697.281	5604.3	4260.6	-2.767	101.855	99162.0	25.481	-70.446
182.8202811	5271.2	3929.5	-3.625	101.852	98181.2	25.478	-70.434
182-559681T	4890.3	3549.1	-2.934	101.684	97411.5	25.476	-70.423
182-00/6811	5178.4	3945.6	-21.302	94.848	96942.0	25.473	-70.414
1169/01.281	4188.6	2854.0	1.852	102.565	96068.0	25.470	-70.403
TR2.20/ 6911	4687.3	344.3	082	101.871	95264.5	25.468	-70.393
185.607 981 1	4.646	2160.7	855	102.280	94235.7	25.466	-70-364
1189704.281	3339 . 3	2008.5	-2.484	102.083	92844.7	25.463	-70-375
1189705.281	3863.2	2553.3	-10.862	100.760	92598.0	25.461	-70.366

CONFIDENTIAL

3150-6024-R8-000 Page A-47

Table A-2b. Rec	onstructed R	eentry Traje	ctory and As	sociated Par	ameters	(1:10 Kadar	
	61	-7 RE-ENTRY RA	DAR 7.18				
TIME FROP LIFTCFF	INERTIAL VEL. Magnituce	RELATIVE VEL. Magnitude	INERTIAL FLT. PATH ANGLE	INERTIAL heading angle	ALT 1TUDE (FEET)	GEODETIC LAT. (DEGREES)	GEODETIC LONG. (DEGREES)
(SECCICS)	(FT/SEC)	(FT/SEC)	(DEGREES)	(DEGREES)			
tot svevett	1 0011	2271-2	19.553	100-127	92165.0	25.459	-70.358
192.0010011	1-0001	3683.3	-13.763	100.054	90968.2	25.457	-70.349
1189708.281	52103	E.1791	-17.850	99.856	89694.2	25.455	-70.341
1140709-281	3224-8	1887-9	925	101.396	88151.0	25.453	-70.333
185-0126811	3761.0	2588.1	-24.518	98.778	87509.2	25.451	-70-326
1189711-281	5382.2	4266.5	-30.780	97.896	86440.7	25.449	-70-316
1189712-2811	3583.7	2239.2	306	100.823	85462.7	25°448	-70-312
1189713-281	3189.7	1848.8	.467	100.877	84996.7	25.446	-70-306
1189714-281	4265.5	2918.1	.405	100.912	84127.5	25.444	-70-298
1189715-281	3522.5	2176.6	.140	100.573	83528.7	25.443	-70-292
1189716-281	2976.6	1637.8	2.764	100.487	82467.0	25°44I	-70.285
1189717-281	3223.0	1874.8	342	99.924	82410.5	25.439	-70-279
1185716-281	5085.4	4594.6	-61.133	90.295	81586.0	25.438	-70-273
1189719-281	5021-7	4051.2	37.265	104.270	77283.0	25.437	-70.268
1189720-281	3346.6	2290.5	29.457	102.612	81448.5	25.435	-70.263
1185721-281	7485.5	6751.5	-53.280	93.547	80788.0	25.433	-70.257
1169722-281	6005.5	5162.3	45.165	104.807	77564.2	25.433	-70-253
1189723.281	6082.2	5544.7	59.441	107.463	79628.2	25.431	-70.249
1189724-281	7695.7	7055.4	-57.747	92.186	78293.0	25.430	-70.243
1189725-281	2765.2	1442.4	-8-974	98.283	74926.0	25.430	-70.240
1185726.281	1989-8	651.4	1.623	98.112	75069.5	25.428	-70.234
1169727_281	1497.4	196.9	1.662	96.187	75096.5	25.427	-70.230
185.8728.1	2310.3	966.1	3.038	98.479	72716.2	25.426	-70-226
1189729-281	1683.3	452.8	10.805	96.855	72705.2	25.425	-70.223
1169730.261	2152.7	832.1	5.776	98.855	69665.2	25.424	-70.218
1189731.281	2404-0	1051.1	-1.921	97.698	70069.2	25.424	-70-216
1169732.261	2833.5	1481.6	526	98.829	70040.5	25.423	-70-212
1185733.281	5995.4	5306.5	-54.111	94.126	69381.7	25.422	- 70 . 209

Table A-2b. Reconstructed Reentry Trajectory and Associated Farameters (7:18 Radar) - Continued

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	19	-7 RE-ENTRY RAI	CAR 7.18				
TIME FRGM LIFTCFF (SECCADS)	INERTIAL VEL. Magnituge (F1/SEC)	RELATIVE VEL. Magnitude (ft/sec)	INERTIAL FLT. Path angle (degrees)	INERTIAL heading angle (degrees;	ALTITUDE (FEET)	GEODETJC LAT. (DEGREES)	GEODETIC LONG. (DEGREES)
1189734.261	1705.5	610.5	17-014	CC0 70			
1189735.281	2055.3	707.0		674.14	0.1000	024-62	-70.204
1162736 201				20.010	0.0009.0	25.420	-70.204
107-0714071		· 19/7	-57.636	88.898	68673.7	25.419	-70.100
135.75/9411	3183.5	2056.8	-26.712	96.493	67922.0	25.410	
1189738.2£1	1469.3	167.8	-2.155	95.380	66426.0	26.418	
1189739.281	1610.2	290 - 4	-4-035			BT4.67	451-02-
1189740.281	1316.2	131.0	12-240		7*06400	114.62	-70.191
1185741.281	8 555C				0.00400	25.416	-70.168
1 1 80 7 4 7 5 5 1			C71.	56. 195	66461.7	25.416	-70.187
707°7'1'00'1	T • 0767	4-610	-21.140	92.083	66293.5	25.415	-70.184
192°5414571	6758.1	6629.3	-76.727	75.474	64851.0	25.414	-70-191
182.44/4811	5985.6	4650.9	6.967	101.427	61235.0	25.414	
189745.281	2448.4	2057.7	-57.149	88.992	60028-0		
l 189746.281	5751.8	5540.9	-74-132	80.845	44305 F		
1189747.261	5320.3	4942-9	45.704	104 401		214+22	
1185748。281	3770.0	0 2045			0+0000	216.62	-70.175
185749-281				012-401	2-41020	25.411	-70.171
100750 301			555+27-	74.653	65501.7	25.410	-70.168
	10/3.0	1299.8	-43.894	91.271	57152.0	25.411	-70-149
T22+TC150T1	1375.1	405.2	15.941	95.667	56587.5	25.411	
185.2616811	6169.8	6172.6	82.974	115.883	52320.2	25.411	
182-5622811	5867.2	5547.0	-69-915	87.677	53861.2	25.210	
195.957.681	2275.1	1838.4	53.467	98.052	52452.5	25.410	
1185755.261	1834.8	0.693	17.302	97.930	54051.7		
189756.281	3841.6	3245.3	5 4 4 9 T				001.0/-
185757-281	5102.5	1344 6			1.12240	25.408	-70.160
185758 JA1				467 ° 66	4-2506+	25.409	-70.158
			41-920	103.173	51668.2	25.408	-70.157
102-122-12011	201112	1468.5	-41.676	91.328	50349.7	25.407	-70-156
TRZ*09/6RT	5587.8	5952.1	81.393	-82.748	46644.0	25.407	-70.159
185761.281	2555235.3	2996605.2	033	-82.510	48634.7	25.478	

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ociated Parameters (7:18 Radar) - Continued

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3150-6024-R8-000 Page A-50

GEODETIC LAT. GEUDETIC LUNG. (DEGREES) (DEGREES) -70.134 -70.132 -70.132 -70.132 -70.132 -70.130 -70.129 -70.129 -70.129 -70.129 -70.128 -70.126 -70.128 -70.126 -70.125 -70.126 -70.12 255.999 255.99 ALTITUCE (FEET) INERTIAL Meading angle (degrees) 96.645 91.269 92.269 92.269 92.317 92.317 92.554 92.602 92.612 92.612 92.616 92.612 92.616 92.616 92.616 92.616 92.616 92.616 92.616 92.512 92.616 92.516 92.516 92.516 92.516 99.517 99.517 99.557 99.557 INERTIAL FLT. Path angle h (degrees) **KACAP 7.18** RELATIVE VEL. Magnitude (FT/SEC) GT-7 RE-ENTRY 2335.5 2136.7 131.9 131.9 131.9 656.7 663.6 663.6 663.6 663.6 663.6 663.6 663.6 132.4 658.5 132.4 658.6 558.7 558.6 558.7 558.6 558.7 558.5 558.7 558.7 558.5 558. INERTIAL VEL. Magnituce (ft/sec) 2792.5 2936.5 2936.2 2944.0 1501.5 2061.5 2061.5 1960.9 1960.9 1960.9 1960.9 1960.9 1960.9 1960.9 1960.9 1290.9 1200.9 1200.9 1000.9 1000.9 1000.9 1000.9 1000.9 1000.9 10 TIME FRCM LIFTGFF (Seccnds)



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3150-6024-R8-000 Page A-51

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	19	I-7 RE-ENTRY RA	CAR 7.18				
TIME FROM LIFTOFF (SECCACS)	INERTIAL VEL. Magnitude (FT/SEC)	RELATIVE VEL. Magnitude (FT/Sec)	INERTIAL FLT. Path angle (degrees)	INERTIAL Heading angle (degrees)	ALTITUDE (feet)	GEODETIC LAT. (DEGREES)	GEODETIC LONG. (DEGREES)
185818.281	1817.7	449.0	- 007	93.881	35746.5	25.394	-70.125
185819.281	1089.4	334.2	-3.702	195.58	35745.7	25.394	-70-125
185820.281	2386.7	1018.5	• • 0 •	95.199	35771.5	25.394	-70-122
185821.281	720.4	677.2	-5.758	83.903	1.17766	25.394	-70.125
189822.281	502.9	1366.7	-46.886	18.035	35627.2	25.396	- 70.131
185823.281	1428.7	239.4	9.277	87.576	35586.5	25.397	-70.135
189824.281	1083.1	636.5	24.296	78.908	35650.2	25.357	-70.136
189825•281	1634.6	1177.3	-1.307	134.967	35966.2	25.397	-70.136

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3150-6024-R8-000 Page A-52

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Table A-2c. Reconstructed Reentry Trajectory and Associated Farameters (IGS)

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PFFNIRY SFGMENT & GFM1N1-7

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EARTH	

		EART	H CENTEREN INERTIA COMPAINATE SYS	NL GRESWUTCH Stew		
TINE	¥	>	7	YDOT	YDDT	1001
(کور)	(ct)	(FT)	(FT)	(FT/SEC)	{FT/SEC}	IFT/SEC1
1794.1875	8567330 . FA	-14066783.00	00*525205	4600 . 88	3286.55	-1-2421-
1704.4875	מ58350 0. FÛ	-16057170.75	21.1205200	4374.J7	IL EUGE	-1478.15
1700-0625	8598710.00	-1404667.75	9019144.12	5058.92	3115.16	-1610.77
52 E 7" I U 8 I	P612294.75	-14937774.00	9015401.37	5702.06	11.7505	-1543.12
]¤O₂.¤]25	9675727 . 87	-16077200.75	90]18]8,42	5577.R3	91 2206	-1474.00
1204.1575	ακ3βες2°β7	-1 / 6 2 2 4] 2 * 75	9008306.75	5272.1A	7 81 . 90	-1407.53
1908.6975	9461422 75	-16016345.00	a()14055,37	5023.77	19 2770	-1245.57
1411.0625	R462950.00	-140000077.75	900] 8P9. R7	4483.27	2423.27	-1735_9E
1913.4375	9473RN0.12	-16903840.75	8999024.75	4452.40	7544.31	-1176.90
1910.1975	R603010.75	-)FRC211F.07	7072774 87	4017.70	07 0020	-1042.12
1820.6975	R 703703.57	-16884722.75	71,114,77	3800.15	79.2525	-1000 28
1823.0625	9712516.12	-] f. B. R. T. G. T. G. T. S.	SCRR781.12	112,125	2251 45	-955,58
1925.4375	R770877.75	-] fR75525.75	R096572.12	3474 64	7183.10	-003 TK
1827.8125	4778794.AF	-16870417.75	4944P5.A7	3246.51	A14.1 8	- 95 2 07
1820.1875	8736307.42	-16865441.00	ACR241A. 25	2077.08	2055, AR	-P04-74
1 R 3 7 , 4 R 7 5	P743721.37	-16840465.25	ROADAOA. 37	7857.1A	1040.07	TT. 207-
1835.0625	A 75.0335 EO	-16P55974.00	ROTROAI. 47	7712.57	1 882.27	-FPE 35
3252 4375	R 756619 27	-16857514.50	8977348°75	7578.28	1 R 7 0 . 74	
1820.8175	R747589.27	-]6547237.50	R975552.67	31°077c	00.1771	50-114-
1942.1575	9768266 . 75	-]/P443088.75	00°277768	01°2220	1721.44	- 575 B7
1944.6875	a773962 . 2e	-16838820°25	9973037 . 75	25°725c	1434.03	-54B,70
1847.0625	A779]30.25	-]6834866.50	RG71766.00	2127.34	1 650. 01	-= 22.70
1940.4275	9724045.25	ÚU 17012871-	RATUERS. 27	2011.56	1570.60	-472.16
1941 8125	el. Jergare	-16627350.00	8040407 ,75	72°UE01	1 5 3 7 . 5 7	20 397-
1854 JP75	A703274.75	-]FP23737.50	A068428.5G	1 R57. 66	1602.75	LČ 2.7-
1856.6875	P 707787 00	-)6P20015.25	a967377 25	1780.55	1474.71	20 917-
1859.0625	8901937.60	-]48]4501.DO	9044475 CM	1710.R2	1404.79	-270°48
1961.4375	RAM5930, P7	-]6813280.50	RCFSF41 . 47	1451.04	90°1951	31.445-
1843.8175	0400790.62	-) < F10031.00	gok4403 K2	1509.40	ושקניטל	740°071-



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Reconstructed Reentry Trajectory and Associated Parameters (IGS) Continued	GFWINI-7 PEFNTRY SFGMENT 4	F≜RTH FENTFPFN INERTIAL GREENWIGH Frorninate system
Table A-2c.		

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	>	>	7	TUUX	YUGT	7001
(<u>1</u> 25)	והדו	(FT)	(FT)	(FT/SFC)	(FT/SEC)	(FT/SFC)
3101	2013633 °6	-16806840.75	75,0795408	1552 42	57 1201	-355° 75
	C1 7722103	-1603533.25	P962045.75	1512,10	228221	21,152-
	Ta 0100000	-16PUC420.50	R967750.75	1480.34	12,1451	- 30× 00
1073 4375	25.902.20A	-16707395.25	ACE1570.50	1440.77	1273.04	-203,53
1075 0175	0197910.47	-14794381.75	BCADP7A.O 0	19-571	1263.59	-207.27
1979 1975	2421166.67	-11701288.75	9040179.75	1400-51	1257.79	£2°0°6~
1995 4375	9 8 4 1 0 7 8 5 0	-16702603.75	8958756,00	76 7261	1144.17	-239,95
1016 6875	981206.75	-14740511-12	80F7A45 550	1233.93	951.72	-104.32
1073 8125	RAGOOP6.42	-14742823.50	8952156.25	96.1251	025°53	-A7.]A
1078 5675	9895016.75	-16738421.76	8951755.52	28.7r21	001.00	[3]]
1026 B175	8904514-47	-14731765.25	8951 224 BT	1244.51	07°300	
1020 1875	9007845 . 1 7	-14729405.75	89510A4.12	1240-07	01.010	16"24-
1042 0475	9012009 17	-16775149.00	A950775.27	1230.12	918.10	- 6 4 . 24
1065.0675	8928856.00	- 167 4414.25	R950057.75	1252.19	R70.R1	
1057 4275	79.1691508	-14712347.75	R949927.R7	1245.43	86°.40	-58,17
1050 8175	01.774rpa	-1K710203.K2	80497RJ.97	1242.72	P68.79	-61.44
1047,1875	75.717208	-14708273.97	894C632 . 50	1 224 553	P45.73	-63,53-
1044 5475	4047447 97	-14706140.50	89494RF , 75	1229.95	71°47	-60.42
1067 0675	24.177 . 25	-16704007.97	8049354.30	1240.0R	F50.70	-44.46
1049.4375	8946570.50	-1670]984.12	8949750.75	1235.10	P 5 2 4 P	-42.71
1074.1875	9957576.27	-16607912.12	894c040°75	1270.54	P62.06	-4].6R
1079.0425	958541.75	-]6402747.12	A94A878.00	1237.06	045°78	-28.79
2010-1875	900P614 50	-16670P01.75	8049508 . 87	1330°22	624.63	
2012.5625	001805.00	-16665308.75	ROLOKAR. 75	1330.54	F 2 4 ° E O	4 H • 4 4
2015.0625	9005104.50	-16467743.75	B040725 . A7	1208.9A	25.53	21.26
2017.4275	900P221_62	-16666297.12	8040781 . 97	1315.91	E94,0]	17.47
2010-8125	9011341.0E	-]6664886.75	8940804 . 50	Él"LÌEL	597.77	00° E
2022 1875	9014435,25	-]6663485.67	8049786 . 52	1294.35	5 5 1 ° 1 5	- 20,00
2024 . 5625	2017497.A7	-16662098.42	4949700.50	1774.33	Eq.), OS	-47.13

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3150-6024-R8-000 Page A-54

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Table A-2c. Reconstructed Reentry Trajectory and Associated Parameters (IGS) -- Continued

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CFMINI-7 REFNIRY SFGMENT 4

GREENWICH	× u
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CENTFRED	
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			CURDINATE SYS	TEM		
•	,	>	7	XDUT	YOUY	7007
(SEC)	(FT)	(FT)	(FT)	(FT/SFC)	(FT/SEC)	(FT/SFC)
		35 30 20 71	8045670 47	1274.67	5.09.3]	-5P.84
2027.0625	1020676+62			1243.67	542.43	06.58-
2020.4375	00.1075500			1266.60	525 77	-115.50
2031.4125	9074671.P7		0000830 EV	1229.26	528.64	-151-99
2034.5625	00°2536806			1224.42	404 88	-172.51
2039.0625	9015621.42	-]6656401.07		1208.46	479.66	-227 . 85
5214 - 2702			8944011 A7	11 84.70	443.59	-264.94
2048.5675	-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1			1157.01	440.21	7U°04.5-
2055.B125	9055634.12		00.5107.52 60.5103 60	1167.97	205.69	35.355-
2047.0375	90-8010-00			5 - U - I I	296.44	70.075-
2060.5625	9041093.47			74 1511	40,905	- 305 T4
2063.0625	78.FF0EA09	-] + + 4 3 4 4 8 8	1 H 901 105 8		207 04	-412.70
2065.4375	9066614.67	-16642728.12	4 4 4 7 7 C 4 4 4			20 7 62-
20F7_8175	9063775.00	-1464]842.00	R036736.P7	62°91 []		7 TO 01
2070-1875	2071001.75	-16641011.75	99787450 SQ	1041.67		
2075 0475	017730.87	-16639318.00	8925040.77	1002.75	× 1 • 0 4 ×	
707 × 275	0070815.87	-16638496.12	9934722 ,12	1076.92	243°U3	25*224-
	0087366.75	-16637728.25	00°237568	1070.71	103°60r	1 4 6 F ° F F
	00010000	-14626789.75	4010700.25	1045.96	06.905	- E B 2 • E 3
	29 000000 C9		Rapapal - FU	1045.97	204°37	-+0H.45
	0007553 75	-14624874.50	9077830.75	1036.44	240.92	-621.63
	0005011 25	- 14636254 - 87	ag74234 .62	1032 A4	260° 06	UE " HE J -
22 F2 • 1667	000766 13	-14672630-17	9024701 A7	1024.50	257.52	- 440.40
SUDA ELSE	0000846.27	C7 70022791-	99731 PQ 75	1004.92	251.56	1 × 8 × 1
		26 20015221	9010753 DO	1005.1P	219.60	- 72] • 63
c/01.		114430041 36	8916213.12	04.40	207.73	-76P. R2
741.4014			PQ14357.27	049.80	201,0R	40° E01-
C.G.C. B.D.C.			801764 00	974.45	170.38	-P01.30
-120°0112	10°//14/in	00 000000000	01 07 70 10	C42.92	148.28	-н?5. А5
7754°E11C	0, 1,4,1,10		5 4 UE 70 UE	04.540	161.22	- P£7.07
7115.8125	73.4188110	-16+24152405				



1 adle A-20	c. Keconst	ructed Keentry	Trajectory and	Associated Pa	trameters (IGS	i) — Continued
		GFMINI-7	REENTRY SEGMENT 4			
		FART	H CENTERFO INFRIA Comroinate Sys	I GREENWICH Tem		
TIME (SEC)	X (FT)	Y (FT)	2 (FT)	YDNT (FT/SFC)	YNNT (FT/SFC)	ZNQT (FT/SEC)
2119.1875 2120.5625	51.3701516 51.3705519	-16628753。62 -16628393。87	8906367,25 8906223.97	942.57 942.52]54。58 148.40	74°70'- 740°44



3150-6024-R8-000 Page A-56

	econstructed Reentry Trajectory and Associated Parameters (IGS) — Continued	CEMINI-J BEENTRY SECHENT 4
-	4-2c. F	
٣	Table 4	

SEGMENT	
REENTRY	
1-11-1	

	6FM	INI-7 REENT	RY SEGMENT 4				
TIME FROM LIFTOFF (SECONDS)	INERTIAL VEL. Magnitude (FT/SEC)	RELATIVE VEL. Magnitude (ft/sec)	INERTIAL FLT. Path Angle (degrefs)	INERTIAL HEANING ANGLF (DEGREES)	ALTITUDE (FEET)	GENDETIC LAT. (DEGREFS)	GEODETIC LONG. (DEGRFFS)
1189677.484	7577.3	6237.1	-5,376	102.196	7.949621	25.561	-70.696
1189679.984	7288.3	5948.5	-5.662	102.068	122143.5	25.551	-70.652
1189682.359	7000.6	5661.1	-5.930	101.928	120421.7	25.54l	-70.612
1189684.734	6716.0	5377.0	-6.215	101.780	118691.0	25.532	- 70.574
1189687.109	6431.1	5092.6	-6.512	101.606	116953.5	25.523	-70,538
1189689.484	6157.1	4819.1	-6.830	101.471	115210.2	25°515	-70.504
1189691.984	5893.8	4556.8	-7,213	101.226	113342.2	25.507	-70.471
1189694.359	550A. F	4171.1	-7. 199	100.485	111634.7	25.500	-70.441
1189696.734	5262.4	3926.1	-7.776	100.664	104441.0	25.494	-70.413
1189701.484	4795.5	3461.8	-8.583	100.172	106539.5	25.487	-70.363
1189703.984	4573.9	3242.1	-9.056	99 ° 891	104739.7	25.476	-70.239
1189706.359	4362.3	3032.3	-9.496	99 . 588	103025.5	25.472	-70.318
1189708.734	4160.7	2832.8	-9 * 6-	99.266	101313.5	25.467	-70.298
1189711.109	3969.2	2643.6	-10.404	98.°10	9960F.2	25.463	-70.290
1189713.484	3787.2	2464.3	-10.880	9A.53R	7.10979	25.459	-70-263
1189715.984	7520.3	2207.5	-11.081	97 . 9A3	96157.2	25.456	-70.246
1169718.359	3372.7	2054.5	-11.532	97.640	94548.2	25.453	-70.232
1169720.734	3277 . 2	1913.1	-11.984	97.283	92949.2	25.450	-70.219
1189723.109	3084.1	1774.1	-12.371	96.935	91364.5	25.448	- 70.207
1189725.484	2955.5	1649.A	-12.767	96.540	99804.2	25.445	-70.196
1189727.984	2844.7	1545.5	-13.347	96.141	BR165.0	いち。ちちい	-70.195
1199730.359	2743.0	1450.6	-13. R6E	95.764	R6602.7	25.44]	-70.176
1189732.734	2595 . 6	1305.4	-13,811	95.248	850R5.0	25.440	-70.167
1189735.109	2508.5	1225.1	-14.227	94.868	83615.5	25.438	-70.]59
1169737.484	2428.3	1152.4	-14.578	94.646	82156.2	25.437	-70.152
1189739.984	2356.9	10°0.3	-15.064	64°.46	R0625.2	25.436	-70.145
1189742.359	2247.2	0.199	-14.740	92 . 952	7971A.O	25.435	-70.139
1189744.734	2183.8	927.4	-15.095	93,646	77863.O	75.434	-70.134

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			- INDERDO AN				
TIME EROM LIFTOFF (Seconds)	INERTIAL VEL. Magnitude (ft/sec)	RELATIVE VEL. Magnitude {FT/SEC}	INERTIAL FLT. Path angle (degrees)	INFRTIAL Heading angle (degrees)	ALTITUOE (FEFT)	GENDETIC LAT. (DEGREES)	GEODETIC LONG. (PriceFes)
1180747.100	2124.6	R77.2	-15-394	93.377	76517.0	25.433	- 20.129
1 1 89749 484	2072.6	R33.0	-15.610	93.099	75194.5	25.432	-70.124
1180751 . 984	2037.2	809.5	-15.108	92.907	73780.0	25.431	-70.120
1189754.359	1981.4	751.8	-15.627	92.560	72474.5	25.431	-70.116
1189756.736	1952.1	730.9	-15.971	92.189	71204.5	25.430	-10-112
1189759.109	1926-7	715.7	-16.255	92.294	69927.5	25.430	- 70.109
1189761.484	1904.5	701.2	-15.498	92.074	6R644.5	25.429	-70.106
1189768.734	1786-2	584.6	-15.341	91.393	64968.0	25.42B	-70.097
1189799.9R4	1561-9	322.4	-10.440	89.400	53155.7	25.427	-70.074
1189807.109	1551.4	4.102	-9-263	89.194	51258.5	25.428	-70-071
1189811.859	1549-1	291.3	-9.300	BB .947	50071.0	25.428	-70.069
1189819-109	1542-1	267.6	-8.315	BB.626	48355.7	25.429	-70.065
1189871.484	1539-5	268.8	-8.456	88.607	47822.2	25.429	- 70,044
1189826.359	1542.6	276.6	-8.690	RR.532	44707.5	25.429	-70.062
1189838.359	1526.2	229.0	-6.950	R9.017	44196.2	25.430	- 70.057
1189840-734	1520.0	227.3	- 7,080	99.082	43754.5	25.431	-70.056
1189843.109	1517.2	227.0	-7.169	89.182	43307.2	25.43]	-70.055
1189845.484	1509.2	223.8	-7.265	89.239	42856.0	25.431	- 70.055
1199847.859	1503.8	728.4	124-2-	39.010	42397.0	25.431	-70.054
1189850.359	1504.2	204.2	-6.394	A8.860	415.2.2	25.431	19.053
1189852.734	1501.3	205.2	-6.514	BR.725	41541.2	25.431	70.052
1189857.484	1503-6	214.6	-6. RKA	88 , 511	40710.0	25,432	-70.050
1189862.359	1498.8	195.6	-6.022	R8.269	39899.7	25.432	-70.049
1189893.484	1481-0	144.3	4.051	8A.943	39073°5	25+435	-70. C
1189895.859	1472.4	127.9	3.593	9.611	39307.5	25.436	-70,020
1189898.359	1450.0	101.5	2.945	90.486	34517.7	25° 436	-70,038
1189900.734	1444.2	119.4	174.5	011.10	39726.2	25.435	-10.038
1189903.109	1438.9	115.5	3.739	47.624	39056.2	25.435	-70,037

Table A-2c. Reconstructed Reentry Trajectory and Associated Parameters (IGS) - Continued

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3150-6024-R8-000 Page A-58

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IGS
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	GFM	IINI-7 REFNT	RY SEGMENT 4				
TIMF FRCM LIFTOFF (SFCONOS)	INFRTIAL VFL. Magniture (FT/SFC)	RFLATIVE VEL. Magniture (FT/SFC)	INERTIAL FLT. Path angle (dfgrees)	INFRTIAL Heading Angle (degrees)	ALTITUDF (FEFT)	GENNETIC LAT. (NEGREES)	GEONFTIC LONG. (DEGRFES)
118005.484	1421.4	107.8	3.284	97.447	40164-0	25.435	750.07-
140007. 859	1403.1	104.0	2.781	93.353	40341.0	75.434	- 70-03-7
199010.359	1 3 49 2	137.1	3.584	94.389	40534.2	25.434	-70.037
467.51998	2-2221	1 50° R	3.212	295.782	40728.2	25.423	-70-037
189915.109	1361 . A	i 1 i 2 i	2.590	96.523	40892.2	25.432	-70.037
58.219081	1346.7	200.6	1.906	58.082	41143.0	25.420	-70.037
199022.359	1333.7	23R . 3	2. KSR	99.505	41275.2	25.42R	-70.038
180927.109	1320.0	2°0°2	1.865	101.910	41521.0	25.425	-70.039
189931 . A59	1296.1	0°64E	2.107	104.097	41733.0	75.421	-70-040
189929.109	1279.4	392.5	0:5.	106.349	41950.0	25.415	- 70. 044
199941.234	1273.6	1.15	2.017	107.988	42010.5	25.412	-70.045
189943 . 859	1263.3	461.2	. 010	109.404	42093.0	25.409	-70.046
189946.359	1263.3	4A] . 7	.167	110.350	42120.0	25.406	-70.047
180948.734	1262.0	499°C	540 ° -	111.175	42120.5	25.404	- 70.040
180951.109	1248.3	544 ° 4	.68]	113.169	42134.0	25.400	-70.050
1 R0053.484	1239.7	570.6	.186	114.371	42153.5	25.397	-70.052
189958.359	1248.0	507.5	686	115.607	42120.0	25.390	- 70.056
189960.734	1245.3	627.£	-1.321	116.967	42065.0	25.387	-70.058
189963.109	1239.9	669.7	463	118.920	42015.5	25.383	-70.060
189967.850	1251.8	700.6	-1.100	120.314	41922.2	25.375	-70.054
189970.359	1246.2	728.7	-1.950	121.598	41832.7	25.370	-70.067
189972.734	1236.7	761.1	-1.010	123.182	41752.0	25.366	-70.069
189975.109	1241.7	7.5.7	-1.423	123-825	416R5.0	25.342	-70.071
180077°484	1246.0	798.1	-1.489	124.816	41595.0	25.357	-70.074
199079.859	1245.3	926.3	-2.558	126.193	41475.7	25.352	-70.077
180084.734	1257.5	£72.3	-2.01R	128.149	41223.0	25.342	-70.042
189989 484	1265.4	923.1	-2.921	130.410	40954.7	25.332	-70.088
199991.459	1268.6	05] ° I	8c4"E-	131.648	40783.0	25.326	-70.091



3150-6024-R8-000 Page A-59

	6FM	INI-7 REENT	RY SEGMENT 4				
TIME FROM LIFTOFF (Seconds)	INERTIAL VEL. Magnitude (ft/Sec)	RELATIVE VEL. Magnithde (ft/sec)	INERTIAL FLT. Path angle (degrees)	INERTIAL Heading angle (dfgrefs)	ALTITUDE (FEFT)	GFODETIC LAT. (degrees)	GENDETIC LONG. (DEGREES)
1 80004 . 734	1275.0	970.2	-2,321	132,528	40624.0	24.321	-70.044
1 20004 7 74	1279-6	000	-2.949	133.616	40473.5	25.315	- 70.098
100000 100	1285.0	1079.8	-3.641	135,111	40292.7	25.309	-70.101
100001 484	1203.2	10551	-3.90R	136.155	40043.2	25.202	-70.105
190003.859	1329.2	1092. F	-4.306	137.318	39851.7	25.297	- 70.109

Table A-2c. Reconstructed Reentry Trajectory and Associated Parameters (IGS) -- Continued





Phase
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PCM
A-3.
Table

GFMINI FOLT PROGRAM

TIME IN SECONNS ERAN LIFTNEE

CEMPUTED POSITION VELOCITY AND ACCELERATION IN GUIDANCE THRUST COURDINATES

		CMPUTED PUST	TINN VELLE	LIT ANU ALLE					
TIME	×	*	~	XCOT	700V	7007	XODOT	V DOUT	ZDOOT
(SECS)	(FT)	(FT)	(FT)	(FT/SEC)	(FT/SEC)	(FT/SFC)	[FT/SFC#2]	(FT/SEC+2)	(FT/SFC#2)
1,368	•	105-	ı	15	-169.22	- 0 6	F. I	-40° 83	15
2 705	7	- AC A	-	56	-264.51	- • 54	17	-41.17	20
6 0 0 V	- r I	-1628	ï	4 4 •	-361.09	-1.12	17	-41.54	25
975.8	י ע ו ו	- 75.95	ي. ا	-1.48	-45 R.77	-1.70	16	-42.04	2A
10.716	с 1	-3773	11-	-1.60	-557.44	-2.38	13	-42.53	31
13.051	- 1 -	-5191	-17	-2.00	-657.41	-3.15	o() • -	-43.00	33
15.826	6 1	-7183	-77	-2.12	17.277-	-4-72	-•05	-43.60	30
18.163	- 7 4	6116-	8 F -	-2.33	-879.76	-4.RO	.07	-44.14	24
20.508	- 29	-11304	150	-1.87	-984.10	-5.29	•26	-44.73	16
22.989	1	-13884	5.3-	-1.30	- 1095.92	- 5 - 5 B	. 71	-45.37	•0 • -
25.435		-16701		19	-1207.73	-5.47	1.66	-45.9R	01
205.70	16-	92001-	- 88	4.18	-1293.73	-5.77	2.67	-46.43	. 02
20.745		LEECC-	-101	12.59	-1409.22	-5.38	4.29	-47.00	•0•
32.192	- 4 - 6	-25924	-115	25.13	-1523.81	-5.48	5.97	-47.55	• 05
34.536	115	00166-	-128	42.04	-1640.69	-5.39	7.64	-48.06	•02
37.083	243	-33950	- 14]	62.43	-1758.96	-5.21	9.34	-48.62	0.
39.526	425	-38303	-154	16.79	-1878.32	-5.12	11.03	-49.14	- 01
41.971	673	-42132	-167	116.67	-1990.36	-5.23	12.71	-49.67	· - 1 ·
44.414	999	-48165	-191	149.73	-2121.11	- 5.72	14.31	-50.17	14
46.859	1408	-53503	-197	1R6.57	-2244.54	-6.63	15.86	-50.68	- U
105.04	1915	-59150	-213	227.37	-2369.07	-6.36	17.55	-51.18	05
51.776	0530	-65156	-228	272.23	-2496.38	-6.38	19.48	-51.55	14
54 222	3256	-71415	-244	522°23	-2622.99	-6.99	21.64	-51.81	28
56.091	3997	-76408	-258	344.48	17.9175-	-7.70	23.26	-51.92	38
52.536	4861	- 43214	-27 <u>8</u>	474.44	-2847.01	-8.70	25.27	-52.10	E E • -
60°984	5977	07206-	-301	489.26	-2974.71	-10.00	27.17	-52.13	18
63-447	7264	-97876	-375	557.31	-3103.90	-9.45	29.23	-52.02	• 12
45.977	9737	-105681	-349	632.15	- 32 37.09	-9.4B	31.43	-51.81	• 72
595 84	10201	-113805	125-	713.00	-3359.58	-7.47	33.68	-51.61	1.40
70.484	17771	-122327	F 8 F -	799.35	-3487.76	÷0°c-	35.99	-51.51	1.94
77.374	14841	-1311 A3	Ûa£́-	A91.70	-3616.14	4°54	38.52	-51.2A	1.72
75.275	14147	-138151	8 Y F -	964.55	-3713.75	7.18	40.63	-51.12	1.37
77.744	1 RF 4.0	-147475	- 349	1070.41	- 3830°24	A.70	43 . 18	-51.00	4

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Phase
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GEMINI FULT PROGRAM

TIME IN SECONDS FROM LIFTOFF

	×	>		Y DOTY	VOAT	1001	10000		
(SECS)	(FT)	(FT)	(FT)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(FT/SEC+2)	(FT/SEC+2)	(FT/SEC+2)
P0.241	62215	-157219	1325	1102.69	-3965.82	60.0	45.21	-51.43	- 41
£2.604	24512	-167102	下 () だ -	1295.93	-4792.00	7.14	47.03	-52.11	8 Y -
P5.140	27821	-177267	-202	1411.40	-4221.96	9.09	49.00	-52.67	- 75
87.615	23415	199701-	Ēu2-	1535.39	-4353.11	3.72	51.35	-53.08	56
90°070	35395	-198727	- 775	1665.25	-4482.57	2.39	52.02	-53.35	26
92.51A	79634	-2Cc657	ċ12-	1790,80	-4613.91	5.5	55.49	-53 . 64	
94.999	44257	-221427	022-	1042.35	-4747.54	1.49	15.02	-53.78	:
56.R94	48965	-230565	-246	2057.43	-4849.80	2.23	61.66	-53.71	
99 . 353	53314	-242653	-240	2212.94	-4981.63	2.55	64.79	-53.47	02.
101.453	50052	-255274	-254	237A.RO	-5115-15	2.78	64.00	-53.25	. 22
104.349	46234	-268207	-746	7552.40	-5247.87	3.50	71.25	-52.98	
104.870	71870	-281408	-236	2726.25	-5390.99	4.49	74.43	-52.40	
109.364	78930	-295197	222-	2926.44R	-5512.11	5.17	78.00	-52.42	
111.858	86476	E0 [50E-	-205	3125.42	-5642.42	7.75	A].48	-52.06	
113.765	97593	-319954	-1 R Q	3283,06	-5741.78	8.96	R4.37	-51.56	52.
116.262	101047	257762-	-144	3497.86	-5870.10	11.22	R.12	-50.79	.74
118.756	110049	-349250	دزا-	3722.53	-5995.24	13.19	00.10	-50.35	-57
121.257	119652	-364358	0 U T	3957 . Rl	-6119.17	14.27	95.52	-50.57	46.
123.726	179717	79459	-63	4197.86	-6244.59	14.48	98.90	-51.37	11.
124.185	140342	-395172	-27	4444.86	-6372.90	14.77	102.41	-52.46	- 06
128.090	148999	-407409	-	4642.35	-6473.33	15.09	105.26	-53.24	- 00
130.549	160735	-423489	0 ť	4905° AG	-6605.50	14.79	109.71	-54.11	25
122.998	13061	023667-	22	5177.47	-6739.17	13.12	113.43	-54.94	32
135.445	196055	-456488	104	5460.46	-6874.51	12.71	117.98	-55.71	06
137.895	828661	1071/7-	135	5754.76	-7011.95	12.20	127.91	-56.50	23
140.342	214294	r24064-	1 F 4	6061.35	-7151.06	11.59	128.16	-57.36	- 25
142.758	239562	-508560	101	63R2.45	-7292.96	10.87	133.87	-58.26	21
145.245	245588	-526594	217	6716.80	-7436.74	10.34	139.99	-59.24	- 13
147.720	262643	-545169	242	7070.59	-7584.39	10.20	146.69	-60.31	-02
150.167	290392	-563911	268	7437.34	-7733.22	10.34	153.79	-61.45	- 20
152.649	299336	-583209	294	7828.OA	-7987.22	11.06	161.01	-62.62	9.6
155.669	323225	-606918	026	8317.32	-8074.59	12.51	169.61	-64.00	- 60
157,024	335081	-618427	347	P347.13	-9084.7 E	11.47	41.32	-14.22	97



3150-6024-R8-000 Page A-62

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Table A-3. PCM Edit Listing for Ascent Flight Phase - Continued

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GEMINI FOIT PROGRAM

TIME IN SECONDS FROM LIFTOFF

(SECS) 150.486 161.942	×	>	2	XOUT	TUCY	7007	XUDUX	VDDDT	
150.486 161.942	(FT)	(FT)	(FT)	(FT/SEC)	(FT/SFC)	(FT/SEC)	(FT/SFC+2)	(FT/SEC+2)	(FT/SFC+2)
161.942	355671	-638293	372	8446.60	-8118.66	9.13	41.6R	-14-01	-1.00
	374541	-658275	195	R 4 8 . 8 .	-R152.43	5.60	42.04	-13.81	-1-04
164.391	3975CR	-678275	404	8653.28	-9146.21	9.98	42.80	-13.91	-1-04
166.706	417750	-697267	410	R753.34	-9218.48	1.44	43.75	-13.90	-1-05
164.905	4 36226	-714554	117	8845.05	-8248.25	- 50	44.61	-13.46	-1-02
171.229	457781	-734571	407	RC54.90	-8291.32	- 3, 23	45.49	-12.70	-1-00
173.648	479595	-754653	304	9066.95	-R30R.43	-5.47	46.67	-10.90	96
176.072	501710	-774820	3.RO	9141.41	-4332.05	-7.70	47.61	- 9. 66	87
178.493	524078	-795019	350	9297.90	-9354.97	-9.94	48.4]	-9-37	
180.920	546784	-815322	333	9416.13	-8377.50	-11.59	49.16	-9.07	- 75
143.341	569725	-R35630	302	9536.10	-8100.23	-13.53	00 07	-8-75	- 66
165.763	592967	-855957	26R	9657 . Al	-94]9.76	-14.99	50.67	-8-44	60
1 P.R. 1 P.3	516487	-876396	230	57A1.34	-9439.79	-16.25	51.43	-R.15	
190.602	540299	-896835	189	9006.75	-8459.33	-17.51	52.21	-7.87	46
193.022	664425	02E216-	145	10033.88	-9478.07	-18.67	52.95	-7.57	- 40
195.441	588863	-927867	00	10163.13	-8495 . 91	-19.34	53.71	-7.22	1.35
107.963	713635	-958464	15	10293.84	-4513.06	-20.21	54.50	-6-87	- 31
200.283	738706	-070085	-	10426.75	-9520.21	-20.98	55.30	-6.54	- 29
202.710	764173	204666-	-50	10562.01	-9544.56	-21.66	56.15	-6.23	26
204.130	789897	-1020497	-103	10698.81	- 4559.32	-22.14	57.00	-5.89	23
207.549	915944	-1041219	-159	10837.64	-9573.38	-22 . 81	57.84	-5.57	21
200.969	842341	-1061981	-213	10978.A9	-9596.14	-23.20	54.72	-5.17	- 20
195.515	60103	-1082701	-270	11121.87	- 4598.50	-23.68	59.60	-4.7R	- 19
714.917	601905	-1103612	1 2 A	11267.27	-9609.39	-24.16	60.51	-4.39	19
217.230	973625	-1124450	195-	11414.71	-8619.55	-24.64	61.46	-3.97	19
219.649	951429	-1145220	-447	11564.65	-8628.73	-25.02	62.41	-3.61	- 17
222.076	979678	-1166770	-508	11717.12	-8636.91	-25.50	63.40	-3.21	17
224.496	1004220	-11871PO	-570	11871.80	-8644.40	-25.79	64.41	-2.83	- 14
226.916	1037139	-1208106	-633	12028.91	-8650.59	-26.27	65.47	-2.47	21
220.336	1066440	-1229047	-698	12188.53	-9656.19	-26.85	66.53	-2.10	25
271.759	1096167	-1250076	-764	12351.05	-9640.9R	-27.53	67.47	-1.73	27
234.184	1126315	-1271021	169-	12516.47	-9664.58	-29.21	48.79	-1.33	- 30
236.609	1156969	-1292045	006-	12684.79	-9567 . 38	-28.89	69.81	06 -	31

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3150-6024-R8-000 Page A-63

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GEMINI EDIT PROGRAM

TIME IN SECONDS FROM LIFTOFF

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		CCMPUTED POSI	TTON VELOC	ITY AND ACCE	LERATION IN	I GUIDANCE T	HRUST COORDIN	ATFS	
141	×	>	7	XDOT	TUUT	ZOUT	X D D T	YDDOT	20001
(SECS)	(FT)	(FT)	(FT)	(FT/SEC)	(FT/SEC)	(FT/SEC)	(FT/SEC+2)	(FT/SEC+2)	{FT/SEC+2}
		7706161	-071	1 2955.53	- 9669-09	-29.76	71.02	51	0€*-
200.95%			-101-	12074.35	-8669.86	-30.25	72.12	- 10	32
150°042	100000000		-1006	13152.44	-8669.18	-30.83	73.41	4 4 8	33
0 1 1 1 1 1 0		5100761-	-1173	54-55551	-8667.50	00.16-	74.62	1.06	15
			-1252	13517.61	-9464.33	-32.68	75.96	1.68	31
200.004		- 11751-	6651-	13704 P	- 9659.37	-33.16	75.77	2. rz	29
000 Cac		1122241-	-1415	13896.12	-9652.71	-34.04	78. R5	00°£	30
		-145461	-1499	14090.74	-9544.76	-34.82	A0.36	3.65	30
		-1475013	-1585	14289.33	- 9634.92	-35.50	60°18	4.33	28
17041070	1677916	-1494937	-1672	14491.50	-9673.58	-36.09	83.57	5.02	28
	1512665	-1518067	-1762	14698.79	-8610.35	-36.87	95°2A	11.5	29
0-1-202	1540040	-1530133	-1853	14909.55	- 9595.53	-37.55	R7.0R	6.42	28
247 434	1594654	-1560174	-1946	15124.89	- 8579.02	-38.33	8 9.01	7.15	28
	CCDEC71	-1581139	-2040	1 = 344.74	-8560.61	-38.82	90 . RO	7.94	28
270 610	1661733	-1602056	-2136	5569.15	-8540.31	-39.61	92 . 84	8° 70	92
110 110	1100114	-1677979	-2234	5758.49	-8517.72	-40.29	94.72	9.57	30
		-1662753	4660-	FT. 503	-9493.03	-41.08	97 . 02	10.49	
	0204721	-1457945	- 2403	16107.13	-8474.99	-41.57	9A.R3	11.36	н 1 1
		-1678775	-2506	16442.03	-9445.72	-47.55	101.29	12.60	- 35
200 000	1100-1	-1400364	- 7611	16692-07	-8413.97	-43.23	103.44	13.65	35
	100044	-1710070	- 7718	16548.77	-4378.73	-44.22	106.02	14.85	46
			-2825	17206-44	-9341.70	-45.00	104.07	16.11	45.1
	1040050	-1750707	-2031	17461.22	75.5058-	-45.79	111.80	17.18	
206.205	2022758	-1784501	-3072	17806.49	-9248.94	-46.77	115.03	1 G	25
204 603	2064334	-1803567	-3141	1 4 C 7 7 . 0 3	-4205.03	-47.56	119.13	14.01	16
	2106566	-1822528	-3292	[R355.0]	-8158.63	-48.16	121.73	20.84	2
	2140520	FF4141-	- 3405	1P641.79	-8]08.95	-48.95	125.20	22,34	4
101 • 104 202 • 205	2515015	-1860187	-3519	18936.11	- 9055.28	-49.74	128.83	24.05	E.E
	295755C	-1878796	-3636	19238.94	- 7007 -	- 50.73	17.2.1	25.88	31
	220226	-1897266	-3754	19550.87	-7015.39	-51.13	136.84	27.70	H Z
	200000000	-1915572	-792-	19472.65	-7868.97	-51.83	141.79	24.04	78
317.764	2374617	-1033705	4006-	20206.04	-7798.37	-52.43	146.57	31.56	62.4
315.814	2436931	-1957429	-4156	20661.07	-7698.53	-53.53	152.19	34+22	17•-



Table A-3. PCM Edit Listing for Ascent Flight Phase - Continued

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GEMINI FOIT PROGRAM

TIME IN SECONDS FROM LIFTOFF

COMPUTED POSITION VELOCITY AND ACCELERATION IN GUIDANCE THRUST COURDINATES

			TIMA ACCOC		I NETITATI	GUIDANCE I		ALES	
TIME	×	*	•	XOUT	YDOT	1001	XOOOT	YDDDT	70007
(SECS)	(FT)	(FT)	(FT)	(FT/SFC)	(FT/SEC)	(FT/SEC)	(FT/SEC+2)	(FT/SEC+2)	(FT/SFC#2)
318.133	7495745	-1975390	-4283	21020.57	-7616.18	-53.93	157.31	36.30	26
194.055	2534429	-1992746	-4406	21393.61	-7528.25	-54.54	164.16	96°30	- 23
322.778	2594664	-2010157	-4534	21782.50	-7473.95	-55.15	170.67	41.86	- 23
325.100	2435692	-20272cm	-4662	22185.71	22.5257-	-55.55	177.72	75.44	23
327.419	2697632	-2044]85	-4792	22605.94	-727.62	-54.07	185.45	46. 83	25
320°736	2740523	-2060804	-4922	23044.15	-7116.58	-56.69	1 93.92	49.46	02
322.067	2794535	-207721ª	-5055	23504.61	-6999.17	-57.50	203.07	52.49	
734.380	2949692	2025002-	-5190	23995.95	-6873.9R	-58.32	212.19	55.51	75
336.079	2912754	-2110472	-5342	24550.71	-6725.31	-59.33	222.40	58.89	41
320.T92	2992013	-2120826	-5507	24625.33	-6701.92	-59.69	1.66	- 48	• 05
341.A14	3021202	-7143373	-5626	24630.88	-6700.49	-58.54	1.59	- 16	50
342.948	3962905	-2157677	1-5751	24675.27	-5699.87	-58.38	1.52	.18	02
345.064	3136522	-2171855	-5974	24637.92	-6699.55	-58.32	. 72	• 20	.02
340.169	3212989	-2192647	- 4055	24639.48	-5699.41	-58.24	. 40	.12	.03
351.206	3265420	-2204902	-6179	24640.20	-6699.19	-58.28	. 29	•0•	.01
353.427	7317925	-2221177	-6303	24640.63	-6699.06	-58.02	•0•	- 00	-01
354°584	3395722	-2242377	-6485	24640.83	-5699 . 03	-58.23	.0°	• 0.2	.02
354.490	3442594	-275505P	-6507	24640.78	-5699 . la	-58.18	- 02	.01	01
361.225	3510.771	-2273415	-6756	24641.19	-6698.91	10.72-	.06	00 -	00.
363.293	3561038	-2287271	-6876	24641.23	-6699.18	-59.34	.07	.01	00.
364.024	3624345	-23055649	-7035	2464].14	-6699.01	-58.17	.26	• 05	02
368.092	2570287	-2319419	-7155	74641.49	-6699.98	-5A.01	8 ë -	.12	.01
370.929	3746743	-2337755	-7315	24444.12	-6699.41	-54,33	• 36	.10	10.
372.859	0777976	-2251616	-7435	24644.16	-6698.0R	-58.08	.12	• 05	.01
375.625	3844934	-2369879	-7593	24644.19	-6698.21	-59.00	00.	00	•0•
377.846	3010661	-2384754	-1722 C277-	24644.22	-6698.29	-58.04	00.	03	•00
270,089	7972487	-2300]12	-7846	24644.76	-6664.37	-57.AR	05	.01	- • 0 2
382.777	4030946	-24]7448	- 8005	24644 .]9	-6658.40	-58.10	- 02	-•00	-•01
384.792	4040447	Ed21292-	- 4125	24644.04	-569R.27	-54.14	.1 ^R	05	- 02
3P7.524	4 54 45	-2449585	-8284	24444.25	-6699.40	-54.06	.11	-•03	- 00
302.272	チンフィディヴ	-2481789	- A56 3	74644.27	-6698.30	-58.13	16	-•00	00 *-
304.405	6322657	-2495676	- 4694	24644.07	-6698.17	-58.17	25.	¥0	• 00
397.146	4395290	-7514031	- 284 -	24644.09	-6698.30	-58.09	03	-•01	-•00



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Table A-

GFWINI EDIT PROGRAM

TIME IN SECONDS FROM LIFTOFF

COMPUTED POSITION VELOCITY AND ACCELERATION IN GUIDANCE THRUST COURDINATES

TIME	X (FT)	Y (FT)	2 (FT)	X00T (FT/SEC)	YDDT (FT/SEC)	2001 (FT/SEC)	XDNGT {FT/SEC+2}	YDD0T (FT/SFC+2)	2000T (FT/SEC+2)
400 DDE	444503	-2527950	- 4963	24643.94	-5698.17	-57.94	.01	Ę0*-	00*-
401-972	4514226	-2546358	-9123	24644.06	-5698.4t	-58.25	.01	10.1	00
404-050	4545439	-2560278	-9244	24644. JO	-6698.47	-58.10	.02	• 00	10.
404.790	4632970	-2578633	F040-	24644.22	-6698.30	-58.02	13	F.O	00*+
408.870	4684237	-2592566	-9524	24644.07	-6698.17	-57.87	- • 1 B	06	*0*-
411.619	4751952	-2610974	-9684	24642 .64	-6699.00	-58.38	- 20	40.1	80*-
413.694	4903115	-2624882	-9805	24642.68	-6698.87	-54.42	12	05	80.
416.436	4870666	-2643245	-9966-	24642.60	-6608.50	-58°73	•01	• 0 •	-•02



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APPENDIX B TRW REGRESSION PROGRAM (REMP) MODIFICATIONS

A change has been implemented in the TRW regression program (REMP) that allows the effect of unmodeled error uncertainties to be reflected in the a posteriori statistics of the error coefficients. This means that if a set of known functions are purposely omitted from the solution due to correlation or restrictions on model size, the uncertainties of these omitted errors can be effectively added to the uncertainties in the errors that are solved for. This change is mathematically sound and can be described in the following equations.

The usual expression for C_{K} , the a posteriori covariance matrix of the error coefficients, is

$$C_{K} = \left(B_{\sigma_{m}}^{T-1} B + C_{K_{o}}^{-1} \right)^{-1}$$
 (1)

where

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B ≡ partial derivations of measurements with respect to error coefficients

 $\sigma_m \equiv$ assumed white noise covariance matrix of data

 $C_{K_0} \equiv$ a priori error coefficient uncertainties.

The more valid expression for C_K , in light of functions which truly exist but are not solved for, is

$$C_{K} = (B^{T}\sigma_{m}^{-1}B + C_{K_{o}}^{-1})^{-1} \left[B^{T}\sigma_{m}^{-1}(\sigma_{m} + \beta \Sigma_{o}^{+}\beta^{T})\sigma_{m}^{-1}B + C_{K_{o}}^{-1} \right]$$
(2)
$$(B^{T}\sigma_{m}^{-1}B + C_{K_{o}}^{-1})^{-1}$$

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APPENDIX B TRW REGRESSION PROGRAM (REMP) MODIFICATIONS

A change has been implemented in the TRW regression program (REMP) that allows the effect of unmodeled error uncertainties to be reflected in the a posteriori statistics of the error coefficients. This means that if a set of known functions are purposely omitted from the solution due to correlation or restrictions on model size, the uncertainties of these omitted errors can be effectively added to the uncertainties in the errors that are solved for. This change is mathematically sound and can be described in the following equations.

The usual expression for C_{K} , the a posteriori covariance matrix of the error coefficients, is

$$C_{K} = \left(B_{\sigma_{m}}^{T} B + C_{K_{o}}^{-1} \right)^{-1}$$
 (1)

where

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B ≡ partial derivations of measurements with respect to error coefficients

 $\sigma_m \equiv$ assumed white noise covariance matrix of data

 $C_{K_o} \equiv$ a priori error coefficient uncertainties.

The more valid expression for C_{K} , in light of functions which truly exist but are not solved for, is

$$C_{K} = (B^{T} \sigma_{m}^{-1} B + C_{K_{0}}^{-1})^{-1} \left[B^{T} \sigma_{m}^{-1} (\sigma_{m} + \beta \Sigma_{0}^{+} \beta^{T}) \sigma_{m}^{-1} B + C_{K_{0}}^{-1} \right]_{(2)}$$
$$(B^{T} \sigma_{m}^{-1} B + C_{K_{0}}^{-1})^{-1}$$

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3150-6024-R8-000 Page B-2

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where

- $\beta \equiv$ partial derivatives of measurements with respect to omitted error coefficients
- $\Sigma_{0} \equiv$ a priori statistics of omitted terms

with manipulation, Equation 2 can be written as

$$C_{K} = C_{K}^{*} + C_{K}^{*} B^{T} \sigma_{m}^{-1} \beta \Sigma_{o} \beta^{T} \sigma_{m}^{-1} B C_{K}^{*} = C_{K}^{*} + \Delta C_{K}^{*}$$

where

$$C_{K}^{*} = (B_{\sigma_{m}}^{T-1}B + C_{K_{o}}^{-1})^{-1}$$

The REMP program now computes the ΔC_{K} term and prints out both C_{K} and ΔC_{K} , omitting the old C_{K} * terms. It is obvious that the uncertainties of the solved-for error coefficients will now be larger than before (ΔC_{K} being always positive), sometimes much larger, depending of course on β and Σ_{0} .

Table B-1 lists the unmodeled error sources considered in the Gemini 7 analysis. The associated 1-sigma a priori uncertainties are also listed.

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Symbol	Error Source	l-Sigma Uncertainties
B _X	X accelerometer bias	100 ppm
${}^{\rm B}_{\rm Y}$	Y accelerometer bias	100 ppm
BZ	Z accelerometer bias	100 ppm
YSF	Y accelerometer scale factor	160 ppm
ZSF	Z accelerometer scale factor	160 ppm
PHIX	Platform misalignment about x accel axis	44.8 arc sec
A5(1)	MISTRAM I 10K P Leg refraction	15 n units
A6(1), A7(1), A8(1)	MISTRAM I 10K P Leg Internal X, Y, Z Survey	5 ppm
B6(1), B7(1), B8(1)	MISTRAM I 10K Q Leg Internal X, Y, Z Survey	5 ppm
A5(2)	MISTRAM I 100K P Leg Refraction	15 n units
A6(2), A7(2), A8(2)	MISTRAM I 100K P Leg Internal X, Y, Z Survey	5 ppm
B6(2), B7(2), B8(2)	MISTRAM I 100K Q Leg Internal X, Y, Z Survey	5 ppm
C4(3)	GE/Final Range Refraction	15 n unite

Table B-1. Unmodeled Errors and 1-Sigma Uncertainties

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REFERENCES

- F. B. Lavenhar, "Preliminary Gemini G and C Data Reduction and Analysis Plan," Space Technology Laboratories, 4160-6009-TU000, 30 October 1964.
- "Evaluation Report of Mod IIIA Radio Tracking System and Mod III G Missile Borne Guidance Equipment With Gemini Launch Vehicle 7 (U), "Technical Operating Report GE No. 66A200, 7 January 1966. (C)

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