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OPERATIONAL LM ABORT AND RESCUE PLAN FOR APOLLO 14 (MISSION H-3)

Orbital Mission Analysis Branch

MISSION PLANNING AND ANALYSIS DIVISION

MANNED SPACECRAFT CENTER HOUSTON, TEXAS

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PROJECT APOLLO

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By Allan L. DuPont and James D. Alexander Orbital Mission Analysis Branch

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1.0 SUMMARY

The purpose of this report is to present the changes and additions for the operational lumar module about and rescue plan from Apollo 13 (ref. 1) to Apollo 14. The abort and rescue plan for Apollo 14 is essentially the same as for Apollo 13 except for the procedures associated with the new nominal direct rendezvous. Therefore, detailed explanations and data are presented only for failures that occur during the nominal ascent rendezvous.

As for Apollo 13, the Apollo 14 no-PDI-O abort requires a 1-2/3 revolution rendervous after an initial phasing maneuver. The no-PDI plus 12 minute aborts and early aborts for each PDI region requires a 2-2/3 revolution rendervous involving what is referred to as the HM-CBI/CDH sequence. For aborts after approximately 9 minutes into the backup powered descent opportunity, the normal one-revolution CBI/CDH sequence is applied. The variable targeting regions extend to PDI plus approximately 15 minutes for both landing opportunities. The 72-1 and T2-2 rendervous plans require 2-2/3 and 1-2/3 revolutions, respectively. Also, TPI again is scheduled at 16 minutes before the end of darkness to maintain an adequate dt between CDH and TPI without causing large radial

The major change is the ballout abort or rescue procedure used when systems or execution errors prevents a completion of the nominal direct ascent technique. Either technique requires approximately 1-2/3 revolutions and consists of the following maneuvers: phasing maneuver (ballout maneuver) at insertion plus 5 minutes for the IM or at insertion plus 12 minutes for the CSM, CSI maneuver at insertion plus 55 minutes for either vehicle; CDH maneuver one-half period after CSI; TPI approximately ¹/₂ minutes after CDF at approximately 16 minutes before daylicht; and TFF approximately 130° of target travel after TFI.

2.0 INTRODUCTION

The changes to the LM abort and rescue plan from Apollo 13 to Apollo 14 result primarily from the enage to the nominal rendezvous profile. That is, the 1-2/3 revolution coelliptic rendezvous used for Apollo 13 is not the nominal profile for Apollo 14. A direct rendezvous is now used, with lift-off approximately 2.5 minutes earlier than for the coelliptic rendezvous, TPI 38 minutes after insertion, and TFF approximately 100° of target travel later.

The abort and rescue techniques for the descent phase of Apollo 1h are unchanged frem Apollo 13. However, a new technique called the bailout rendervous technique is now used for aborts and rescues for which the 1M has lifted off the lunar surface at approximately the nominal time but is unable to continue the direct rendervous because of contingency in the systems and/or the trajectory. The bailout rendervous is a 1-2/3 revolution rendezvous beginning with a phasing maneuver near insertion followed by a standard coelliptic sequence.

One such condition for using the bailout technique is an uncorrectable overspeed or underspeed at insertion. For this situation, the IM is able to use the ballout technique for the region from approximately 50-fps underspeed to approximately 135-fps overspeed. However, the CSM can use only the ballout technique for rescues from approximately 18-fps underspeed to approximately 175-fps overspeed. For the region from 50- to 18-fps underspeed, the CSM usut use the CSI-dwell sequence initiated at insertion plus 20 minutes. This high-dwell sequence is also used for anytime lift-off cases. For overspeeds greater than 170 fps, the CSM must use the manual-insertion type DKI in order to perform a

Data have been presented for the LM- and CGM-active bailouts and related techniques that are associated with the overspeed/underspeed conditions. Detailed data, such as state vectors, similar answer tables, and MSTM coverage, are not included. For a number answer such detailed data are available upon request. In this report, the sibuteen events, rather than the ground elapsed time, is emphasized because these techniques and sequences are applicable for all acceptable launch dates and launcing sites.

3.0 SYMBOLS AND DEFINITIONS

3.1 Symbols and Abbreviations

•

CDH	constant differential height (coelliptic) maneuver
CSI	coelliptic sequence initiation
CSM	command and service modules
DI	dwell initiation
DKI	docking initiation processor (in RTCC)
DT	dwell termination
НАМ	height adjustment maneuver of HAM-CSI/CDH sequence (ref. 1)
LM	lunar module
MSFN	Manned Space Flight Network
NCL	DKI phase adjustment maneuver
NH	DKI height adjustment maneuver
NSR	DKI coelliptic maneuver
no-PDI	powered descent is not initiated
no-PDI-0	abort point one-half revolution after CSM circularization and one revolution prior to the nominal PDI
PDI	powered descent initiation
TPI	terminal phase initiation
TPF	terminal phase finalization
T2	single-point preferred lift-off after landing
Δh	differential altitude
Δt	elapsed time
٨V	velocity increment



3.2 Definitions

active vehicle

section 4.3

bailout

coelliptic Ah

Ah during the coelliptic phase for which the differential altitude remains nearly constant

height adjustment maneuver of DKI

external maneuver which sets up the establishment of the desired coelliptic Ah 180° later

rendezvous for which the LM is the totally

high-dwell sequence section 4.2

LM-active rendezvous

manual insertion

phase adjustment maneuver of DKI

rescue

theoretical AV

external maneuver which establishes the desired phase (central) angle at the subsequent maneuver

nonnominal rendezvous sequence for which the CSM performs one or more of the rendezvous maneuvers; for this report, it is assumed that the CSM is totally active during a rescue

Keplerian impulsive AV; for example, the TPF AV for the impulsive intercept velocity match

4.0 RENDEZVOUS TECHNIQUES

The abort and reacus rendezvous techniques involved in the operational plan are described in this section. There is basically one new LM-active maneurer sequence, and it is used when the LM is unable to continue the direct rendezvous because of a contingency situation. This sequence, referred to as the basicut sequence, requires approximately 1-2/3 revolutions to rendezvous and uses the basic CSI-CDH coelliptic sequence. Three rescue techniques are involved. If the LM is in a situation that requires a rescue, the CSM will utilize one of the following maneuver sequences: a CSM bailout sequence, a CSM high-dvell sequence, or a CSM DKI sequence esimilar to the manual-insertion DKI sequence.

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4.1 Bailout Sequence

This five-impulse sequence is initiated by a phasing maneuver referred to as the bailout maneuver; it is directed along the local horizontal and is performed either at insertion plus 5 minutes for the LMactive sequence or at insertion plus 12 minutes for the CSM-active sequence.

The initial maneuver is followed by the CSI-CDH coelliptic sequence, with CSI at insertion plus 55 minutes for either vehicle. CDH is scheduled one-half period after CSI, with a separate plane change maneuver scheduled between CSI and CDB. The technique is targeted to obtain a dh of approximately 15 n. mi. TFI occurs approximately 16 minutes before daylight. TFP is 130° of target travel after TFI. Figures 1 and 2 illustrate the bailout sequence.

4.2 High-Dwell Rescue Sequence

The high-dwell rescue sequence is essentially a six-maneuver CSMactive sequence initiated by a local horizontal phasing maneuver called dwell initiation (DI) at insertion plus 20 minutes. Dwell termination (DT) occurs at approximately the same longitude as the DI maneuver with approximately three revolutions between DI and DT. The dwell phase is followed by the CSI-CDB coelliptic sequence, with CSI 30 minutes after DT and CDB come-haif period after CSI. The An is targeted for approximately 15 n. mi., with TFI lighting conditions the same as for the bailout technique. Figure 3 illustrates this rescue sequence.

4.3 Manual-Insertion-Type Rescue Sequence

This rescue technique is infinited by a ground-computed DKI plan at approximately insertion plus 110 minutes. The LN, if able, performs a 10-fbs horizontal posigrade boost maneuver at approximately the first DK line-of-apsides after insertion. The initial rescue maneuver, a phase adjust maneuver (NCI), is performed approximately 110 minutes after insertion, approximately over the landing site. In real time, an attempt will be made to place this maneuver on the LM line-of-agsides to minimize the radial velocity component of the CDM maneuver. The second maneuver (NH), which is a height adjustment maneuver, is performed 1/2, 1-1/2, or 2-1/2 revolutions after NCl depending on the LM apolume altitude. The onboard GSI logic would be used to compute the NH maneuver if pre-CSI tracking were obtainable. See figure 1(g) in reference 1 for an illustration of this rescue technique.

5.0 DISCUSSION

The LM-martive and CSM active maneuver sequences that apply to the various LM failure situations are presented in this section. The discussion is divided into the different phases, and the failure situations are discussed only to the extent that they determine the procedures. A summary of the plan is presented in figure 4. Relative motion plots are presented for specific cases in each phase. Relative range time historics are also included for these cases. It is emphasized that the LM is always below during the coelliptic and terminal phases regardless of which vehicle is active. A coelliptic ah of 15 n. mi. and TFI lighting of b minutes prior to daylight are the standard targeted values.

5.1 Discussion of the Bailout Sequence

5.1.1 <u>IM-active rendezvous</u>. The ballout sequence is applicable when the decision to above the direct rendezvous sequence is made after lift-off. Three possible reasons for an abort decision leading to the ballout technique are a velocity error at insertion that is not corrected by either a trim or a tweak maneuver, a tweak maneuver greater than 60-fps total AV or a post-tweak perilume altitude less than 5 n. mi.

The abort technique is the CSI/CDH sequence preceded by a phasing maneuver called the bdilout maneuver. This phasing maneuver is ground-computed and is performed at insertion plus 5 minutes. CSI is performed is targeted for a coelliptic ah of 15 n.ml., with TDI 16 minutes prior to daylight and 130° of target target later.

Figure 5 presents range and relative motion data for the bailout technique after nominal lift-off and insertion. Figure 6 provides similar information for an uncorrected insertion underspeed acceptable at insertion because the LW would be on an impact trajectory with a larger underspeed. Figure 7 provides the same information for a LM uncorrected overspeed of 135 fps. At this point, the resulting ballout anneyure results in a perilume below the minimum allowable of 5 n. mi. Therefore, this is the maximum uncorrected overspeed allowed for which the LM bailout is applicable.

5.1.2 Regrue. The rescue ballout technique is similar to the abort technique and is used whenever the UM is unable to perform the ballout maneuver. Again, the sequence is the CSI/CDH technique preceded by a ground-computed phasing maneuver. However, the CSM ballout maneuver is performed at insertion puble 12 minutes for the rescue case, with CSI M3 minutes after the ballout maneuver. CDH is one-half period after CSI and is targeted for a dh of 15 n. mi above the IM orbit. TFI is at the same g.e.t. as for the IM-active case, with TFP 130° of target travel later.

Figure 8 illustrates relative range and relative motion data for a GM-active rendezvous after an on-time LM litt-off and an accurate LM insertion. Figure 9 contains the same information for a GSM bailout after a LM uncorrected insertion underspeed of 18 fps. After the CSI maneuver, this rendezvous reaches the low perlume limit of 5 n. ml. The CSM must pass through perlume to reach CDM in this underspeed area. Therefore, a LM insertion underspeed of 18 fps is the underspeed limit to the applicability of the CSM bailout technique. Figure 10 presents relative range and relative motion data for a LM uncorrected overspeed of 175 fps. This represents the LM insertion overspeed limit for use of the CSM bailout technique for the same reasons described previously. It should be noted that the CSM is able to take over the rescue during any of the rendezvous maneuvers.

5.2 Discussion of the High-Dwell Rescue Sequence

A IM insertion underspeed less than 18 fps allows the use of the GSM bailout technique. Also, if the IM is able to perform the ballout maneuver after any overspeed or underspeed, the CSM can perform essentially a "mirror image" GSI/OH sequence.

However, if the LM is unable to maneuver after inserting with an underspeed greater than 16 fps, the CSM must use the high-devil rendervous sequence. This technique has been revised from that presented in reference 1 and now consists of ground-computed phasing maneuvers followed by the CSI(DDH sequence. The initial maneuver, duell initiation, is performed 20 minutes after insertion, placing the CSM in an orbit with an apolume above 300 n. mi. Another phasing maneuver, dwell termination, is performed at approximately the same longitude as the DI maneuver, with at least three CSM revolutions between DI and DT. If required, an additional tweak phasing maneuver can be performed between DI and DT at each CSM crossing of the DI longitude.

The CSI/CDH sequence described previously completes the rendezvous, with CSI performed 30 minutes after the DT maneuver. The revised highdwell sequence is being used because the range prior to CSI allows onboard tracking by either vehicle.

Figure 11 provides relative range a relative motion data for a 50-fps LM uncorrected underspeed at insertion.

5.3 Discussion of the Manual-Insertion-Type Rescue Sequence

The manual-insertion sequence (ref. 1) is used for situations in which a LM uncorrected overspeed at insertion is greater than suproximately 175 fps. The maneuvers are ground-computed from the HCOC program and begin with a phasing maneuver (BCI) performed approximately 110 minutes after insertion. The second maneuver is a height maneuver (BH) that is performed an odd number of half revolutions after MCI (i.e., one-half revolution later, 1-1/2 revolutions after MCI (i.e., one-half revolution later, 1-1/2 revolutions after MCI (i.e., one-half determine the necessary number of phasing revolutions are the total AV expended for the sequence and the total time necessary to rendervous. The third maneuver, performed one-half revolution after NH, is the coelliptic maneuver (INSR) and is targeted for a dh of 15 n. mi. CSM TFI is 16 minutes prior to deylight, with TFF approximately 130° of target travel hater.

Figure 12 illustrates relative range and relative motion data for a CSM rescue after a LM uncorrected overspeed of 180 fps.

5.4 Specific Cases Available Upon Request

The following specific cases have been generated and placed on tape and can be made available upon request to the authors. The detailed data for these cases include state vectors before and after each maneuver, detailed maneuver tables, exact lighting, and MSNR coverage.

- a. LM-active no-PDI-0 abort
- b. Rescue after accurate no-PDI-O abort maneuver
- c. Rescue after partial no-PDI-O abort maneuver

1. Partial AV = 0 fps, phasing orbits = 2 (n=4)

2. Partial AV = 20 fps, phasing orbits = 2 (n=4)

3. Partial AV = 20 fps, phasing orbits = 1 (n=2)

d.	LM-active no-PDI-1 plus 12 minute abort	
e.	Rescue after accurate no-PDI-1 plus 12 minute abort	
f.	Rescue after partial no-PDI-1 plus 12 minute abort	
	1. Partial $\Delta V = 0$ fps, phasing orbits = 3 (n=6)	
	2. Partial $\Delta V = 20$ fps, phasing orbits = 3 (n=6)	
	3. Partial $\Delta V = 20$ fps, phasing orbits = 2 (n=4)	
	4. Partial $\Delta V = 60$ fps, phasing orbits = 2 (n=4)	
	5. Partial $\Delta V = 60$ fps, phasing orbits = 1 (n-2)	
g.	LM-active no-PDI-2 plus 12 minute abort	
h.	Rescue after accurate no-PDI-2 plus 12 minute abort	
i.	Rescue after partial no-PDI-2 plus 12 minute abort	
	 Partial AV = 0 fps, phasing orbits = 5 (n=10) 	
	 Partial AV = 5 fps, phasing orbits = 5 (n=10) 	
	 Partial ΔV = 5 fps, phasing orbits = 4 (n=8) 	
	4. Partial $\Delta V = 20$ fps. phasing orbits = 4 (n=8)	
	5. Partial $\Delta V = 20$ fps, phasing orbits = 3 (n=6)	
	6. Partial AV = 50 fps, phasing orbits = 3 ($n=6$)	
	7. Partial AV = 50 fps physing orbits = 2 ($n-k$)	
	8. Partial AV = 95 fps phosing orbits = 2 ($n=4$)	
	9. Partial AV = 95 fps phasing orbits = 2 (n=4)	
1.	IM-active rendervous following on about such similar but a	
k l	IN active rendervous for owing an abort each minute during PDI-]	
1.	IM active rendervous following abort at 12-1	
1.	an accure rendervous for owing abort each minute during PDI-2	

m. LM-active rendezvous following abort at T2-2

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- n. IM-active direct rendezvous with IM bailout
- o. LM-active direct rendezvous with CSM bailout
- p. CSM rescue following manual LM insertion
 - 1. Low orbit
 - 2. Medium orbit
 - 3. High orbit
- CSM rescue after LM contingency insertion into a 10- by 10-n. mi. orbit

6.0 CONCLUSIONS

The information and data discussed in this report present the operational abort and rescue plan for cases resulting from an attempt to execute the nominal direct ascent rendezvous profile. The supplementary specific data, which are available upon request, can provide a basis for the various consumbles, time line, software, and propulsion analyses.

With two exceptions, reference 1 should provide accurate information for abort and rescue techniques for the remaining situations, including pre-FDI aborts, powered descent aborts, and aborts from the lumar surface. The exceptions are (1) the high-dwell sequence described in reference 1, which has been revised to the sequence described in the report, and (2) lift-off from the lumar surface for the manual insertion technique, which should be at 11.5 minutes instead of 9 minutes after the nominal time.







Figure 2.- CSM-active rendezvous following a CSM bailout maneuver.



Event

- 1 Insertion
- 2 Dwell initiation (DI)
- 3 Dwell termination (DT)
- 4 CSI
- 5 CDH
- 6 TPI
- 7 TPF

Figure 3. - CSM-active hi-dwell rescue sequence.



IM overspeed/underspeed at insertion, n.mi.

Figure 4.- Recommended rendezvous techniques for aborts and rescues after an on-time lift-off and a contingency orbit insertion.

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Figure 5. - Range and relative motion (curvilinear, CSM-centered) data for a LM-active rendezvous following a LM ballout maneuver at insertion plus 5 minutes.



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Figure 6.- Range and relative motion (curvilinear, CSM-centered) data for a LM-active rendezvous following a LM bailout maneuver for an insertion underspeed of 50 feet per second.



Figure 7. - Range and relative motion (curvilinear, CSM-centered) data for a LM-active rendezvous following a LM bailout maneuver for an insertion overspeed of 135 feet per second.



Figure 8.- Range and relative motion (curvilinear, LM-centered) data for a CSM-active rendezvous following a CSM bailout maneuver at insertion plus 12 minutes.



Figure 9. - Range and relative motion (curvilinear, LM-centered) data for a CSM-active rendezvous following a CSM bailout maneuver for an insertion underspeed of 18 feet per second.

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Figure 10. - Range and relative motion (curvilinear, LM-centered) data for CSM-active rendezvous following a CSM ballout maneuver for an insertion overspeed of 170 feet per second.



Figure 11. - Range and relative motion (curvilinear, LM-centered) data for a CSM-active rendezvous following a LM in sertion with an underspeed of 50 feet per second.



Figure 12. - Range and relative motion (curvilinear. LM-centered) data for a CSM-active rendezvous following a LM insertion with an overspeed of 180 feet per second.

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