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### ABSTRACT

The System Status Report is distributed monthly on the 15th. This month's revision of E-1142 (Rev. 22) contains, in general, the following information for the Block I and Block II Command Module and LEM equipment configurations: weights, centers of gravity, moments of inertia, power requirements, status of computer programs, and reliability figures.

PAGE\_\_\_\_\_\_\_

### Section 1

### INTRODUCTION

### 1-1 INTRODUCTION

The definition of what constitutes Block I and Block II Command Module and LEM hardware is contained in the Glossary, section 5 of this report.

The following information is included in this month's report:

- Command Module, Block I: weights, centers of gravity, moments of inertia, power requirements, and a brief description of Block I 100-series systems.
- (2) Command Module, Block II: weights, power requirements, status of computer programs, and reliability figures.
- (3) LEM: weights, power requirements, and reliability figures.

### 1-2 ACCURACY

The accuracy of numerical values reported in this revision should not be considered to be within the tolerances implied by the significant figures quoted. The reported values, although based upon the most current information, are subject to normal changes as design and development phases approach completion.

### Section 2

### BLOCK I COMMAND MODULE DATA

### 2-1 WEIGHTS

Table 2-1 presents the weights of all Block I equipment, grouped according to specific location within the Command Module. Weights are reported to the component level and to the nearest tenth of a pound.

Given component weights are identified as estimated, calculated, and measured in the order of increasing accuracy. These terms are defined by North American Aviation as follows.

Estimated weights (E) are based on rough calculations. Calculated weights (C) are based on detailed calculations made from final production drawings that will be used to build flyable equipment. Measured weights (M) are the actual weights of equipment built to the production drawings.

North American Aviation will provide and be responsible for cold plate weights that are not integral with guidance and navigation equipment.

2-1.1 WEIGHTS STATUS REPORTING. Table 2-I also offers a comparison of present component weight values with those listed in System Status Report, E-1142 (Rev. 21, June 15, 1964. All weight changes are explained in paragraph 2-2.

2-1.2 CONTROL WEIGHT. Column (a) in table 2-I contains the February 15, 1964 weight status of Apollo G&N Equipment. Column (a) adds up to approximately the total control weight specified in letter PG-64-113 (March 6, 1964) from Mr. D. Gilbert, ASPO, to Mr. M. Trageser, MIT/IL.

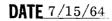
2-1.3 DESIGN LOAD WEIGHT. At NASA Coordination Meeting No. 15A, MIT agreed to assign "not-to-exceed" design load weights for individual Block I G&N subsystems. These weights were assigned by MIT in MIT letter AG 594-64, 18 May 1964, and are shown in column (d) of Table 2-I in this report. The total design load weight represents a secure maximum, since it is unlikely that the largest increases in each subsystem will occur simultaneously. The design loads listed recognize possible individual increases to account for changes accepted by NASA for the Block I flight systems (100-series systems). See paragraph 2-5.

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Table 2-I. Current	Current Weight Status of Block I Command Module (198	is of Block	I Command	Module (lbs	s at 1 g)	
	Status		Status 2 / 2 /			Design Load Wt.** E/64
ltem	2/64 (a)	(b-a)	6/04 (b)	(c-b)	(/ 04 (c)	0/04 (d)
G&N SYSTEMS						<u>.</u>
CDU Assy	14.5 (M)	-0.9	13.6 (M)	0.0	13.6 (M)	18.0
Optical Subsystem						
SXT	14.6 (C)					
SCT	13.8 (C)	<b>≻</b> +1.1	46.2 (M)	0.0	46.2 (M)-	
Optical Base & Gearing	16.7 (E)					
Optical Eyepieces					1	
SXT	1.3(E)	+0.3	1.6 (M)	0.0	1 6 (M)	<b>&gt;</b> 100.0
SCT	2.3 (E)	+0.3	2.6 (M)	0.0	2.6 (M)	
NVB & Resilient Mounts	25.0(E)	0.0	25.0(E)	+0.7	25.7 (M)	
Bellows Assy	13.5 (M)	0.0	13.5 (M)	-0.8	12.7 (M)-	
IMU	60.2 (M)	0.0	60.2 (M)	0.0	60.2 (M)	$\int 65.0$
Coolant Hoses (two)	1.0(E)	-0.3	0.7 (E)	0°0	0.7(E)_	
Power Servo Assy	59.4 (C)	+0.4	59.8 (C)	-0.7	59.1 (C)	75.0
G&N Interconnection Assy	35.2 (E)	-5.2	30.0 (C)	0.0	30.0 (C)	45.0
G&N to S/C Interface Assy	8.0(E)	0.0	8.0(E)	0.0	8°0 (E)	L 100.0
AGC (no spares)	70.0(E)	0.0	70.0(E)	0.0	70°0 (E)	
Optical Shroud	3.5 (M)	-0.4	3.1 (M)	0°0	3, 1 (M)	4.5
LOWER EQUIPMENT BAY						
D&C						
D&C Electronics	2.9 (M)	0.0	2.9 (M)	0.0	2.9 (M)	_
Control Electronics	2.9 (E)	-0.9	2.0 (M)	0.0	2.0 (M)	
G&N Ind Cont Panel	9.5 (M)	+0.4	9.9 (M)	0.0	9.9 (M)	√ 70.0
IMU Control Panel	2.4 (M)	+0,2	2.6 (M)	0.0	2.6 (M)	
MDV (includes 1 film)	7.7 (C)	+1.3	9.0 (M)	0°0	9°0 (M)	
D&C/AGC Signal Conditioner Assy	20.6 (M) 0.0	-0,2 +4,6	20,4 (M) 4,6 (E)	$^{+1.0}_{-0.0}$	$\begin{bmatrix} 21, 4 (C) \\ 4, 6 (E) \end{bmatrix}$	0°°°

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		·····	·		ومحمد والمراجع والمراجع والمراجع المراجع المراجع المراجع المراجع والمراجع والمراجع المراجع المراجع والمراجع وال
~	Design Load Wt.** 5/64 (d)	26.0 3.0 0.0 2.5	520		lbert, ASPO, to See paragraph 2-1.3.
at 1 g) (cont)	Status 7/64 (c)	21.4 (C) 2.5 (E) 2.5 (M) 0.0 1.6 (M)	412.9	25.0(E) 34.6(E) 16.7(E) 2.5(E) 0.3(E)	
Todule (lbs	(c-b)	+1.0 0.0 0.0 0.0	+1.2	0°0 0°0 0°0	m Mr. D. ( y 18, 1964).
Current Weight Status of Block I Command Module (lbs at 1	Status 6/64 (b)	20.4 (M) 1.5 (E) 2.5 (M) 0.0 1.6 (M)	411.7	25.0 (E) 34.6 (E) 16.7 (E) 2.5 (E) 0.3 (E)	6, 1964) fro 594-64 (Ma
s of Block I	(b-a)	-0.1 0.0 +0.1 -3.6	3, 3	0°0 0°0 0°0	113 (March -1.2. F letter AG
eight Status	Status 2/64 (a)	20.5 (M) 20.5 (M) 1.5 (E) 2.4 (E) 3.6 (E) 1.7 (M)	415.0%	25.0(E) 34.6(E) 16.7(E) 2.5(E) 0.3(E)	in letter FG-64-113 See paragraph 2-1.2 e taken from MIT let
Table 2-I. Current W	Item	MAIN PANEL AREAD&C/AGCD&C/AGCLOOSE STORED ITEMSEye Relief EyepiecesFilm Cartridges (4)Horizon PhotometerOptics Cover	TOTAL	List of Possible Spares for Block I AGC Spare Logic Tray AGC Spare Memory Tray AGC Spare (Unique) Modules PSA Spare (Unique) Modules CDU Spare Spare Relay & Diode Module	*Control weight specified in letter FG-64-113 (March 6, 1964) from Mr. D. Gilbert, ASFO, to Mr. Trageser, MIT/IL. See paragraph 2-1.2. **Design Load Weights are taken from MIT letter AG 594-64 (May 18, 1964). See paragraph 2



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BLOCK I COMMAND MODULE COMMAND MODULE

Table 2-II. Block I Command Module Center of Gravity and Moment of Inertia Data	nmand Mc	odule Cent	er of Grav	ity and Mc	ment of In	iertia Data	
	Weight	Cent	Centers of Gravity (inches)	vity	Mon	Moments of Inertia (lb-in <sup>2</sup> )	ertia
шал	(201)	x	Υ	Z	Ixx	Iyy	Izz
LOWER EQUIPMENT BAY							
CDU Assy Optical Subsystem	13.6	63.5	-14,4	35.8	73	144	131
SXT SCT							
Opt. Base & Gearing	- 50.4	69.6	0°5	31, 1	1468	992	1737
SXT							
SCT	60, 2	56.6	0°0	41.7	1186	1450	1438
NVB & Resilient Mounts	25.7*-	► 64. 3	-0.1	41.3	3270	4050	5210
Bellows Assy	12.7*_			0		c T T	
G&N Interconnection Assy		53.1	-1°1		3610	3110	4860
G&N to S/C Interface Assy	8.0	37.8	8° 9	44.8	378	403	32
D&C/NAV Station					, ,		č
IMU Cont Panel	2.6		-15.4	30,9	15	22	24
D&C Electronics	2,9		9.6		20	52	ත (
Control Electronics Assy	2.0	63.1	10,7		6	15	0000
Optical Shroud & Cover	4.7		0.0		387	108	413
G&N Ind. Control Panel	9.9		0,1		455	110	560
D&C/AGC	$21.4^{*}$		14.8	36.3	294	1114	780
MDV (Includes 1 film)	9.0		4,5	31,0	518	92	531
AGC (no spares)	70.0	37.8	1.3	46, 1	4980	3990	1710
PSA	59.1*	45,0	-1.1		3940	1460	2620
Signal Conditioner Assy	4.6	49.8		40, 5	28	29	14
Coolant Hoses	0.7	64.8	6.5	34.9	2	∞	15
					-		
		<b>)</b>	(cont)				

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Table 2-II. Block I Command Module Center of Gravity and Moment of Inertia Data(cont)	nand Modu	le Center	of Gravity	and Mome	ent of Inert	tia Data(cc	int)
Tterres	Weight	Cent	Centers of Gravity (inches)	vity	Mor	Moments of Ir (lb-in <sup>2</sup> )	Inertia
Пеш	(lbs)	X	Y	Z	Ixx	Iyy	Izz
<u>MAIN PANEL AREA</u> D&C/AGC	21.4*	67.8	-12.5	-20.4	283	256	317
Total Moments of Inertia About the Basic X, Y, Z Axes of the Command Module	408.9*	55.1*	- 0. 3*	37.3*	681, 030	1, 939, 0641, 308, 074	1,308,074
LOOSE STORED ITEMS Eye Relief Eyepieces Film Cartridges (4)	1.5 2.5	(SCT, (Each	(SCT, 4-5/8" x 2 1/2" dia. (Each cartridge, 1-1/2 x 3	1/2" dia. 1-1/2 x 3	SXT 3" x 2 x 6 inches)	2-1/4" dia.) \$)	a. )
* These values represent changes since the last report, Rev. 21, dated June 15, 1964.	nges since	e the last 1	report, Re	v. 21, dat	ed June 18	5, 1964.	

# COMMAND MODULE

### 2-2 REPORTED WEIGHT CHANGES

2-2.1 NVB & RESILIENT MOUNTS. The 0.7-pound weight increase is based upon an ACSP "measured weight of parts" last received by MIT/IL on June 17, 1964.

2-2.2 BELLOWS ASSY. The 0.8-pound decrease is also based on the above list (see section 2-2.1).

2-2.3 POWER SERVO ASSY. The 0.7-pound weight decrease results from the elimination of the Backup Mode Electronics.

2-2.4 D&C/AGC (LEB and MP). The addition of 1.0 pound to each of the D&C/AGC's is to account for the weight of the potting compound which was not considered in the original measured weights.

### 2-3 CENTERS OF GRAVITY

Table 2-II presents the centers of gravity of each weight component or packaged assembly, determined with respect to the basic X, Y, Z axes of the Command Module. Center of gravity values are given to the nearest tenth of an inch.

### 2-4 MOMENTS OF INERTIA

Table 2-II also presents the moment of the inertia of each weight component or packaged assembly, determined about each of the component axes which (1) run through the center of gravity of the component and (2) are parallel to the basic X, Y, Z axes of the Command Module. The total center of gravity and moments of inertia of all G&N equipment (excluding loose stored items) have been calculated about the basic X, Y, Z axes also.

#### 2-5 BLOCK I (100-SERIES SYSTEMS)

The Block I weights reported in E-1142 have represented the basic Block I configuration. This configuration was not expected to be used for flight tests. All flight systems were to be Block II which would incorporate all changes necessary for flight. Recent scheduling decisions have made it necessary to use systems earlier than Block II for in-flight tests. Accordingly, a series of modifications to the basic zero-series Block I have been approved by NASA (Ref: MSC TWX No. E G04-17-64-208) to identify the 100-series Block I flight systems (previously called Block IF). The weight reporting for Block I this month is for the zero-series configuration. As the design details of the 100-series systems become firm, the Block I status reporting will begin to represent the 100-series systems.

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Changes from zero-series to 100-series Block I G&N systems include: (1) addition of an horizon photometer and star tracker with associated electronics (2) a redesigned packaging of the flight computer, (3) modification of the electronics packaging to achieve moisture proofing and to solve deficiencies in S&ID thermal interface material, (4) less flammable wiring insulation, and (5) addition of insulation to the cold surfaces.

### 2-6 COMMAND MODULE POWER REQUIREMENTS.

The power requirements of the Command Module G&N equipment on the primary +28 VDC power supply are shown in figure 2-1, which presents the magnitude and location of dissipated power values on a subassembly level. This chart assumes a 14-day lunar orbit mission as defined by S&ID for power profile computation (Ref: S&ID letter 63 MA 7332).

Table 2-III shows the magnitude and location of power dissipation for the established G&N activities, each of which consists of various power levels of operation.

Table 2-IV shows the energy requirements for each G&N activity on a power level basis. The table is based upon MIT letter AG 679-6, "G&N Power Profile Status," dated August 14, 1963. The vertical column to the left indicates the various G&N activities (phases of operation) for the model 14-day mission submitted by S&ID in S&ID letter 63 MA 7332. The column also indicates the power requirement and operating time for each specific activity. The top row indicates the power requirement and operating time of each G&N power consuming equipment. The table sums up the energy consumptions for each G&N activity and each G&N power consuming equipment.

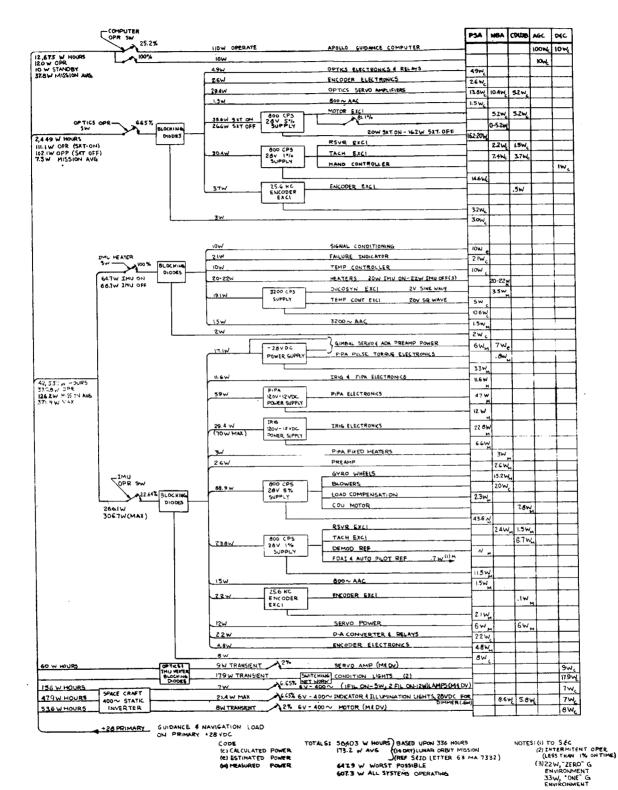


Figure 2-1. Electrical Load on Primary +28 VDC Power Supply

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	Table 2-III.		ominal	Power	Dissipa	tion (w	atts) vs	Nominal Power Dissipation (watts) vs G&N Activity	y	
×0	G&N Activity	NBA	3A		Ъ	PSA		Thermal	D&C	
Ωы	(power levels)	IMU	OBA	CDU JB	IMU	OBA	AGC	Load On S/C Coolant	and S&C	Electrical Load
A	IMU & AGC Operate (1,4)	74.5	0	22.1	233.5	0	110	440.1	10.7	450.8
В	IMU Alignment (1, 2, 4, 6)	74.5	39	44	233.5	63.6	110	564.6	42.7	607.3
U	Low-Orbit Navigation (1, 3, 4, 6)	74.5	33.8	44	233.5	59.8	110	555.6	42.7	598.3
D	Standby & Computing (1, 5)	25.5	0	0.	41.2	0	110	176.7	10	186.7
्राध	Midcourse Navigation (1, 2, 5, 6)	25.5	39	21.9	41.2	63. 6	110	301.2	42	343.2
Γ.	IMU & AGC Standby (5, 7)	25.5	0	0	41.2	0	10	76.7	0	76.7
Ċ	IMU Operate & AGC Standby (4, 7)	74.5	0	22.1	233.5	0	10	340.1	0.7	340.8
		<ol> <li>AGC</li> <li>AGC</li> <li>Optio</li> <li>Optio</li> <li>Optio</li> <li>IMU</li> <li>IMU</li> <li>IMU</li> <li>AGC</li> </ol>	AGC Optics, SXT on Optics, SXT off IMU Operate IMU Standby Display and Control AGC Standby	T on T off tte by d Conti	Ę		120 watts 111.1 watts 102.1 watts 330.8 watts 66.7 watts 45.4 watts 10 watts	watts watts watts watts watts watts watts		

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Table 2-IV. Block I Command Module Power Profile for 14-Day Lunar Orbit Mission

L			Energy Consum	Ē	Energy Consumption (kwh)	abtion (kwh)			
NUON	G&N Activity	(1) AGC Operate 120 watts 84.67 hrs	(2) Optics SXT on 111.1 watts 18.53 hrs	<ul><li>(3) Optics</li><li>SXT off</li><li>SXT off</li><li>102. 1 watts</li><li>3. 83 hrs</li></ul>	(4) IMU Operate 330.8 watts 76.09 hrs	<ul> <li>(5) IMU</li> <li>Standby</li> <li>66. 7 watts</li> <li>260. 32 hrs</li> </ul>	(6) Display & Controls 45.4 watts 22.36 hrs	(7) AGC Standby 10.0 watts 251.74 hrs	Total
<	IMU & AGC Operate 450.8 watts, 56.71 hrs	6. 805	-	1	18.759	ţ	ł	ł	25.564
A	IMU Alignment 607.3 watts, 8.20 hrs	0.984	0.911	1	2.712	ł	0.372	1	4.979
U	Low-Orbit Navigation 598.3 watts, 3.83 hrs	0.459	5	0.391	1.266	. <b>I</b>	0.173	ł	2.289
A	Standby & Computing 186.7 watts, 5.60 hrs	0.672	1	1	1	0.373	ł	1	1.045
<b>M</b>		1. 239	1.147	Ι.		0.689	. 0.468	ľ	3.543
		1	1	ł	-	16.300	<b> </b>	2.443	18.743
U		-	1	ł	2.431	1	ł	0, 073	2.504
	TOTAL	10.159	2.058	0.391	25.168	17.362	1.013	2.516	58.667

# COMMAND MODULE



### Section 3

### BLOCK II COMMAND MODULE DATA

### 3-1 RELIABILITY

The following numbers do not assume the use of in-flight spares or repair but do include the use of a redundant computer. Estimated Command Module G&N reliability is based on the 138-hour mission as defined in the Lunar Landing Mission Design Plan. The changes in reliability result from a refinement of calculations.

Subsystem	Operating Time (hrs) Full Power	Probability of Mission Success
IMU	31	0, 99576**
AGC (2)	19*	0.99996**
DSKY	19	0.99995**
PSA	31*	0.99421**
CDU (5)	31	0.99426***
Optics	18	0. 99804**
Total	G&N System	0. 98229**

Table 3-I. Reliability (as of 7/15/64)

\*Certain assemblies function continuously.

\*\*Changes since last month's report, E-1142 (Rev. 21).

### 3-2 WEIGHTS

Table 3-II presents the weights of all Block II equipment. Refer to section 2-1 for a general explanation of weight reporting.

3-3 REPORTED WEIGHT CHANGES

3-3.1 BELLOWS ASSY. See section 2-2.2.

3-3.2 D&C/AGC (LEB and MP). The 5.4-pound decrease for each D&C/AGC results from the use of smaller relays.

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Table 3-II. Curren	Current Weight Status of Block II Command Module (lbs	tus of Block	t II Comman	d Module (lt	is at 1 g)	
	Ctatuc		Ctatuc		Statue	Design
Item	2/64		5/64		7 /64	Load Wt. $5/64$
	(a)	(b-a)	(q)	(c-b)	(c)	(p)
G&N SYSTEMS						
CDU Assy	15.0(E)	+7.9	22.9(E)	0.0	22.9(E)	
Optical Subsystem		4		<		
SXT	18.2 (C)	+0.2	18.7 (C)	0.0	18.7 (C)	
SCT	13.8 (C)	+0.5	14.3 (C)	0.0	14.3(C)	
Optical Base & Gearing	16.7(E)	+0.3	17.0(E)	0.0	17.0(E)	
<b>Optical Evepieces</b>					•	
SXT	1.3(E)	+0.3	1.6 (E)	0.0	1.6(E)	
SCT	2.3(E)	+0.3	2. () (E)	0.0	2.6(E)	
NVB & Resilient Mounts	22.0(E)	-4.0	18. v (E)	0.0	18.0(E)	
Bellows Assy	13.5 (M)	0.0	13.5 (M)	x .0-	12.7 (M)	
IMU	42.0(E)	0.0	42.0(E)	0.0	$\supset$	
Coolant Hoses (two)	1.0(E)	-0.3	0.7(E)	0.0	0.7 (E)	
Power Servo Assy	41.6(E)	0.0	41.6(E)	0.0	41:6(E)	
G&N Interconnection Assy	35.2 (E)	-5.2	30.0(E)	0.0	30.0(E)	
G&N to S/C Interface Assy	8.0(E)	0.0	8.0(E)	0.0	8.0(E)	
AGC (2 complete computers)	84.0 (E)	+4.0	0	0.0	88.0(E)	3
Optical Shroud	3.5 (M)	-0.4	3.1 (E)	0.0	3.1(E)	
LOWER EQUIPMENT BAY						
D&C				,		
D&C Electronics	1.5(E)	0.0	1.5 (E)	0.0	1.5 (E)	
Control Electronics	2.9(E)	-0.9	2.0(E)	0.0	2.0(E)	
G&N Ind Cont Panel	11.1(E)	0.0	11.1(E)	0.0	11.1(E)	
MDV (includes 2 films)	8.3 (E)	+1.3	9.6(E)	0.0	9.6 (E)	
D&C/AGC	20.6(E)	-0.2	20.4(E)	-5.4	15.0(E)	

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COMMAND MODULE

Table 3-II. Currer	nt Weight St	Current Weight Status of Block II Command Module (lbs) (cont)	k II Comma	nd Module (1	bs) (cont)	
Item	Status 2/64 (a)	(b-a)	Status 6 /64 (b)	(c-b)	Status 7 /64 (c)	Design Load Wt. 5/64 (d)
<u>MAIN PANEL AREA</u> D&C/AGC	20.5 (E)	-0.1	20.4(E)	-5, 4	15.0 (E)	
LOOSE STORED ITEMS Eye Relief Eyepieces Film Cartridges (3) AGC Covers (2) PSA Cover Optics Cover	1.5(E) 1.8(E) 8.5(E) 3.5(E) 1.7(E)	0.0 +0.1 -4.0 0.0 -0.1	1.5(E) 1.9(E) 4.5(E) 3.5(E) 1.6(M)	0.0 0.0 0.0	1.5(E) 1.9(E) 4.5(E) 3.5(E) 1.6(M)	
TOTAL	400.0* Control Weight	0.0	400.0	-11.6	388.4	492.6**
*Control Weight specified in letter ( Mr. M. Trageser, MIT/IL. See pa **Design Load Weight taken from Sé Does not include loose stored items	r (PG-64-113, M paragraph2-1.2. S&ID letter 63 M ns.	fied in letter (PG-64-,13, March 6, 1964) from Mr. IT/IL. See paragraph 2-1.2. : taken from S&ID letter 63 MA 2032, February 11, 1 e stored items.	, 1964) fron 2, Februar	1 Mr. D. G.	D. Glbert, ASPO 964.	3

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### 3-4 BLOCK II WITH DIGITAL STABILIZATION AND CONTROL FUNCTIONS

The Block II Command Module G&N System reported here is the system concept planned until June 4, 1964. On this day, MSC reoriented the Block II G&N System to include spacecraft powered and free fall stabilization and control functions (Ref: minutes of meeting, S&ID, MIT/IL, and MSC, Implementation Meeting No. 1, June 4, 1964, MSC, Houston, Texas).

The effect of these changes on system hardware has not yet been fully assessed and will not be reflected in this report until next month.

### **3-5 POWER REQUIREMENTS**

The power requirements of the Block II Command Module G&N equipment on the primary +28 VDC power supply are shown in figure 3-1, which presents the magnitude and location of dissipated power values on a subassembly level. This chart assumes a 14-day lunar orbit mission as defined by S&ID for power profile computation (Ref: S&ID letter 64 MA 3540).

Table 3-III shows the energy consumptions on a G&N activity and G&N equipment basis. The vertical column to the left indicates the various G&N activities (phases of operation). This column also indicates the power requirement and operating time for each specific activity. The top row indicates the power requirement and operating time of each G&N power-consuming equipment.

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### BLOCK II

# COMMAND MODULE

20 W STANDB 17.1 WMISSION A	(MAK)	4	100 W								<u> </u>
210 W OPERATE 20 W STANDE 47.1 W MISSION A	(MAK)					APOLLO GUIDANCE COMPUTER PRIMARY	4			90W c	10Ws
20 W STANDB 47.1 WMISSION A			£0W				1			200	
						OPTKS ELECTRONICS & RELAYS					
<b></b>			304 W	_		OPTICS SERVO AMPLIFIERS	4.9%				
· ·-			1.5W			800~ AAC		15.2 W			
· ·-							1.5 W	<u> </u>	<u> </u>		ļ
OPTICS	0PR	BLOCKING	34.W	800 CPS 28V 5% SUPPLY		HOTOR EXCI			<u> </u>		
SW	<u>`</u>	DIODES		SOPPLY				15.2W			
594 W HOURS 130.7 W DPR 8.7 W MISSION A						RSVR EXCI	ABW	·	<u> </u>		
at w mission a	VG		21.5W	280 CPS		TACH EXCI	]—-	2.2 W	i		<u> </u>
				SUPPLY		HAND CONTROLLER	}	7.4W			
				L_				ļ		<u> </u>	I₩ <sub>C</sub>
			LIOW			PHOTOMETRY	10.94			<u> </u>	-
			194 W	3V SUPPL		ELECTRONIC COU	iowe		1		<b> </b>
				L					944		
			Céw			ELECTRONIC COU	}		10 We 6We		
			<u>3w</u>				- 3W.			<u> </u>	$\vdash$
			JOW .				<u> </u>				
	IMU HEATER		2.IW			SIGNAL CONDITIONING	10we				
	SW WCX		low				2.1Wc				
	56.5 W IMU ON	DIODES	20-22W	· · · · · ·		TEMP CONTROLLER	iow,				
	58.5W IMU OFF					HEATERS 20W IMU ON-22W IMU OFF(3)	1	20-22			
		1	10.9 W	SUPPLY	·	DUCOSYN EXCL 2V SINE WAVE		3.5w			
			1.5W	L		3200 ~ AAC	7.4%	1			
		L_	2w			AAL	1.5W				
					_	CINEAL SERVE ADA DEFAND DA	zw,				
				-28VDC		GIMBAL SERVO ( ADA PREAMP POWER	6W,	7 w			
			ſ	POWER SUP	·PLY	PIPA PULSE TORQUE ELECTRONICS	1	.8w			
			2.3W	۲ <u>ــــ</u>			3.5W				
5,05C W HOURS			2.5W			IRIG ELECTRONICS	2.3Wc				
97.3 W FINE ALIGN				PIPA # JRK	۶ <del> </del>	PIPA ELECTRONICS	494W				
109 W MISSION AVE			61.4W 73.5W FINE ALIGN	POWER SUPP	<u> </u>	SWITCH					
			SWON			IRIG ELECTRONKS	10.1 W				
			30.1W				12-14				
				3V SUPPLY	·	ELECTRONIC COU			15,1 W		
			<u>9</u> w						15 W.		
			2.6 W			PREAMP	i		9 W.		
	71411					RSVR_EXCI	- 	2.6W			
	OPR SW		9.IW	800 CPS		DEMOD REF	L	2.4 ¥			
	25,78	BLOCKING		SUPPLY		FDAI & AUTO PLOT REF .7We	11/1				
	228.7 W	DIODES				/we					
	240.8 W FINE ALIG		1.5W			800~ AAC	5W,				
			1			GYRO WHETLS	1.5W				
			48.4W	800 CPS 28V 5% 0		BLOWERS	1	7.6 W			
				SUPPLY		PIPA FIXED HEAT	1	10 4			
			1		····· •			5 W.			
					-	GYRO WHEELS	258y				
			39.2W	800 CPS		BLOWERS		7.6 W			
				28V5%C	φB			iow,			
					- 1	······································	1				
			aw	h	···		21.6¥				
		·	×			······································	8Wc	~~~	]		
											1
5 W HOURS		OPTICS P	9W TRANSIENT	<u>2%</u>		SERVO AMP (MOV)	$\vdash$				
		INU HEATER BLOCKING DIODES	17.9 W TRANSIEN		SWITCHIN	G CONDITION LIGHTS (2)	1				9W.
8 W HOURS			7W	6A4%]	NET WOR	(IFIL ON - 5W, Z FIL ON-12W)LAMPS (ME DV)					- 4
O W HOURS	SPACE CRAFT 400~ STATIC		15.6 W MAX,	6.44%	V-400	K] (IFIL ON - & W, Z FIL ON - /2W)LAMPS(M(DV) → INDICATOR & ILLUMINATION LIGHTS, 28 VOC FOR → MOTOR (M(DV) PIMMER(.6M)	}				7W.
19 W HOURS	INVERTER	<u>.</u>	OW TRANSIENT	12% 6	V-400	~ MOTOR (M ( DV) DIMMER (.6W	┠┵┥	B.6W			7Wc
-											8w <sub>c</sub>
			NAVIGATION LOAD								
-	c	N PRIMARY			-						
			CODE (C) CALCULATEI	POLIER	TOTALS	5: 53,812 W HOURS) BASED UPON 308,3 HOUR 167 W AVG (4 DAY)LUNAR ORBIT MISSI J(REP. SEID LETTER 63 M	95 //w	,	NOTES:	i) TO :	S C RHITEN

Figure 3-1. Electrical Load on Primary +28 VDC Power Supply

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Table 3-III. Block II Command Module Power Profile for 14-Day Lunar Orbit Mission

	BUMMARY OF BLOCK II COMMAND MODULE ENERGY CONSUMPTION (Kilowatt Hours)	II COMMAND	MODULE ENF	SRGY CONSUM	IPTION (Kilow	att Hours)			
		-	2	3	4	5	ه	6	
Operating Mode	G& N ACTIVITY	One Operate AGC Operate 120 wathours 130 wathours	TWO DET 210 Walte 3.10 hour	AGC any Standing 20 Wa hour	THATU THE	TINUT OF BUT	Deratette Operatette 38.6 hours 18.85 hours	Optice te Optice te 130.95 hours	TOTAL
×	Accomplish & confirm course corrections Inactivity & Monitor 405, 2 watts 55, 72 hrs.	6.686			15, 891				22.577
É	Alignments Landmark Trackings SXT Sightings 575. 5 watts 12.69 hrg.	1. 523			3,619		0. 503	1. 658	7.303
υ	Star Occultation Sightings 178.5 watts 2,90 hrs.	0. 348				0,170			0. 518
Q	SXT Sightings (Midcourse) 348,8 watts 7.16 hrs.	0 859				0, 418	0. 283	0. 936	2. 496
þ	Inactivity & Monitor 78.5 watts 217.31 hrs.			4, 346		12, 713			17. 059
ír,	Inactivity & Monitor 305, 2 watts 8,09 hrs.			0.162	2. 307				2.469
U	Computer Updates Major Maneuvers 495,2 watts 2.97 hrs.		0.624		0.847	•			1. 471
×	. Computer UpdateB 268,5 watta 0.73 hrs.		0,153			0.043			0.196
	TOTAL 308.30 hours	9.416	0.777	4, 508	22,664	13. 344	0.786	2, 594	54, 089

BLOCK II COMMAND MODULE

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### 3-6 STATUS OF COMMAND MODULE AGC PROGRAMS

Table 3-IV lists current Command Module memory estimates and the status of AGC programs. The status of LEM AGC programs is not reported at this time.

A high and low word estimate is given with each program. Each status is defined as follows:

- (1) Planning stage
- (2) Programming stage
- (3) Checkout on AGC simulation
- (4) Checkout on G&N simulation
- (5) Checkout on AGC

Table 3-IV.	Current Memory	Estimates a	and the Status
of	Command Module	AGC Progra	ams

		-	Estimate ords)
Program	Status	High	Low
List Processing Interpreter	(5)	1712	1712
AGC Executive	(5)	253	253
AGC Waitlister	(5)	145	145
AGC System Exerciser	(5)	500*	294*
G&N System Exerciser	(4)	650	400
Display, Keyboard, and			
Telemetry	(5)	2000	2000
Input/Output Control	(5)	1750*	$1275^{*}$
Midcourse & Orbital Navigation	(5)	2000*	1500*
Midcourse & Orbital Guidance	(3)	500	500
Pre-Launch Platform Alignment	(5)	400*	350*
In-Flight Platform Alignment	(4)	1024	900
Re-Entry Control	(4)	1800	1200
Injection and De-Boost	(4)	1000	400
Restart	(5)	500*	200*
Aim-Point Determination			
& Abort	(1)	4000	2000
Totals		18234	13129

\*Programs in stage (5) whose low and high estimates are not identical reflect an anticipated increase in computational facility.

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#### Section 4

### LUNAR EXCURSION MODULE DATA

### **4-1 RELIABILITY**

The numbers in table 4-I do not assume the use of in-flight spares or repair. Changes in reliability values result from a refinement in calculations. The estimated reliabilities are based on MIT/IL's Guidance Monitor System Note No. 3, dated January 23, 1964.

•	Subsystem	Operating Time (hrs)	Probability of Mission Success
	IMU	6.25	0.99914
<ul> <li>Ality Antipation of Street, and Ality</li> </ul>	AGC	6.25	0.99768*
	PSA	6.25	0.99928*
and the second second	CDU (5)	6.25	0.99897*
	OMU	0.75	0.99997
	Total G&N S	ystem	0.99505*

### Table 4-I. Reliability (as of 7/15/64)

\*These values have changed since the last report (Rev. 21).

### 4-2 WEIGHTS FOR LEM

Lunar Excursion Module weights are presented in table 4-II. In general the data conform to the information contained in paragraphs 2-1, 2-1.1, and 2-1.2.

The row labeled "Bare Guidance System" is inserted to provide for comparisons with similarly specified systems.

At NASA coordination meeting L6A, May 26 and 27, 1964, the installation configuration of the telescope and IMU was changed from the existing installation, wherein the IMU was inside the LEM pressure shell, to an outside configuration. Moreover, the vibration environment recently specified in preliminary ICD LIS-520-10001, dated May 26, 1964, "LEM Design Environment," states levels which are much greater than anticipated in the G&N design. Vibration isolation mounts for the telescope and IMU

Table 4-II. Estimated Weichts of LEM GaN Components (IDS ILD Status         Status         St							
$Z_{1}$ (0=4)         (b-a)         (b)         (c-b)         (c)           (a)         (b-a)         (b)         (c-b)         (c)         (c) $Z_{15}$ (E) $U_{10}$ $Z_{2}$ (E) $U_{10}$ $Z_{2}$ (C)         (c) $Z_{15}$ (E) $U_{10}$ (c) $Z_{15}$ (E) $U_{10}$ $Z_{15}$ (E) $U_{10}$ $Z_{15}$ (E) $U_{10}$ $Z_{15}$ (C) $Z_{16}$ (C)	ſable 4-II.	mated Weig Status	nts of LEM	GEN COMPO Status	nents (108 8	Status 5.00	Design Load Wt.
I5.0 (E) $+7.9$ 22.9 (E)0.022.9 (E)24.5 (E)0.024.5 (E)0.024.5 (E)2.0 (E)0.02.0 (E)0.02.0 (E)5.0 (E)0.02.0 (E)0.02.0 (E)5.0 (E)0.042.0 (E)0.042.0 (E)42.0 (E)0.010.0 (E)0.042.0 (E)10.0 (E)0.019.5 (E)0.042.0 (E)10.0 (E)0.019.5 (E)0.010.0 (E)19.5 (E)0.019.5 (E)0.015.0 (E)19.5 (E)0.019.5 (E)0.015.0 (E)2.0 (E)0.019.5 (E)0.024.8 (E)2.10 (E)0.024.8 (E)0.024.8 (E)2.24 (E)0.024.4 (E)0.024.8 (E)2.4 (E)0.024.8 (E)0.024.8 (E)2.10.0 * $+5.5$ 110.80.024.8 (E)2.11.9108.3 $+2.5$ 110.80.02.11.9108.3 $+2.5$ 110.82.11.1108.3 $+2.5$ 110.82.11.1108.3 $+2.5$ 110.82.11.12.11.221.421.64 (E)that been ass	Item	2/6 <del>4</del> (a)	(b-a)	(p)	(c-b)	1/64 (c)	(d)
24.5(E) $0.0$ $24.5(E)$ $0.0$ $24.5(E)$ $0.0$ $24.5(E)$ $5.0(E)$ $0.0$ $2.0(E)$ $0.0$ $2.0(E)$ $0.0$ $2.0(E)$ $5.0(E)$ $0.0$ $42.0(E)$ $0.0$ $42.0(E)$ $0.0$ $2.0(E)$ $42.0(E)$ $0.0$ $19.5(E)$ $0.0$ $19.5(E)$ $-4.5$ $15.0(E)$ $19.5(E)$ $0.0$ $19.5(E)$ $0.0$ $10.0(E)$ $0.0$ $42.0(E)$ $8$ $15.0(E)$ $0.0$ $19.5(E)$ $-4.5$ $15.0(E)$ $10.0$ $8$ $15.0(E)$ $0.0$ $10.0(E)$ $0.0$ $2.0(E)$ $2.0(E)$ $8$ $15.0(E)$ $0.0$ $2.0(E)$ $0.0$ $2.0(E)$ $2.0(E)$ $8$ $2.0(E)$ $0.0$ $2.2(E)$ $2.2(E)$ $2.2(E)$ $2.2(E)$ $8$ $2.0(E)$ $0.0$ $2.2(E)$ $2.2(E)$ $2.2(E)$ $2.2(E)$ $8$ $2.0(E)$ $0.0$ $2.2(E)$ $2.2(E)$ $2.2(E)$ $2.2(E)$ $2.2(E)$ $8$		15.0 (E)	+7.9	22. 9 (E)	0.0	22.9(E)	*
5.0 (E)0.05.0 (E)0.05.0 (E)42.0 (E)0.042.0 (E)0.042.0 (E)42.0 (E)0.010.0 (E)0.010.0 (E)10.0 (E)0.010.0 (E)0.015.0 (E)19.5 (E)0.019.5 (E)0.015.0 (E)19.5 (E)0.019.5 (E)0.015.0 (E)19.5 (E)0.019.5 (E)0.02.0 (E)19.5 (E)0.019.5 (E)0.02.0 (E)2.0 (E)0.024.0 (E)0.024.8 (E)24.8 (E)0.024.8 (E)0.024.8 (E)24.8 (E)0.024.8 (E)0.024.8 (E)24.8 (E)0.024.4 (E)0.024.8 (E)24.4 (E)0.024.4 (E)0.024.8 (E)24.8 (E)0.024.4 (E)0.024.4 (E)210.0 * $+6.4$ $216.4$ $-4.5$ $211.9$ 210.0 * $+5.5$ $110.8$ 0.0 $24.4$ $veight$ $veight$ $0.0$ $24.4$ $0.0$ $veight$ $108.3$ $+2.5$ $110.8$ $0.0$ $virthas been assigned.110.80.0110.8v/IL.See section 2-1.2.1964) from Mr. D. Gilbert,$	cope and All Eyepieces	24.5(E) 2.0(E)	0.0	24.5(E) 2.0(E)	0.0	24.5(E) 2.0(E)	ан 1917 - Солон Солон 1917 - Солон Со
5.0 (E)       0.0       5.0 (E)       0.0       5.0 (E)         42.0 (E)       0.0       42.0 (E)       0.0       42.0 (E)         10.0 (E)       0.0       19.5 (E) $-4.5$ 15.0 (E)         19.5 (E)       0.0       19.5 (E) $-4.5$ 15.0 (E)         2.0 (E)       0.0       19.5 (E) $-4.5$ 15.0 (E)         41.5 (E)       0.0       2.0 (E)       0.0       2.0 (E)         41.5 (E) $+2.5$ 44.0 (E)       0.0       2.3 (E)         4.3 (E) $-2.0$ 2.4 (E)       0.0       2.4 (E)         24.8 (E) $0.0$ 2.4 (E) $0.0$ 2.4 (E)         24.6 (E) $0.0$ $2.4 (E)$ $0.0$ 2.4 (E)         210.0 * $+5.5$ $110.8$ $0.0$ $2.4 (E)$ $210.0 *       +2.5 110.8 0.0 2.4 (E) 210.1 *       -4.5 2.11.9$	igit Readout for					ļ	
42.0 (E)       0.0       10.0 (E)       0.0       10.0 (E)       0.0       10.0 (E)       10.0         19.5 (E)       0.0       19.5 (E)       0.0       19.5 (E)       -4.5       15.0         19.5 (E)       0.0       15.0 (E)       0.0       15.0 (E)       0.0       20.0         19.5 (E)       0.0       15.0 (E)       0.0       15.0 (E)       0.0       215.0 (E)         2.0 (E)       0.0       2.0 (E)       0.0       2.0 (E)       0.0       2.0 (E)         41.5 (E) $+2.5$ 44.0 (E)       0.0       2.0       2.3 (E)       2.4 (E)         24.8 (E)       0.0       2.4 (E)       0.0       2.4 (E)       0.0       2.4 (E)         24.8 (E)       0.0       2.4 (E)       0.0       2.4 (E)       0.0       2.4 (E)         24.4 (E)       0.0       2.4 (E)       0.0       2.4 (E)       0.0       2.4 (E)         210.0 *       4.1 (E)       0.0       2.4 (E)       0.0       2.4 (E)       0.0       2.4 (E)         210.0 *       2.4 (E)       0.0       2.4 (E)       0.0       2.4 (E)       0.0       2.4 (E)       2.4 (E)         210.0 *       2.1 (E)       0.0	ule	5.0(E)	0.0	5.0(E)	0.0	5.0(E) 43.0(F)	
10.0 (E)       0.0       10.0 (E) $0.0$ 10.0 (E)         19.5 (E)       0.0       19.5 (E) $-4.5$ 15.0 (E)         15.0 (E)       0.0       15.0 (E)       0.0       15.0 (E)         2.0 (E)       0.0       2.0 (E)       0.0       2.0         41.5 (E) $+2.5$ $44.0 (E)$ 0.0       2.0         41.5 (E) $+2.5$ $44.0 (E)$ 0.0       2.0         24.8 (E)       0.0       2.4 (E)       0.0       2.3         24.8 (E)       0.0       2.4 (E)       0.0       2.4         210.0 * $+6.4$ 216.4 $-4.5$ 211.9         Control       Weight       0.0       2.4 (E)       0.0       2.4         108.3 $+2.5$ 110.8       0.0       2.4       2         211.9       Control       Weight       108.3 $-4.5$ 2       2         211.1.2       108.3 $+2.5$	DCA Interconnection	42.U(E)	0.0	(m) 0 .2#	> >		
y and Controls 19.5 (E) 0.0 19.5 (E) -4.5 15.0 ( ay and Controls 15.0 (E) 0.0 15.0 (E) 0.0 15.0 ( beedures, etc 2.0 (E) 0.0 2.0 (E) 0.0 2.0 ( 41.5 (E) +2.5 44.0 (E) 0.0 2.0 2.3 ( 24.8 (E) 0.0 24.8 (E) 0.0 2.4 (E) 0.0 2.4 ( 24.8 (E) 0.0 24.8 (E) 0.0 2.4 (E) 0.0 0 0.0 2.4 (E) 0.0 0 0.0 2.4 (E) 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0		10.0(E)	0.0	10.0(E)	0.0	0	
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2.4(E)       0.0       2.4(E)       0.0       2.4(E)         210.0*       +6.4       216.4       -4.5       211.9         Control       Weight       -4.5       211.9         Nuter)       108.3       +2.5       110.8       0.0       110.8         Inter)       108.3       +2.5       110.8       0.0       110.8         Intr/IL.       See section       2-1.2.       8       106.1       6       1964) from Mr. D. Gilbert, ght has been assigned		24.8(E)	0.0	xo ·	0.0	24·0(E)	
210.0*       +6.4       216.4       -4.5       211.9         Control       Weight       9       9       9       10.0         Neight       108.3       +2.5       110.8       0.0       110.8         Inter       108.3       +2.5       110.8       0.0       110.8         Intr/IL.       See section       2-1.2.       5       5       5         Intr/IL.       See section       2-1.2.       5       5       5         Intr/IL.       See section       2-1.2.       5       5       5         Intr       As been assigned       1.13       5       5       5       5	over	2.4(E)	0.0	4	0.0	4	
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Neight     Weight       Nuter)     108.3       +2.5     110.8       0.0     110.8       ified in Letter PG-64-113 (March 6, 1964) from Mr. D. Gilbert, MIT/IL. See section 2-1.2.       MIT/IL. See section 2-1.2.       ght has been assigned.	· · ·	Control					
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cified in Letter PG-64-113 (March 6, 1964) from Mr. D. Gilbert, MIT/IL. See section 2-1.2. ght has been assigned.	Guidance System I, PSA, and computer)	108.3	+2.5	110.8	0.0	110.8	
MIT/IL. See section ght has been assigned.	trol Weight specified in Le	tter PG-64-	113 (March	6, 19 <b>64)</b> fr	m Mr. D. (	filbert, AS	0
	MIT/IL. ght has bee	See section on assigned.					

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would be required. However, at NASA Coordination Meeting L7A, June 4, 1964, GAEC lowered its estimate of flight vibration environment by a factor of 5. Accordingly, the vibration mounts were removed. The design changes resulting from this activity are not yet reflected in this weight report.

4-3 REPORTED WEIGHT CHANGES

4-3.1 AGC DISPLAY AND CONTROLS. See section 3-3.2 for an explanation of the 4.5-pound decrease.

**4-4 POWER REQUIREMENTS** 

The estimate for LEM power and energy consumption shown in figure 4-1 is based upon recent Command Module G&N Block II data and preliminary ICD LIS-390-2, LEM Electrical Load Analysis Form.

Table 4-III shows the energy requirements for each G&N activity on a power level basis. The table is also based upon LEM ICD LIS-390-2. The vertical column to the left indicates the various G&N activities (phases of operation). The column also indicates the power requirement and operating time for each specific activity. The top row indicates the power requirement and operating time of each G&N power consuming equipment. The table sums up the energy consumption for power consuming equipment.

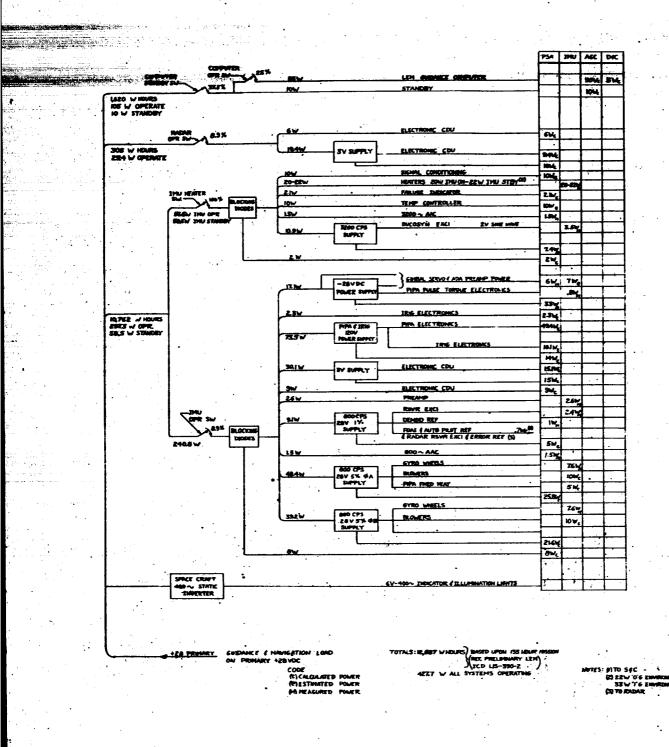


Figure 4-1. Electrical Load on Primary +28 VDC Power Supply

PICE 4-4

Total 5, 013 0, 085 1. 373 1, 075 12.659 5. 113 Negligible Negligible Negligible I 1. I 0.398 0, 303 0, 005 Table 4-III. LEM Power Profile Based on LEM ICD LIS-390-3 I ł I ú 1975 ST. (57) 7.204 0, 918 5. 113 1. 17**3** ł I Way to 3. 484 3. 643 0, 059 978 4 8 . . /) (198) 4 8 . . . /) (198) 4 8 . . . . /) . ۱ I 4 0.357 0, 157 0, 20 ..... Lan 1 2 ption in Kilowatt Big 97 4 4 4 Jos 10 1. 252 0, 021 **8** 1 I ł \*\*\*\*\* 0 .0 0, 000 0,000 Bummary of Lunar Excursion Module Energy Cons I ۱ Į. ۱ 200 427.7 watte Guidance During Major Event 0.20 hours 427.7 watts 58. 5 watts 68. 5 watts 68. 5 watte Inscitvity Alignment Midcourse Messurements 11,72 bours 427,7 we LEM GAN Aptivity inactivity 87.40 hours Inactivity 20.05 hours Inactivity 15.70 hours **Total Hours** Mode Ħ ₽. ≽ Ħ -

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### Section 5

### GLOSSARY AND SYSTEM DEFINITION

### Apollo Guidance Computer (AGC)

<u>CM BLOCK I</u> A single complete flight computer containing all logic, memory, associated power supplies, and all interface circuits except those identified with the CDU's. Does not contain the associated displays and controls.

Consists of two trays containing replaceable electronic modules, the AGC end connector, and toe plate. Does not include the necessary cold plate or the G&N to S/C Interface Assembly which is located in the adjacent area. Space exists for carrying an extra spare pair of AGC trays. These would not function in this spares location but could interchange with faulty trays in the active position. The spare trays are reported separately.

<u>CM BLOCK II</u> Two complete and active computers each having the same functions as the Block I AGC. Consists of two wiring matrix headers mounted on each side of the cold plate. This cold plate is not included in this accounting and must be moved up from the Block I configuration location. The modules of the "X" computer mount on one of these headers, those of the "Y" computer on the other.

Block I and Block II AGC's are not interchangeable.

LEM A single complete flight computer having the same functions as one of the Block II computers. Unless installation constraints yet to be determined prevent it, the LEM computer will be physically identical with the Block II computers.

### AGC Covers

CM BLOCK I Not required.

<u>CM BLOCK II</u> Two covers, one for each computer, may be required if it becomes necessary to seal the Malco connectors against moisture.

LEM Same as Block II except that there is only one cover.

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#### AGC Spares

### CM BLOCK I Spare AGC logic and memory trays.

CM BLOCK II AND LEM No spares.

#### Alignment Optical Telescope (AOT)

CM BLOCK I AND BLOCK II Not in CM; see Optical Subsystem.

<u>LEM</u> A 3-position periscope with single-degree-of-freedom manually read reticule for alignment of the IMU. Includes the weight of the bellows assembly and the longeye-relief eyepiece.

### Bellows Assembly

<u>CM BLOCK I AND CM BLOCK II</u> Flexible pressure seal between CM structure and optical subsystem on NAV BASE for penetration of pressure hull with optics.

<u>LEM</u> One bellows with a double convoluted wall and two seals providing a flexible seal for pressure penetration of the AOT in the spacecraft. This weight is included in the AOT value.

### Book of Procedures

CM Not in CM; see MDV.

<u>LEM</u> Book or other form of maps, charts, procedures, instructions, etc., needed for lunar operations.

#### Coupling Data Unit (CDU) Assembly

The CDU provides the necessary signal interfaces among the IMU gimbal angles, optics gimbal angles, radar gimbal angles, angle registers in the AGC, the spacecraft autopilot attitude error signals, and the tracking radar command error signals.

<u>CM BLOCK I</u> Five interchangeable gear boxes each with necessary motor tachometer, resolver synchros, and encoder with mounting frame work. Does not include associated electronics which are located in the PSA.

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<u>CM BLOCK II</u> Functionally identical to Block I except the instrumentation is all electronic. Includes all support electronics (including special power supply) and header; is located in same volume as Block I CDU's. Changes in resolver synchro characteristics and mode controls make Block I and II CDU's noninterchangeable.

LEM Interchangeable with CM Block II CDU's except for the headers.

### Cold Plates

<u>CM BLOCK I, BLOCK II, AND LEM</u> Cold plates for the IMU are built into the IMU. Necessary cold plates for electronics are part of the equipment supplied by the spacecraft manufacturer.

### Control Electronics Assembly

<u>CM BLOCK I</u> Consists of one power transformer, one relay and diode module, and a bracket end connector. Used to support display and control functions.

CM BLOCK II May be relocated with other similar functions.

LEM Not defined in LEM.

### Coolant Hoses

<u>CM BLOCK I AND CM BLOCK II</u> Consists of (1) two aluminum flex coolant hoses, one between IMU and spacecraft and one between optics and spacecraft, (2) bracket assembly screws and clamp, and (3) entrapped coolant. Note that a third aluminum flex coolant hose between the optics and the IMU is considered as part of the weight of the optics base.

LEM Not identified as part of LEM.

Display and Control/Apollo Guidance Computer (D&C/AGC)

<u>CM BLOCK I</u> Number displays and keyboard control associated with the operation of the AGC. Two functionally identical and parallel operation units: one in lower equipment bay and one on main panel between left and center couches.

<u>CM BLOCK II</u> Functionally identical to Block I but smaller configuration because of smaller relays.

LEM Identical to Block II except only a single unit is required.

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### D&C Electronics Assembly

<u>CM BLOCK I</u> Consists of a chassis, a relay and diode module, a demod. elect. module, a saturable reactor, a time delay module, a connector, and wiring. Used to support display and control functions.

CM BLOCK II Not defined at this time.

LEM Not defined in LEM at this time.

### Eye Register for Reticule

CM Not in CM.

<u>LEM</u> Device or equipment not yet defined in detail, to position the LEM pilot's eye to use the window marking reticule pattern for landing point observation and selection during the constant flight path phase of landing.

### Film Cartridges

<u>CM BLOCK I AND BLOCK II</u> Consists of film cartridges and film for map and data viewer.

LEM Does not exist in LEM.

### G&N Indicator Control Panel

<u>CM BLOCK I AND BLOCK II</u> Consists primarily of controls and displays for the operation of the optics, MDV, IMU temperature control, panel brightness control, and attitude impulse control. It includes display and control elements, panel, panel wiring, and supporting hardware. Block II panel will probably contain horizon photometer controls also.

LEM Not defined at this time for LEM.

### <u>G&N Interconnection Assembly</u>

<u>CM BLOCK I</u> Consists of PSA End Connector Assembly and interconnect wiring harness which electrically ties together the assemblies that constitute a completely integrated system. This term does not include the G&N to S/C Interface Assembly weight or the weights of harness support brackets which are an NAA responsibility.

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CM BLOCK II Similar to Block I but not interchangeable with Block I.

<u>LEM</u> Not clearly defined but at present is called the AGC/PSA Interconnection Assy. Because of the wide separation of G&N components, most interconnection will be accomplished as part of spacecraft wiring.

### <u>G&N to S/C Interface Assembly</u>

<u>CM BLOCK I</u> Interconnections between the spacecraft wiring channel, the computer end connector, and the PSA end connector. Contains no active electronics. The G&N Harness Tray Assy is also included as part of this assembly.

<u>CM BLOCK II</u> Similar in function to Block I except the configuration is much different and not interchangeable with Block I.

LEM Not identified yet as a separate item in LEM.

### Horizon Photometer

<u>CM BLOCK I</u> Only 100-Series Systems will have a horizon photometer and star tracker, using a Block II optical sextant. Zero-series Block I weights do not include an horizon photometer.

<u>CM BLOCK II</u> An earth horizon brightness photometer and automatic star tracker for navigation measurements against the earth's illuminated limb. The sensors are incorporated into the head of the SXT, the weight of which includes this function. The PSA includes support electronics.

<u>LEM</u> Not part of LEM.

### Inertial Measurement Unit (IMU)

<u>CM BLOCK I</u> Size 14 IMU (14-inch case diameter) gimbal assembly including all parts inside hermetic case and including entrapped coolant.

<u>CM BLOCK II</u> Size 12.5 IMU functionally interchangeable with Block I unit, but not physically interchangeable with Block I.

LEM Size 12.5 IMU as described above.

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### IMU Control Panel

<u>CM BLOCK I</u> Consists of panel, wiring, attitude error meter, CDU transfer switch, manual alignment switch, CDU mode control switches, connector, and supporting hardware.

<u>CM BLOCK II</u> Does not exist in Block II. Moding is done by AGC program and AGC push buttons.

LEM Not defined at this time for LEM.

### Long-Eye-Relief Eyepieces

<u>CM BLOCK I AND BLOCK II</u> Consists of a SXT and a SCT eyepiece to provide eye relief of at least 1.6 inches for closed-visor operation. Used in place of normal eyepieces of SXT and SCT.

 $\underline{\text{LEM}}$  Long-eye-relief eyepiece for the AOT is included as part of the AOT in this accounting.

### Map and Data Viewer (MDV)

<u>CM BLOCK I AND BLOCK II</u> Film viewer for display of maps, charts, procedures, etc. Weight includes one film cartridge for Block I MDV and tentatively two for Block II MDV.

LEM Not in LEM; see Book of Procedures.

### NVB and Resilient Mounts

<u>CM BLOCK I</u> Rigid beryllium structure supporting the IMU and the optical subsystem with its associated hardware. The NVB is attached to the spacecraft using flexible resilient mounts to prevent spacecraft strains from distorting the NVB and the alignment between the IMU and Optics. These mounts also provide shock and vibration attenuation.

<u>CM BLOCK II</u> Functionally similar to Block I but will be lighter and provide for mounting the size 12.5 IMU.

<u>LEM</u> The need for tieing the AOT and IMU together exists but is accomplished by using structure provided by the spacecraft contractor. See paragraph 4-2.

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### Optical Eyepieces

CM BLOCK I AND BLOCK II Removable SXT eyepiece and SCT eyepiece.

LEM Included as part of the AOT.

### Optical Subsystem

<u>CM BLOCK I</u> Consists of SXT, SCT, Optical Base, and associated hardware defined as follows:

SXT:	Sextant a two-line-of-sight, narrow-field, two- degree-of-freedom sextant and its attached gearing.
SCT:	Scanning Telescope a single-line-of-sight, wide- field-of-view, two-degree-of-freedom articulation optical instrument and its attached gearing.
OPTICAL BASE:	Base for SXT and SCT with associated gearing and internal cooling. Includes the weight of the coolant hose between the IMU and Optical Base.

<u>CM BLOCK II</u> Similar to Block I except for changes in the sextant to provide line-ofsight velocity control directly without CDU's. The horizon photometer and automatic star tracker are incorporated into the SXT.

LEM Not in LEM; see AOT.

### Optical Shroud & Cover Assembly

CM BLOCK I AND BLOCK II Consists of the optical shroud and protective cover.

LEM Does not exist in LEM.

### Power Servo Assembly (PSA)

<u>CM BLOCK I</u> Consists of most of the support electronics: power supplies; IMU, Optics, and CDU servos; IMU temperature control; accelerometer and gyro pulse torquing; and signal conditioning electronics. Consists of 10 trays with replaceable modules which plug into the PSA end connector assembly. Includes front toe plate but not the cold plate.

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<u>CM BLOCK II</u> Similar in function to Block I but does not contain the CDU servos and signal conditioning electronics needed in Block I. Includes electronics for horizon photometer and automatic star tracker. Consists of a single plane matrix header to mount onto the cold plate with the modules plugging onto the top.

<u>LEM</u> Consists of electronics similar to those identified in the Block II PSA minus various electronics modules. Does not include CDU, Optics, and Photometry electronics associated with the Block II PSA.

#### PSA End Connector Assembly

<u>CM BLOCK I</u> Electrical interconnection between the PSA trays, the G&N Interconnection Assy, and the G&N to S/C Interface Assy. The End Connector weight is reported in the G&N Interconnection Assembly weight.

<u>CM BLOCK II & LEM</u> Not identified as a separate item; will be part of the PSA matrix header.

### PSA Covers

CM BLOCK I Not required.

CM BLOCK II Cover to protect the PSA module connections from moisture during flight.

LEM Same as Block II except lighter in weight.

### Signal Conditioner Assembly

CM BLOCK I AND II & LEM Condition signals for telemetry.

### Two-Digit Readout for Reticule

CM Not in CM.

<u>LEM</u> A 2-digit readout driven by the AGC from 00 to 99 to indicate range component of landing point using fixed numbered scale on window reticule.

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