General Disclaimer

One or more of the Following Statements may affect this Document

- This document has been reproduced from the best copy furnished by the organizational source. It is being released in the interest of making available as much information as possible.
- This document may contain data, which exceeds the sheet parameters. It was furnished in this condition by the organizational source and is the best copy available.
- This document may contain tone-on-tone or color graphs, charts and/or pictures, which have been reproduced in black and white.
- This document is paginated as submitted by the original source.
- Portions of this document are not fully legible due to the historical nature of some of the material. However, it is the best reproduction available from the original submission.

Produced by the NASA Center for Aerospace Information (CASI)

(212)



NATIONAL AERONAUTICS AND SPACE ADMINISTRATION MSC INTERNAL NOTE NO. 68-FM-117

MAY 15, 1968

RTCC REQUIREMENTS FOR MISSIONS F AND G: SELENOGRAPHIC-MNBY VELOCITY TRANSFORMATION FORMULATION

By Paul F. Flanagan, Mathematical Physics Branch

(This revision supersedes MSC Internal Note No. 68-FM-98 dated April 19, 1968.)

MISSION PLANNING AND ANALYSIS DIVISION

MANNED SPACECRAFT CENTER HOUSTON, TEXAS

(ACCESSION NUMBER)	(THRU)
10	1
(PAGES)	(CODE)
TMX.64468	21
CR OR TMX OR AD NUMBER)	(CATEGORY)

-35753

TMX.((NASA CR OR TMX OR A

MSC INTERNAL NOTE NO. 68-FM-117

PROJECT APOLLO

RTCC REQUIREMENTS FOR MISSIONS F AND G: SELENOGRAPHIC-MNBY VELOCITY TRANSFORMATION FORMULATION

By Paul F. Flanagan Mathematical Physics Branch

May 15, 1968

MISSION PLANNING AND ANALYSIS DIVISION NATIONAL AERONAUTICS AND SPACE ADMINISTRATION MANNED SPACECRAFT CENTER HOUSTON, TEXAS

Approved: James C. McPherson, Chief

Mathematical Physics Branch

Approved:

John P. Mayer, Chief Mission Planning and Analysis Division

RTCC REQUIREMENTS FOR MISSIONS F AND G:

SELENOGRAPHIC-MNBY VELOCITY TRANSFORMATION FORMULATION

By Paul F. Flanagan

SUMMARY

This document presents the formulation and implementation procedures for use in the RTCC for transforming velocity vectors from the selenographic coordinate system to the mean nearest Besselian year (MNBY) system. The formulation includes equations for computing the lunar angular velocity vector.

INTRODUCTION

The selenocentric MNBY system is moon centered and has its axes parallel to the following: the X-axis is in the mean earth equatorial plane and through the mean vernal equinox at the beginning of the nearest Besselian year; the Z-axis is north through the mean earth spin axis; and the Y-axis is on the mean earth equatorial plane and forms a righthanded orthogonal system.

The moon fixed selenographic system is defined as follows. The X-axis is fixed in the moon's equatorial plane and points approximately toward the center of the earth; the Z-axis is fixed in the moon through the moon spin axis; and the Y-axis is in the equatorial plane and completes the right-handed orthogonal system.

The interpolated precession-libration matrix (L) used to transform the velocity is also used to transform position vectors. If R_M is a position vector in the selenocentric MNBY system and R_G is a position vector in the selenographic system, then

$$R_M = L^T R_G$$

and

 $R_{G} = LR_{M}$.

VELOCITY VECTOR TRANSFORMATION

The inertial MNBY velocity, $\bar{R}_{\rm M}^{}$, of a vehicle with a fixed selenographic position, $R_{\rm G}^{}$, is computed using the following equation

$$\dot{R}_{M} = L^{T}(W \times R_{G})$$

where W is the moon's angular velocity expressed in the selenographic system.

The following general equations can be used to compute the inertial velocity for a vehicle moving relative to the selenographic system at velocity \dot{R}_{α} or for the reverse computation.

$$\dot{\mathbf{R}}_{M} = \mathbf{L}^{\mathbf{T}}(\dot{\mathbf{R}}_{\mathbf{G}} + \mathbf{W} \times \mathbf{R}_{\mathbf{G}})$$

 $\dot{\mathbf{R}}_{\mathbf{G}} = \mathbf{L}\dot{\mathbf{R}}_{M} - \mathbf{W} \times \mathbf{R}_{\mathbf{G}}$

COMPUTATION OF W

The following equations are used to compute the angular velocity vector, W. These equations account for the rate of change of Ω , the longitude of the mean ascending node of the lunar orbit measured in the ecliptic plane from the mean equinox of date, and M, the geocentric mean longitude of the moon measured in the ecliptic plane from the mean equinox of date to the mean ascending node of the lunar orbit, and then along the orbit.

The computations neglect the small effect of the rates of precession, obliquity of the ecliptic, and physical libration. The inclination (i) of the lunar orbit to the ecliptic is constant and is $1^{\circ}32'39''$ (ref. 1).

Prelaunch initialization:

1. Input year of launch, YOL, and day of launch, DOL. January 1 is day 1.

2. Compute Julian centuries from January 0.5, 1900 to midnight prior to launch:

TIL = integral part [(YOL - 1901)/4]
TB = (YOL - 1900)365 + TIL + DOL - 0.5
TM = TB/36525

3. Compute time rates of angles, Ω and M in rad/hr:

 $\Omega = [-1934.1420083 + 0.004155556'TM + (0.66666667 \times 10^{-5})TM^{2}]RATE$

 $\dot{M} = [481267.8831417 - 0.002266667TM + (0.56666667 \times 10^{-5})TM^2]RATE$ where RATE = $\pi/(180 \cdot 36525 \cdot 24) = 1.9110212776572292 \times 10^{-8}$ and converts $\dot{\Omega}$ and \dot{M} from deg/Julian century to rad/hr.

4. Compute constant terms:

 $Kl = \Omega \cos i$ $K2 = \Omega \sin i$

5. Compute W_Z in rad/hr:

 $W_{Z} = \dot{M} - \dot{\Omega} + Kl$

Computation of W_{χ} and W_{χ} at any time t during mission:

1. Input hours from midnight prior launch, H.

2. Compute Julian centuries from January 0.5, 1900 to anytime t:

T = (TB + H/24)/36525

3. Compute M - Ω in deg:

 $M - \Omega = 11.2508889 + 483202.02515T$

- 0.003211111 T^2 - (0.03333333 × 10⁻⁵) T^3

4. Compute W_X and W_Y in rad/hr:

 $W_X = K2 \sin (M - \Omega)$ $W_Y = K2 \cos (M - \Omega)$

A listing of a single-precision checkout program to compute the angular velocity, W, is given in table I. A sample output for RTCC checkout is provided in table II for midnight January 1 through 10, 1969.

3

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR.

TABLE I.- LISTING OF SINGLE-PRECISION CHECKOUT PROGRAM

TO COMPUTE THE ANGULAR VELOCITY VECTOR W

```
ALAL CHO.KI.KS
ACCEPT[YOL, H]
1 ACCEPTITOLI
IYCL=YOL
TIL=(IYO)-1001)/4
TB=(YOL-1900.)*365.+TIL+DOL-.5
TH=TH/36505.
PEGPA=3.14159265/190.
ANGLI=5540.*[EGRA/3600.
OD=(-1934.1420083+(.004155556+.65866878-5+Th)*TM)*D1201
CT=(4%1267.8831417+(-.00226566+.55556667E-5*Th)*TH)*THOCT
K1=OF *COSEANGLII
MC=OD*SIN[AMGLI]
W(3)=(1 D-OD+K1)
T=(T3+F/24.)/36525.
ENO=(11.250889+(483202.02515+(-.003211111-.03333333E-5*T)*T)*T)*DEGRA
W(1) = (K2 \times SIN[MMO])
W(2) = (K2*COS[MMO])
27=1.0/(36525.0*24.0)
W(1)=W(1)*77.
"(2)="(2)*77
1(3)=1(3)*77
DISPLAY[W(1),W(2),W(3)]
DISPLAY[YOL,DOL,H]
CC TC 1
711
```

TABLE II.- ANGULAR VELOCITY VECTORS FOR

PRELAUNCH INITIALIZATION FOR MIDNIGHT OF JANUARY 1 THROUGH 10, 1969

Day	Angular velocity, rad/hr		
200	W _x	W y	Wz
l	$-0.929147614 \times 10^{-6}$	-0.454106239 × 10 ⁻⁶	$0.958135087 \times 10^{-2}$
2	-0.100841172 × 10 ⁻⁵	-0.229420041 × 10 ⁻⁶	$0.958135087 \times 10^{-2}$
3	$-0.103415296 \times 10^{-5}$	0.744292239 × 10 ⁻⁸	$0.958135087 \times 10^{-2}$
4	-0.100500508 × 10 ⁻⁵	0.24391089 × 10 ⁻⁶	$0.958135087 \times 10^{-2}$
5	$-0.922515165 \times 10^{-6}$	0.467432877 × 10 ⁻⁶	$0.958135087 \times 10^{-2}$
6	$-0.791061451 \times 10^{-6}$	0.666145255 × 10 ⁻⁶	$0.958135087 \times 10^{-2}$
7	$-0.617621078 \times 10^{-6}$	$0.829501023 \times 10^{-6}$	$0.958135087 \times 10^{-2}$
8	$-0.411399568 \times 10^{-6}$	0.948829879 × 10 ⁻⁶	$0.958135087 \times 10^{-2}$
9	-0.183342448 × 10 ⁻⁶	0.101779825 × 10 ⁻⁵	$0.958135087 \times 10^{-2}$
10	$0.544458047 \times 10^{-7}$	0.103274556 × 10 ⁻⁵	$0.958135087 \times 10^{-2}$

5

REFERENCE

 Roth, H.: Description of Two Modified Versions of the Selenographic Coordinate Transformation Program (Phase I). Report No. 3400-6059-RU000, July 21, 1965.

6